



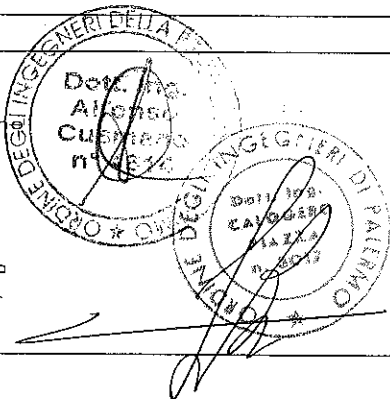
CITTA' DI PALERMO

LAVORI DI CONSOLIDAMENTO STRUTTURALE DELLA PALESTRA
ANNESSA AL PLESSO SCOLASTICO "L. SCIASCIA"
VIA DE GOBBIS N° 13 PALERMO

Progettisti e D.L.:

Ing. Alfonso Cusmano

Ing. Calogero Piazza



Visti

L'Impresa

Elaborato:

Consolidamento strutturale:
Tabulato di calcolo progetto

Tav.

ST.05

Scala:

Data

Archivio

C:\..\sciascia\pro-terra

DATI STRUTTURA:

*** DATI STRUTTURA

NODI--	Coord. X	Coord. Y	Coord. Z	num.=
1	0.0000	480.0000	0.0000	119
2	0.0000	480.0000	318.0000	
3	0.0000	480.0000	613.0000	
4	0.0000	960.0000	0.0000	
5	0.0000	960.0000	318.0000	
6	0.0000	960.0000	613.0000	
7	0.0000	1440.0000	0.0000	
8	0.0000	1440.0000	318.0000	
9	0.0000	1440.0000	613.0000	
10	0.0000	1920.0000	0.0000	
11	0.0000	1920.0000	318.0000	
12	0.0000	1920.0000	613.0000	
13	0.0000	1920.0000	376.0000	
14	0.0000	240.0000	0.0000	
15	0.0000	240.0000	318.0000	
16	0.0000	720.0000	0.0000	
17	0.0000	720.0000	318.0000	
18	0.0000	1200.0000	0.0000	
19	0.0000	1200.0000	318.0000	
20	0.0000	1680.0000	0.0000	
21	0.0000	1680.0000	318.0000	
22	0.0000	2040.0000	0.0000	
23	0.0000	2040.0000	376.0000	
24	0.0000	2400.0000	0.0000	
25	0.0000	2400.0000	376.0000	
26	0.0000	2400.0000	668.0000	
27	0.0000	0.0000	376.0000	
28	0.0000	0.0000	613.0000	
29	0.0000	0.0000	318.0000	
30	0.0000	0.0000	0.0000	
31	0.0000	0.0000	668.0000	
32	0.0000	1920.0000	668.0000	
33	360.0000	0.0000	0.0000	
34	840.0000	0.0000	0.0000	
35	1200.0000	0.0000	0.0000	
36	360.0000	0.0000	376.0000	
37	360.0000	0.0000	668.0000	
38	840.0000	0.0000	376.0000	
39	840.0000	0.0000	668.0000	
40	1200.0000	0.0000	376.0000	
41	1200.0000	0.0000	613.0000	
42	1200.0000	0.0000	668.0000	
43	1200.0000	240.0000	0.0000	
44	1200.0000	480.0000	0.0000	
45	1200.0000	720.0000	0.0000	
46	1200.0000	960.0000	0.0000	
47	1200.0000	1200.0000	0.0000	
48	1200.0000	1440.0000	0.0000	
49	1200.0000	1680.0000	0.0000	
50	1200.0000	1920.0000	0.0000	
52	1200.0000	2400.0000	0.0000	
53	1200.0000	240.0000	376.0000	
54	1200.0000	480.0000	376.0000	
55	1200.0000	480.0000	613.0000	
56	1200.0000	960.0000	376.0000	
57	1200.0000	960.0000	613.0000	
58	1200.0000	1440.0000	376.0000	
59	1200.0000	1440.0000	613.0000	
60	1200.0000	1920.0000	376.0000	
61	1200.0000	1920.0000	613.0000	
62	1200.0000	720.0000	376.0000	
63	1200.0000	1200.0000	376.0000	
64	1200.0000	1680.0000	376.0000	
65	1200.0000	2160.0000	376.0000	
66	1200.0000	2160.0000	0.0000	
67	1200.0000	2400.0000	376.0000	
68	1200.0000	2400.0000	613.0000	
69	1200.0000	2400.0000	668.0000	
72	360.0000	2400.0000	0.0000	
73	840.0000	2400.0000	0.0000	
74	360.0000	2400.0000	376.0000	
75	360.0000	2400.0000	668.0000	
76	840.0000	2400.0000	376.0000	
77	840.0000	2400.0000	668.0000	
78	0.0000	480.0000	668.0000	
79	1200.0000	480.0000	668.0000	
80	0.0000	960.0000	668.0000	
81	1200.0000	960.0000	668.0000	
82	0.0000	1440.0000	668.0000	
83	1200.0000	1440.0000	668.0000	
84	1200.0000	1920.0000	668.0000	

85	300.0000	1920.0000	668.0000
86	900.0000	1920.0000	668.0000
87	300.0000	1440.0000	668.0000
88	900.0000	1440.0000	668.0000
89	300.0000	960.0000	668.0000
90	900.0000	960.0000	668.0000
91	300.0000	480.0000	668.0000
92	900.0000	480.0000	668.0000
93	600.0000	1920.0000	668.0000
94	600.0000	1440.0000	668.0000
95	600.0000	960.0000	668.0000
96	600.0000	480.0000	668.0000
97	300.0000	480.0000	638.0000
98	900.0000	480.0000	638.0000
99	300.0000	960.0000	638.0000
100	900.0000	960.0000	638.0000
101	900.0000	1440.0000	638.0000
102	300.0000	1440.0000	638.0000
103	300.0000	1920.0000	638.0000
104	900.0000	1920.0000	638.0000
105	600.0000	480.0000	623.0000
108	600.0000	960.0000	623.0000
109	600.0000	1440.0000	623.0000
110	600.0000	1920.0000	623.0000
111	120.0000	0.0000	668.0000
112	240.0000	0.0000	668.0000
113	480.0000	0.0000	668.0000
114	600.0000	0.0000	668.0000
115	720.0000	0.0000	668.0000
116	960.0000	0.0000	668.0000
117	1080.0000	0.0000	668.0000
118	120.0000	2400.0000	668.0000
119	240.0000	2400.0000	668.0000
120	480.0000	2400.0000	668.0000
121	600.0000	2400.0000	668.0000
122	720.0000	2400.0000	668.0000
123	960.0000	2400.0000	668.0000
124	1080.0000	2400.0000	668.0000

ASTE	Nome	Proprieta	Nodo iniz.	Nodo fin.	Rilasci in.	Rilasci fin.	num.=	Orient.
	1	2	1	2			205	0.0
	2	2	2	3				0.0
	3	2	4	5				0.0
	4	2	5	6				0.0
	5	2	7	8				0.0
	6	2	8	9				0.0
	7	2	10	11				0.0
	8	2	13	12				0.0
	9	2	11	13				0.0
	10	3	14	15				0.0
	11	3	16	17				0.0
	12	3	18	19				0.0
	13	3	20	21				0.0
	14	3	22	23				0.0
	15	3	24	25				0.0
	16	3	25	26				0.0
	17	3	27	28				0.0
	18	3	30	29				0.0
	19	3	29	27				0.0
	20	3	28	31				0.0
	21	4	29	15	RyRz	RyRz		0.0
	22	4	15	2	RyRz	RyRz		0.0
	23	4	2	17	RyRz	RyRz		0.0
	24	4	17	5	RyRz	RyRz		0.0
	25	4	5	19	RyRz	RyRz		0.0
	26	4	19	8	RyRz	RyRz		0.0
	27	4	8	21	RyRz	RyRz		0.0
	28	4	21	11	RyRz	RyRz		0.0
	29	4	13	23	RyRz	RyRz		0.0
	30	4	23	25	RyRz	RyRz		0.0
	31	4	32	26	RyRz	RyRz		0.0
	32	4	9	12	RyRz	RyRz		0.0
	33	4	6	9	RyRz	RyRz		0.0
	34	4	3	6	RyRz	RyRz		0.0
	35	4	28	3	RyRz	RyRz		0.0
	36	5	30	14				180.0
	37	5	14	1				180.0
	38	5	1	16				180.0
	39	5	16	4				180.0
	40	5	4	18				180.0
	41	5	18	7				180.0
	42	5	7	20				180.0
	43	5	20	10				180.0
	44	5	10	22				180.0
	45	5	22	24				180.0
	46	5	30	33				180.0
	47	5	33	34				180.0

48		34	35			180.0
49		33	36			90.0
50		36	37			90.0
51		34	38			90.0
52	3	38	39			90.0
53	3	35	40			0.0
54	3	40	41			0.0
55	3	41	42			0.0
56	4	27	36	RyRz	RyRz	0.0
57	4	36	38	RyRz	RyRz	0.0
58	4	38	40	RyRz	RyRz	0.0
62	5	35	43			180.0
63	5	43	44			180.0
64	5	44	45			180.0
65	5	45	46			180.0
66	5	46	47			180.0
67	5	47	48			180.0
68	5	48	49			180.0
69	5	49	50			180.0
73	2	44	54			0.0
74	2	54	55			0.0
75	2	46	56			0.0
76	2	56	57			0.0
77	2	48	58			0.0
78	2	58	59			0.0
79	2	50	60			0.0
80	2	60	61			0.0
81	3	43	53			0.0
82	3	45	62			0.0
83	3	47	63			0.0
84	3	49	64			0.0
85	3	66	65			0.0
86	3	52	67			0.0
87	3	67	68			0.0
88	3	68	69			0.0
89	4	41	55	RyRz	RyRz	0.0
90	4	55	57	RyRz	RyRz	0.0
91	4	57	59	RyRz	RyRz	0.0
92	4	59	61	RyRz	RyRz	0.0
93	4	61	68	RyRz	RyRz	0.0
94	4	40	53	RyRz	RyRz	0.0
95	4	53	54	RyRz	RyRz	0.0
96	4	54	62	RyRz	RyRz	0.0
97	4	62	56	RyRz	RyRz	0.0
98	4	56	63	RyRz	RyRz	0.0
99	4	63	58	RyRz	RyRz	0.0
100	4	58	64	RyRz	RyRz	0.0
101	4	64	60	RyRz	RyRz	0.0
102	4	60	65	RyRz	RyRz	0.0
103	4	65	67	RyRz	RyRz	0.0
104	5	50	66			180.0
105	5	66	52			180.0
107	5	24	72			180.0
108	5	72	73			180.0
109	5	73	52			180.0
110	6	1	44			0.0
111	6	4	46			0.0
112	6	7	48			0.0
113	6	10	50			0.0
114	3	72	74			90.0
115	3	74	75			90.0
116	3	73	76			90.0
117	3	76	77			90.0
118	4	25	74	RyRz	RyRz	0.0
122	4	74	76	RyRz	RyRz	0.0
123	4	76	67	RyRz	RyRz	0.0
128	2	55	79			0.0
129	2	57	81			0.0
130	2	59	83			0.0
131	2	61	84			0.0
132	2	3	78			0.0
133	2	6	80			0.0
134	2	9	82			0.0
135	2	12	32			0.0
136	1	32	85			0.0
139	1	86	84			0.0
140	1	82	87			0.0
143	1	88	83			0.0
144	1	80	89			0.0
147	1	90	81			0.0
148	1	78	91			0.0
151	1	92	79			0.0
152	1	85	93			0.0
153	1	93	86			0.0
154	1	87	94			0.0
155	1	94	88			0.0
156	1	89	95			0.0
157	1	95	90			0.0

18	SX	60	X	3.4467E+01
19	SX	74	X	4.3925E+01
20	SX	76	X	4.3925E+01
21	SX	53	X	2.5975E+01
22	SX	54	X	3.4467E+01
23	SX	62	X	2.5975E+01
24	SX	56	X	3.4467E+01
25	SX	63	X	2.5975E+01
26	SX	58	X	3.4467E+01
27	SX	64	X	2.5975E+01
28	SX	65	X	2.5975E+01
29	SX	41	X	1.0767E+02
30	SX	28	X	6.9626E+01
31	SX	3	X	1.4301E+02
32	SX	6	X	1.4301E+02
33	SX	9	X	1.4301E+02
34	SX	12	X	7.4954E+01
35	SX	55	X	2.1739E+02
36	SX	57	X	2.1739E+02
37	SX	59	X	2.1739E+02
38	SX	61	X	2.1739E+02
39	SX	68	X	1.0767E+02
40	SX	31	X	2.2062E+02
41	SX	37	X	4.4346E+02
42	SX	39	X	4.4346E+02
43	SX	42	X	2.2062E+02
44	SX	26	X	2.6593E+02
45	SX	32	X	2.2218E+02
46	SX	78	X	1.4988E+02
47	SX	80	X	1.4988E+02
48	SX	82	X	1.4988E+02
49	SX	69	X	1.9073E+02
50	SX	84	X	1.4988E+02
51	SX	79	X	1.4988E+02
52	SX	81	X	1.4988E+02
53	SX	83	X	1.4988E+02
54	SX	75	X	3.8369E+02
55	SX	77	X	3.8369E+02
56	SX	85	X	2.9623E+02
57	SX	86	X	2.9623E+02
58	SX	87	X	2.9623E+02
59	SX	88	X	2.9623E+02
60	SX	89	X	2.9623E+02
61	SX	90	X	2.9623E+02
62	SX	91	X	2.9623E+02
63	SX	92	X	2.9623E+02
64	SX	93	X	2.9623E+02
65	SX	94	X	2.9623E+02
66	SX	95	X	2.9623E+02
67	SX	96	X	2.9623E+02
68	SX	111	X	4.3989E+02
69	SX	112	X	4.3989E+02
70	SX	113	X	4.3989E+02
71	SX	114	X	4.3989E+02
72	SX	115	X	4.3989E+02
73	SX	116	X	4.3989E+02
74	SX	117	X	4.3989E+02
75	SX	118	X	3.8011E+02
76	SX	119	X	3.8011E+02
77	SX	120	X	3.8011E+02
78	SX	121	X	3.8011E+02
79	SX	122	X	3.8011E+02
80	SX	123	X	3.8011E+02
81	SX	124	X	3.8011E+02
82	SY	29	Y	3.4841E+01
83	SY	15	Y	6.7156E+01
84	SY	2	Y	7.4675E+01
85	SY	17	Y	6.7156E+01
86	SY	5	Y	7.4675E+01
87	SY	19	Y	6.7156E+01
88	SY	8	Y	7.4675E+01
89	SY	21	Y	6.7156E+01
90	SY	11	Y	3.8400E+01
91	SY	27	Y	5.2715E+01
92	SY	36	Y	1.0701E+02
93	SY	38	Y	1.0701E+02
94	SY	40	Y	6.6597E+01
95	SY	25	Y	6.3392E+01
96	SY	13	Y	4.2895E+01
97	SY	23	Y	7.9804E+01
98	SY	67	Y	3.5054E+01
99	SY	60	Y	3.4467E+01
100	SY	74	Y	4.3925E+01
101	SY	76	Y	4.3925E+01
102	SY	53	Y	2.5975E+01
103	SY	54	Y	3.4467E+01
104	SY	62	Y	2.5975E+01
105	SY	56	Y	3.4467E+01

106	SY	63	Y	2.5975E+01
107	SY	58	Y	3.4467E+01
108	SY	64	Y	2.5975E+01
109	SY	65	Y	2.5975E+01
110	SY	41	Y	1.0767E+02
111	SY	28	Y	6.9626E+01
112	SY	3	Y	1.4301E+02
113	SY	6	Y	1.4301E+02
114	SY	9	Y	1.4301E+02
115	SY	12	Y	7.4954E+01
116	SY	55	Y	2.1739E+02
117	SY	57	Y	2.1739E+02
118	SY	59	Y	2.1739E+02
119	SY	61	Y	2.1739E+02
120	SY	68	Y	1.0767E+02
121	SY	31	Y	2.2062E+02
122	SY	37	Y	4.4346E+02
123	SY	39	Y	4.4346E+02
124	SY	42	Y	2.2062E+02
125	SY	26	Y	2.6593E+02
126	SY	32	Y	2.2218E+02
127	SY	78	Y	1.4988E+02
128	SY	80	Y	1.4988E+02
129	SY	82	Y	1.4988E+02
130	SY	69	Y	1.9073E+02
131	SY	84	Y	1.4988E+02
132	SY	79	Y	1.4988E+02
133	SY	81	Y	1.4988E+02
134	SY	83	Y	1.4988E+02
135	SY	75	Y	3.8369E+02
136	SY	77	Y	3.8369E+02
137	SY	85	Y	2.9623E+02
138	SY	86	Y	2.9623E+02
139	SY	87	Y	2.9623E+02
140	SY	88	Y	2.9623E+02
141	SY	89	Y	2.9623E+02
142	SY	90	Y	2.9623E+02
143	SY	91	Y	2.9623E+02
144	SY	92	Y	2.9623E+02
145	SY	93	Y	2.9623E+02
146	SY	94	Y	2.9623E+02
147	SY	95	Y	2.9623E+02
148	SY	96	Y	2.9623E+02
149	SY	111	Y	4.3989E+02
150	SY	112	Y	4.3989E+02
151	SY	113	Y	4.3989E+02
152	SY	114	Y	4.3989E+02
153	SY	115	Y	4.3989E+02
154	SY	116	Y	4.3989E+02
155	SY	117	Y	4.3989E+02
156	SY	118	Y	3.8011E+02
157	SY	119	Y	3.8011E+02
158	SY	120	Y	3.8011E+02
159	SY	121	Y	3.8011E+02
160	SY	122	Y	3.8011E+02
161	SY	123	Y	3.8011E+02
162	SY	124	Y	3.8011E+02

AREE DI CARICO	SupXY	SupXZ	SupYZ	num.=
1	0.00	0.00	2880000.00	7
2	1735200.00	0.00	0.00	
3	0.00	867600.00	0.00	
4	1034400.00	0.00	0.00	
5	568800.00	0.00	0.00	
6	0.00	517200.00	0.00	
7	0.00	350400.00	0.00	

CARICHI ASTE	Asta	Dir	Tip	RIF	Parametro 1	Parametro 2	Parametro 3	Parametro 4	num.=
163	Peso	136	Z	A 1 glo	-2.5000E-02				656
164	Peso	139	Z	A 1 glo	-2.5000E-02				
165	Peso	152	Z	A 1 glo	-2.5000E-02				
166	Peso	153	Z	A 1 glo	-2.5000E-02				
167	Peso	140	Z	A 1 glo	-2.5000E-02				
168	Peso	143	Z	A 1 glo	-2.5000E-02				
169	Peso	154	Z	A 1 glo	-2.5000E-02				
170	Peso	155	Z	A 1 glo	-2.5000E-02				
171	Peso	144	Z	A 1 glo	-2.5000E-02				
172	Peso	147	Z	A 1 glo	-2.5000E-02				
173	Peso	156	Z	A 1 glo	-2.5000E-02				
174	Peso	157	Z	A 1 glo	-2.5000E-02				
175	Peso	148	Z	A 1 glo	-2.5000E-02				
176	Peso	151	Z	A 1 glo	-2.5000E-02				
177	Peso	158	Z	A 1 glo	-2.5000E-02				
178	Peso	159	Z	A 1 glo	-2.5000E-02				
179	Peso	213	Z	A 1 glo	-2.5000E-02				
180	Peso	216	Z	A 1 glo	-2.5000E-02				

181	Peso	215	Z	A	1	glo	-2.5000E-02
182	Peso	217	Z	A	1	glo	-2.5000E-02
183	Peso	219	Z	A	1	glo	-2.5000E-02
184	Peso	222	Z	A	1	glo	-2.5000E-02
185	Peso	221	Z	A	1	glo	-2.5000E-02
186	Peso	223	Z	A	1	glo	-2.5000E-02
187	Peso	226	Z	A	1	glo	-2.5000E-02
188	Peso	225	Z	A	1	glo	-2.5000E-02
189	Peso	227	Z	A	1	glo	-2.5000E-02
190	Peso	230	Z	A	1	glo	-2.5000E-02
191	Peso	229	Z	A	1	glo	-2.5000E-02
192	Peso	231	Z	A	1	glo	-2.5000E-02
193	Peso	233	Z	A	1	glo	-2.5000E-02
194	Peso	236	Z	A	1	glo	-2.5000E-02
195	Peso	235	Z	A	1	glo	-2.5000E-02
196	Peso	237	Z	A	1	glo	-2.5000E-02
197	Peso	240	Z	A	1	glo	-2.5000E-02
198	Peso	239	Z	A	1	glo	-2.5000E-02
199	Acci	136	Z	A	1	glo	-1.5000E-02
200	Acci	139	Z	A	1	glo	-1.5000E-02
201	Acci	140	Z	A	1	glo	-1.5000E-02
202	Acci	143	Z	A	1	glo	-1.5000E-02
203	Acci	144	Z	A	1	glo	-1.5000E-02
204	Acci	147	Z	A	1	glo	-1.5000E-02
205	Acci	148	Z	A	1	glo	-1.5000E-02
206	Acci	151	Z	A	1	glo	-1.5000E-02
207	Acci	153	Z	A	1	glo	-1.5000E-02
208	Acci	152	Z	A	1	glo	-1.5000E-02
209	Acci	155	Z	A	1	glo	-1.5000E-02
210	Acci	154	Z	A	1	glo	-1.5000E-02
211	Acci	157	Z	A	1	glo	-1.5000E-02
212	Acci	156	Z	A	1	glo	-1.5000E-02
213	Acci	159	Z	A	1	glo	-1.5000E-02
214	Acci	158	Z	A	1	glo	-1.5000E-02
215	Acci	213	Z	A	1	glo	-1.5000E-02
216	Acci	216	Z	A	1	glo	-1.5000E-02
217	Acci	215	Z	A	1	glo	-1.5000E-02
218	Acci	217	Z	A	1	glo	-1.5000E-02
219	Acci	219	Z	A	1	glo	-1.5000E-02
220	Acci	222	Z	A	1	glo	-1.5000E-02
221	Acci	221	Z	A	1	glo	-1.5000E-02
222	Acci	223	Z	A	1	glo	-1.5000E-02
223	Acci	226	Z	A	1	glo	-1.5000E-02
224	Acci	225	Z	A	1	glo	-1.5000E-02
225	Acci	227	Z	A	1	glo	-1.5000E-02
226	Acci	230	Z	A	1	glo	-1.5000E-02
227	Acci	229	Z	A	1	glo	-1.5000E-02
228	Acci	231	Z	A	1	glo	-1.5000E-02
229	Acci	233	Z	A	1	glo	-1.5000E-02
230	Acci	236	Z	A	1	glo	-1.5000E-02
231	Acci	235	Z	A	1	glo	-1.5000E-02
232	Acci	237	Z	A	1	glo	-1.5000E-02
233	Acci	240	Z	A	1	glo	-1.5000E-02
234	Acci	239	Z	A	1	glo	-1.5000E-02
235	Vent	21	X	A	2	glo	7.4870E-03
236	Vent	22	X	A	2	glo	7.4870E-03
237	Vent	23	X	A	2	glo	7.4870E-03
238	Vent	24	X	A	2	glo	7.4870E-03
239	Vent	25	X	A	2	glo	7.4870E-03
240	Vent	26	X	A	2	glo	7.4870E-03
241	Vent	27	X	A	2	glo	7.4870E-03
242	Vent	28	X	A	2	glo	7.4870E-03
243	Vent	19	X	A	2	glo	7.4870E-03
244	Vent	17	X	A	2	glo	7.4870E-03
245	Vent	20	X	A	2	glo	7.4870E-03
246	Vent	35	X	A	2	glo	7.4870E-03
247	Vent	2	X	A	2	glo	7.4870E-03
248	Vent	34	X	A	2	glo	7.4870E-03
249	Vent	4	X	A	2	glo	7.4870E-03
250	Vent	33	X	A	2	glo	7.4870E-03
251	Vent	6	X	A	2	glo	7.4870E-03
252	Vent	32	X	A	2	glo	7.4870E-03
253	Vent	9	X	A	2	glo	7.4870E-03
254	Vent	8	X	A	2	glo	7.4870E-03
255	Vent	29	X	A	2	glo	7.4870E-03
256	Vent	30	X	A	2	glo	7.4870E-03
257	Vent	135	X	A	2	glo	7.4870E-03
258	Vent	31	X	A	2	glo	7.4870E-03
259	Vent	16	X	A	2	glo	7.4870E-03
260	Vent	132	X	A	2	glo	7.4870E-03
261	Vent	133	X	A	2	glo	7.4870E-03
262	Vent	134	X	A	2	glo	7.4870E-03
263	Vent	16	X	A	2	glo	7.4870E-03
264	Vent	15	X	A	2	glo	7.4870E-03
265	Vent	14	X	A	2	glo	7.4870E-03
266	Vent	7	X	A	2	glo	7.4870E-03
267	Vent	13	X	A	2	glo	7.4870E-03
268	Vent	5	X	A	2	glo	7.4870E-03

269	Vent	12	X	A	2	glo	7.4870E-03
270	Vent	3	X	A	2	glo	7.4870E-03
271	Vent	11	X	A	2	glo	7.4870E-03
272	Vent	1	X	A	2	glo	7.4870E-03
273	Vent	10	X	A	2	glo	7.4870E-03
274	Vent	18	X	A	2	glo	7.4870E-03
275	Vent	54	X	A	5	glo	3.7430E-03
276	Vent	55	X	A	5	glo	3.7430E-03
277	Vent	90	X	A	5	glo	3.7430E-03
278	Vent	91	X	A	5	glo	3.7430E-03
279	Vent	92	X	A	5	glo	3.7430E-03
280	Vent	131	X	A	5	glo	3.7430E-03
281	Vent	128	X	A	5	glo	3.7430E-03
282	Vent	129	X	A	5	glo	3.7430E-03
283	Vent	130	X	A	5	glo	3.7430E-03
284	Vent	89	X	A	5	glo	3.7430E-03
285	Vent	74	X	A	5	glo	3.7430E-03
286	Vent	76	X	A	5	glo	3.7430E-03
287	Vent	78	X	A	5	glo	3.7430E-03
288	Vent	80	X	A	5	glo	3.7430E-03
289	Vent	87	X	A	5	glo	3.7430E-03
290	Vent	88	X	A	5	glo	3.7430E-03
291	Vent	93	X	A	5	glo	3.7430E-03
292	Vent	94	X	A	5	glo	3.7430E-03
293	Vent	95	X	A	5	glo	3.7430E-03
294	Vent	96	X	A	5	glo	3.7430E-03
295	Vent	97	X	A	5	glo	3.7430E-03
296	Vent	98	X	A	5	glo	3.7430E-03
297	Vent	99	X	A	5	glo	3.7430E-03
298	Vent	100	X	A	5	glo	3.7430E-03
299	Vent	101	X	A	5	glo	3.7430E-03
300	Vent	102	X	A	5	glo	3.7430E-03
301	Vent	103	X	A	5	glo	3.7430E-03
302	Vent	36	X	A	2	glo	7.4870E-03
303	Vent	37	X	A	2	glo	7.4870E-03
304	Vent	38	X	A	2	glo	7.4870E-03
305	Vent	39	X	A	2	glo	7.4870E-03
306	Vent	40	X	A	2	glo	7.4870E-03
307	Vent	41	X	A	2	glo	7.4870E-03
308	Vent	42	X	A	2	glo	7.4870E-03
309	Vent	43	X	A	2	glo	7.4870E-03
310	Vent	44	X	A	2	glo	7.4870E-03
311	Vent	45	X	A	2	glo	7.4870E-03
312	Vent	19	Y	A	3	glo	7.4870E-03
313	Vent	56	Y	A	3	glo	7.4870E-03
314	Vent	50	Y	A	3	glo	7.4870E-03
315	Vent	52	Y	A	3	glo	7.4870E-03
316	Vent	57	Y	A	3	glo	7.4870E-03
317	Vent	58	Y	A	3	glo	7.4870E-03
318	Vent	54	Y	A	3	glo	7.4870E-03
319	Vent	55	Y	A	3	glo	7.4870E-03
320	Vent	17	Y	A	3	glo	7.4870E-03
321	Vent	20	Y	A	3	glo	7.4870E-03
322	Vent	53	Y	A	3	glo	7.4870E-03
323	Vent	51	Y	A	3	glo	7.4870E-03
324	Vent	49	Y	A	3	glo	7.4870E-03
325	Vent	18	Y	A	3	glo	7.4870E-03
326	Vent	16	Y	A	7	glo	3.7430E-03
327	Vent	115	Y	A	7	glo	3.7430E-03
328	Vent	117	Y	A	7	glo	3.7430E-03
329	Vent	122	Y	A	7	glo	3.7430E-03
330	Vent	123	Y	A	7	glo	3.7430E-03
331	Vent	118	Y	A	7	glo	3.7430E-03
332	Vent	87	Y	A	7	glo	3.7430E-03
333	Vent	88	Y	A	7	glo	3.7430E-03
334	Vent	46	Y	A	3	glo	7.4870E-03
335	Vent	47	Y	A	3	glo	7.4870E-03
336	Vent	48	Y	A	3	glo	7.4870E-03
337	Vent	213	Y	A	3	glo	7.4870E-03
338	Vent	216	Y	A	3	glo	7.4870E-03
339	Vent	215	Y	A	3	glo	7.4870E-03
340	Vent	217	Y	A	3	glo	7.4870E-03
341	Vent	219	Y	A	3	glo	7.4870E-03
342	Vent	222	Y	A	3	glo	7.4870E-03
343	Vent	221	Y	A	3	glo	7.4870E-03
344	Vent	223	Y	A	3	glo	7.4870E-03
345	Vent	226	Y	A	3	glo	7.4870E-03
346	Vent	225	Y	A	3	glo	7.4870E-03
347	Vent	227	Y	A	7	glo	3.7430E-03
348	Vent	230	Y	A	7	glo	3.7430E-03
349	Vent	229	Y	A	7	glo	3.7430E-03
350	Vent	231	Y	A	7	glo	3.7430E-03
351	Vent	233	Y	A	7	glo	3.7430E-03
352	Vent	236	Y	A	7	glo	3.7430E-03
353	Vent	235	Y	A	7	glo	3.7430E-03
354	Vent	237	Y	A	7	glo	3.7430E-03
355	Vent	240	Y	A	7	glo	3.7430E-03
356	Vent	239	Y	A	7	glo	3.7430E-03

357 Pann	21	Z	A	2	glo	-2.0400E-02
358 Pann	22	Z	A	2	glo	-2.0400E-02
359 Pann	23	Z	A	2	glo	-2.0400E-02
360 Pann	24	Z	A	2	glo	-2.0400E-02
361 Pann	25	Z	A	2	glo	-2.0400E-02
362 Pann	26	Z	A	2	glo	-2.0400E-02
363 Pann	27	Z	A	2	glo	-2.0400E-02
364 Pann	28	Z	A	2	glo	-2.0400E-02
365 Pann	29	Z	A	2	glo	-2.0400E-02
366 Pann	30	Z	A	2	glo	-2.0400E-02
367 Pann	45	Z	A	2	glo	-2.0400E-02
368 Pann	44	Z	A	2	glo	-2.0400E-02
369 Pann	43	Z	A	2	glo	-2.0400E-02
370 Pann	42	Z	A	2	glo	-2.0400E-02
371 Pann	41	Z	A	2	glo	-2.0400E-02
372 Pann	40	Z	A	2	glo	-2.0400E-02
373 Pann	39	Z	A	2	glo	-2.0400E-02
374 Pann	38	Z	A	2	glo	-2.0400E-02
375 Pann	37	Z	A	2	glo	-2.0400E-02
376 Pann	36	Z	A	2	glo	-2.0400E-02
377 Pann	31	Z	A	2	glo	-2.0400E-02
378 Pann	32	Z	A	2	glo	-2.0400E-02
379 Pann	33	Z	A	2	glo	-2.0400E-02
380 Pann	34	Z	A	2	glo	-2.0400E-02
381 Pann	35	Z	A	2	glo	-2.0400E-02
382 Pann	62	Z	A	4	glo	-7.2000E-03
383 Pann	63	Z	A	4	glo	-7.2000E-03
384 Pann	64	Z	A	4	glo	-7.2000E-03
385 Pann	65	Z	A	4	glo	-7.2000E-03
386 Pann	66	Z	A	4	glo	-7.2000E-03
387 Pann	67	Z	A	4	glo	-7.2000E-03
388 Pann	68	Z	A	4	glo	-7.2000E-03
389 Pann	69	Z	A	4	glo	-7.2000E-03
390 Pann	104	Z	A	4	glo	-7.2000E-03
391 Pann	105	Z	A	4	glo	-7.2000E-03
392 Pann	103	Z	A	4	glo	-7.2000E-03
393 Pann	102	Z	A	4	glo	-7.2000E-03
394 Pann	101	Z	A	4	glo	-7.2000E-03
395 Pann	100	Z	A	4	glo	-7.2000E-03
396 Pann	99	Z	A	4	glo	-7.2000E-03
397 Pann	98	Z	A	4	glo	-7.2000E-03
398 Pann	97	Z	A	4	glo	-7.2000E-03
399 Pann	96	Z	A	4	glo	-7.2000E-03
400 Pann	95	Z	A	4	glo	-7.2000E-03
401 Pann	94	Z	A	4	glo	-7.2000E-03
402 pann	93	Z	A	5	glo	-2.0400E-02
403 pann	92	Z	A	5	glo	-2.0400E-02
404 pann	91	Z	A	5	glo	-2.0400E-02
405 pann	90	Z	A	5	glo	-2.0400E-02
406 pann	89	Z	A	5	glo	-2.0400E-02
407 Pann	46	Z	A	3	glo	-3.4000E-02
408 Pann	47	Z	A	3	glo	-3.4000E-02
409 Pann	48	Z	A	3	glo	-3.4000E-02
410 Pann	58	Z	A	3	glo	-3.4000E-02
411 Pann	57	Z	A	3	glo	-3.4000E-02
412 Pann	56	Z	A	3	glo	-3.4000E-02
413 Pann	107	Z	A	6	glo	-7.2000E-03
414 Pann	108	Z	A	6	glo	-7.2000E-03
415 Pann	109	Z	A	6	glo	-7.2000E-03
416 Pann	123	Z	A	6	glo	-7.2000E-03
417 Pann	122	Z	A	6	glo	-7.2000E-03
418 Pann	118	Z	A	6	glo	-7.2000E-03
419 Pann	213	Z	A	3	glo	-3.4000E-02
420 Pann	216	Z	A	3	glo	-3.4000E-02
421 Pann	215	Z	A	3	glo	-3.4000E-02
422 Pann	217	Z	A	3	glo	-3.4000E-02
423 Pann	219	Z	A	3	glo	-3.4000E-02
424 Pann	222	Z	A	3	glo	-3.4000E-02
425 Pann	221	Z	A	3	glo	-3.4000E-02
426 Pann	223	Z	A	3	glo	-3.4000E-02
427 Pann	226	Z	A	3	glo	-3.4000E-02
428 Pann	225	Z	A	3	glo	-3.4000E-02
429 pann	227	Z	A	7	glo	-3.4000E-02
430 pann	230	Z	A	7	glo	-3.4000E-02
431 pann	229	Z	A	7	glo	-3.4000E-02
432 pann	231	Z	A	7	glo	-3.4000E-02
433 pann	233	Z	A	7	glo	-3.4000E-02
434 pann	236	Z	A	7	glo	-3.4000E-02
435 pann	235	Z	A	7	glo	-3.4000E-02
436 pann	237	Z	A	7	glo	-3.4000E-02
437 pann	240	Z	A	7	glo	-3.4000E-02
438 pann	239	Z	A	7	glo	-3.4000E-02
439 Perm	136	Z	A	1	glo	-1.5000E-02
440 Perm	139	Z	A	1	glo	-1.5000E-02
441 Perm	152	Z	A	1	glo	-1.5000E-02
442 Perm	153	Z	A	1	glo	-1.5000E-02
443 Perm	140	Z	A	1	glo	-1.5000E-02
444 Perm	143	Z	A	1	glo	-1.5000E-02

445	Perm	154	Z	A	1	glo	-1.5000E-02		
446	Perm	155	Z	A	1	glo	-1.5000E-02		
447	Perm	144	Z	A	1	glo	-1.5000E-02		
448	Perm	147	Z	A	1	glo	-1.5000E-02		
449	Perm	156	Z	A	1	glo	-1.5000E-02		
450	Perm	157	Z	A	1	glo	-1.5000E-02		
451	Perm	148	Z	A	1	glo	-1.5000E-02		
452	Perm	151	Z	A	1	glo	-1.5000E-02		
453	Perm	158	Z	A	1	glo	-1.5000E-02		
454	Perm	159	Z	A	1	glo	-1.5000E-02		
455	Perm	213	Z	A	1	glo	-1.5000E-02		
456	Perm	216	Z	A	1	glo	-1.5000E-02		
457	Perm	215	Z	A	1	glo	-1.5000E-02		
458	Perm	217	Z	A	1	glo	-1.5000E-02		
459	Perm	219	Z	A	1	glo	-1.5000E-02		
460	Perm	222	Z	A	1	glo	-1.5000E-02		
461	Perm	221	Z	A	1	glo	-1.5000E-02		
462	Perm	223	Z	A	1	glo	-1.5000E-02		
463	Perm	226	Z	A	1	glo	-1.5000E-02		
464	Perm	225	Z	A	1	glo	-1.5000E-02		
465	Perm	227	Z	A	1	glo	-1.5000E-02		
466	Perm	230	Z	A	1	glo	-1.5000E-02		
467	Perm	229	Z	A	1	glo	-1.5000E-02		
468	Perm	231	Z	A	1	glo	-1.5000E-02		
469	Perm	233	Z	A	1	glo	-1.5000E-02		
470	Perm	236	Z	A	1	glo	-1.5000E-02		
471	Perm	235	Z	A	1	glo	-1.5000E-02		
472	Perm	237	Z	A	1	glo	-1.5000E-02		
473	Perm	240	Z	A	1	glo	-1.5000E-02		
474	Perm	239	Z	A	1	glo	-1.5000E-02		
475	pret	188	Z	TE	loc		-1.4000E+02	-1.4000E+02	
476	pret	190	Z	TE	loc		-1.4000E+02	-1.4000E+02	
477	pret	191	Z	TE	loc		-1.4000E+02	-1.4000E+02	
478	pret	193	Z	TE	loc		-1.4000E+02	-1.4000E+02	
479	pret	194	Z	TE	loc		-1.4000E+02	-1.4000E+02	
480	pret	196	Z	TE	loc		-1.4000E+02	-1.4000E+02	
481	pret	197	Z	TE	loc		-1.4000E+02	-1.4000E+02	
482	pret	199	Z	TE	loc		-1.4000E+02	-1.4000E+02	
483	pret	201	Z	TE	loc		-1.4000E+02	-1.4000E+02	
484	pret	200	Z	TE	loc		-1.4000E+02	-1.4000E+02	
485	pret	205	Z	TE	loc		-1.4000E+02	-1.4000E+02	
486	pret	204	Z	TE	loc		-1.4000E+02	-1.4000E+02	
487	pret	208	Z	TE	loc		-1.4000E+02	-1.4000E+02	
488	pret	207	Z	TE	loc		-1.4000E+02	-1.4000E+02	
489	pret	211	Z	TE	loc		-1.4000E+02	-1.4000E+02	
490	pret	210	Z	TE	loc		-1.4000E+02	-1.4000E+02	
491	Cari	19	Z	TE	loc		1.5000E+01	1.5000E+01	
492	Cari	50	Z	TE	loc		1.5000E+01	1.5000E+01	
493	Cari	52	Z	TE	loc		1.5000E+01	1.5000E+01	
494	Cari	54	Z	TE	loc		1.5000E+01	1.5000E+01	
495	Cari	55	Z	TE	loc		1.5000E+01	1.5000E+01	
496	Cari	17	Z	TE	loc		1.5000E+01	1.5000E+01	
497	Cari	20	Z	TE	loc		1.5000E+01	1.5000E+01	
498	Cari	16	Z	TE	loc		1.5000E+01	1.5000E+01	
499	Cari	115	Z	TE	loc		1.5000E+01	1.5000E+01	
500	Cari	117	Z	TE	loc		1.5000E+01	1.5000E+01	
501	Cari	87	Z	TE	loc		1.5000E+01	1.5000E+01	
502	Cari	88	Z	TE	loc		1.5000E+01	1.5000E+01	
503	Cari	10	Z	TE	loc		1.5000E+01	1.5000E+01	
504	Cari	11	Z	TE	loc		1.5000E+01	1.5000E+01	
505	Cari	12	Z	TE	loc		1.5000E+01	1.5000E+01	
506	Cari	13	Z	TE	loc		1.5000E+01	1.5000E+01	
507	Cari	49	Z	TE	loc		1.5000E+01	1.5000E+01	
508	Cari	53	Z	TE	loc		1.5000E+01	1.5000E+01	
509	Cari	51	Z	TE	loc		1.5000E+01	1.5000E+01	
510	Cari	14	Z	TE	loc		1.5000E+01	1.5000E+01	
511	Cari	15	Z	TE	loc		1.5000E+01	1.5000E+01	
512	Cari	18	Z	TE	loc		1.5000E+01	1.5000E+01	
513	Cari	114	Z	TE	loc		1.5000E+01	1.5000E+01	
514	Cari	116	Z	TE	loc		1.5000E+01	1.5000E+01	
515	Cari	81	Z	TE	loc		1.5000E+01	1.5000E+01	
516	Cari	82	Z	TE	loc		1.5000E+01	1.5000E+01	
517	Cari	83	Z	TE	loc		1.5000E+01	1.5000E+01	
518	Cari	84	Z	TE	loc		1.5000E+01	1.5000E+01	
519	Cari	85	Z	TE	loc		1.5000E+01	1.5000E+01	
520	Cari	86	Z	TE	loc		1.5000E+01	1.5000E+01	
521	Cari	2	Z	TE	loc		1.5000E+01	1.5000E+01	
522	Cari	4	Z	TE	loc		1.5000E+01	1.5000E+01	
523	Cari	6	Z	TE	loc		1.5000E+01	1.5000E+01	
524	Cari	9	Z	TE	loc		1.5000E+01	1.5000E+01	
525	Cari	8	Z	TE	loc		1.5000E+01	1.5000E+01	
526	Cari	135	Z	TE	loc		1.5000E+01	1.5000E+01	
527	Cari	132	Z	TE	loc		1.5000E+01	1.5000E+01	
528	Cari	133	Z	TE	loc		1.5000E+01	1.5000E+01	
529	Cari	134	Z	TE	loc		1.5000E+01	1.5000E+01	
530	Cari	131	Z	TE	loc		1.5000E+01	1.5000E+01	
531	Cari	128	Z	TE	loc		1.5000E+01	1.5000E+01	
532	Cari	129	Z	TE	loc		1.5000E+01	1.5000E+01	

621	comp	136	X	FC	loc	4.0000E+04	4.0000E+04		
622	comp	139	X	FC	loc	-4.0000E+04	-4.0000E+04	3.0000E+02	0.0000E+00
623	comp	143	X	FC	loc	-4.0000E+04	-4.0000E+04	3.0000E+02	0.0000E+00
624	comp	147	X	FC	loc	-4.0000E+04	-4.0000E+04	3.0000E+02	0.0000E+00
625	comp	151	X	FC	loc	-4.0000E+04	-4.0000E+04	3.0000E+02	0.0000E+00
626	Nuov	136	Z	A	1 glo	-6.5000E-03			
627	Nuov	139	Z	A	1 glo	-6.5000E-03			
628	Nuov	152	Z	A	1 glo	-6.5000E-03			
629	Nuov	153	Z	A	1 glo	-6.5000E-03			
630	Nuov	140	Z	A	1 glo	-6.5000E-03			
631	Nuov	143	Z	A	1 glo	-6.5000E-03			
632	Nuov	154	Z	A	1 glo	-6.5000E-03			
633	Nuov	155	Z	A	1 glo	-6.5000E-03			
634	Nuov	144	Z	A	1 glo	-6.5000E-03			
635	Nuov	147	Z	A	1 glo	-6.5000E-03			
636	Nuov	156	Z	A	1 glo	-6.5000E-03			
637	Nuov	157	Z	A	1 glo	-6.5000E-03			
638	Nuov	148	Z	A	1 glo	-6.5000E-03			
639	Nuov	151	Z	A	1 glo	-6.5000E-03			
640	Nuov	158	Z	A	1 glo	-6.5000E-03			
641	Nuov	159	Z	A	1 glo	-6.5000E-03			
642	Nuov	213	Z	A	1 glo	-6.5000E-03			
643	Nuov	216	Z	A	1 glo	-6.5000E-03			
644	Nuov	215	Z	A	1 glo	-6.5000E-03			
645	Nuov	217	Z	A	1 glo	-6.5000E-03			
646	Nuov	219	Z	A	1 glo	-6.5000E-03			
647	Nuov	222	Z	A	1 glo	-6.5000E-03			
648	Nuov	221	Z	A	1 glo	-6.5000E-03			
649	Nuov	223	Z	A	1 glo	-6.5000E-03			
650	Nuov	226	Z	A	1 glo	-6.5000E-03			
651	Nuov	225	Z	A	1 glo	-6.5000E-03			
652	Nuov	227	Z	A	1 glo	-6.5000E-03			
653	Nuov	230	Z	A	1 glo	-6.5000E-03			
654	Nuov	229	Z	A	1 glo	-6.5000E-03			
655	Nuov	231	Z	A	1 glo	-6.5000E-03			
656	Nuov	233	Z	A	1 glo	-6.5000E-03			
657	Nuov	236	Z	A	1 glo	-6.5000E-03			
658	Nuov	235	Z	A	1 glo	-6.5000E-03			
659	Nuov	237	Z	A	1 glo	-6.5000E-03			
660	Nuov	240	Z	A	1 glo	-6.5000E-03			
661	Nuov	239	Z	A	1 glo	-6.5000E-03			

PESI PROPRI ASTE-----|-----|-----|-----|-----|
 Cond. Nome Carichi Aste
 1 662-818 1-58, 62-69, 73-105, 107-118, 122-123, 128-136,
 139-140, 143-144, 147-148, 151-159, 213, 215-217,
 219, 221-223, 225-227, 229-231, 233, 235-237,
 239-240

CONDIZIONI DI CARICO-----|-----|-----|-----|num.= 13

Nome		
1	Peso_proprio_____	N. carichi: 157 Lista carichi: 662-818
2	Peso_copertura_____	N. carichi: 36 Lista carichi: 163-198
3	Carichi_accid_cop_____	N. carichi: 36 Lista carichi: 199-234
4	Vento_X_____	N. carichi: 77 Lista carichi: 235-311
5	Vento_Y_____	N. carichi: 45 Lista carichi: 312-356
6	Permanente_Tomp_____	N. carichi: 82 Lista carichi: 357-438
7	Perm_in_Copertura_____	N. carichi: 36 Lista carichi: 439-474
8	pretensione_____	N. carichi: 16 Lista carichi: 475-490
9	Carico_Termico_____	N. carichi: 127 Lista carichi: 491-617
10	carichi_per_pretens_____	N. carichi: 8 Lista carichi: 618-625
11	Nuovo_massetto_all_____	N. carichi: 36 Lista carichi: 626-661
12	Sisma_X_____	N. carichi: 81 Lista carichi: 1-81
13	Sisma_Y_____	N. carichi: 81

DATI ANALISI SISMICA:

Analisi sismica - Statica equivalente - (Condizione 14)

Numero condizione generanti carichi sismici : 5
 Condizione 001 con coefficiente 1
 Condizione 006 con coefficiente 1
 Condizione 002 con coefficiente 1
 Condizione 003 con coefficiente 0.33
 Condizione 011 con coefficiente 1

Coefficiente di intensita' sismica = 0.07
 Coefficiente di protezione sismica = 1.2
 Coefficiente di fondazione = 1
 Coefficiente di struttura = 1
 Quota di partenza = 0
 Quota massima = 668

Piani	Masse	C.distrib.	Forze di p	M. torc.	Bar. X	Bar. Y
318.000	12971.56	0.04363	565.9	0.0	0.000	966.037
376.000	17643.16	0.05158	910.1	0.0	686.098	1113.716
613.000	19721.86	0.08410	1658.5	0.0	784.968	1120.077
668.000	143149.40	0.09164	13118.3	0.0	593.254	1156.167

DESCRIZIONE CASI DI CARICO:

NOME	DESCRIZIONE	TIPO	CONDIZ. INSERITE			CASI INSERITI	
			Num.	Coeff.	Segno	Num.	Coeff.
1	P.P.+ Perm.	somma	1	1.000	+		
			2	1.000	+		
			6	1.000	+		
			7	1.000	+		
2	P.P.+Perm.(no masset	somma	1	1.000	+		
			2	1.000	+		
			6	1.000	+		
3	C.2 +Pretens.	somma	8	1.000	+	2	1.000
			10	1.000	+		
4	C.3+Nuevo Massetto	somma	11	1.000	+	3	1.000
5	C.4 + Accid.	somma	3	1.000	+	4	1.000
6	C.5 + Vx	somma	4	1.000	+	5	1.000
7	C.5 + Vy	somma	5	1.000	+	5	1.000
8	C.5 + Dt	somma	9	1.000	±	5	1.000
9	C.5 + Sx	somma	12	1.000	±	5	1.000
10	C.5 + Sy	somma	13	1.000	±	5	1.000

SPOSTAMENTI NODALI:

SPOSTAMENTI NODI DI COPERTURA

CASO DI CARICO : 1 P.P.+ Perm.

COMBINAZIONE

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio_____ +	1.00
2	Peso_copertura_____ +	1.00
6	Permanente_Tomp_____ +	1.00
7	Perm._in_Copertura_ +	1.00

1) +1.00*c001 +1.00*c002 +1.00*c006 +1.00*c007

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0184515	-0.0055271	-0.2239813	0.0000107	-0.0000125	-0.0000009
31	-0.0163999	-0.0050273	-0.2573480	0.0000021	-0.0000102	0.0000010
32	-0.0113701	-0.0052646	-0.2458790	0.0000083	0.0054976	0.0000083
37	-0.0166472	-0.0077481	-0.3620094	-0.0000106	0.0007833	-0.0000027
39	-0.0174971	-0.0067442	-0.3567450	-0.0000172	-0.0008132	0.0000030
42	-0.0176530	-0.0031894	-0.2377985	-0.0000122	-0.0000427	-0.0000010
69	-0.0195594	-0.0051975	-0.2014153	0.0000285	-0.0000401	0.0000009
75	-0.0186903	-0.0024835	-0.3076361	-0.0000002	0.0007899	0.0000074
77	-0.0194006	-0.0020256	-0.3023803	0.0000025	-0.0008233	-0.0000039
78	-0.0102404	-0.0051964	-0.2489442	0.0000061	0.0054987	-0.0000059
79	-0.0249874	-0.0042704	-0.2211030	0.0000097	-0.0055454	0.0000075
80	-0.0098676	-0.0054099	-0.2568651	0.0000104	0.0055065	-0.0000001
81	-0.0261052	-0.0044812	-0.2271406	0.0000137	-0.0055559	0.0000016
82	-0.0102223	-0.0049324	-0.2583357	0.0000018	0.0055067	0.0000016
83	-0.0264811	-0.0039999	-0.2284762	0.0000047	-0.0055565	0.0000000
84	-0.0261693	-0.0042011	-0.2180173	0.0000087	-0.0055451	-0.0000055
85	-0.0151241	-0.0031326	-1.8335659	0.0000022	0.0041228	0.0000047
86	-0.0223828	-0.0027975	-1.8197459	0.0000047	-0.0041692	-0.0000030
87	-0.0142108	-0.0044336	-1.8480274	0.0000019	0.0041268	0.0000017
88	-0.0225043	-0.0039765	-1.8330970	0.0000031	-0.0041766	-0.0000001
89	-0.0138471	-0.0054452	-1.8464986	0.0000122	0.0041267	-0.0000002
90	-0.0221260	-0.0049813	-1.8316199	0.0000134	-0.0041763	0.0000017
91	-0.0140124	-0.0066754	-1.8368098	0.0000122	0.0041231	-0.0000029
92	-0.0212101	-0.0062114	-1.8229231	0.0000135	-0.0041695	0.0000045
93	-0.0187453	-0.0025010	-2.4929652	0.0000069	-0.0000230	0.0000004
94	-0.0183641	-0.0040120	-2.5077554	0.0000020	-0.0000249	0.0000008
95	-0.0179853	-0.0054044	-2.5062193	0.0000133	-0.0000248	0.0000008
96	-0.0176233	-0.0068771	-2.4962144	0.0000093	-0.0000231	0.0000008
111	-0.0163973	-0.0065400	-0.5000932	-0.0000021	0.0009110	-0.0000077
112	-0.0165153	-0.0070584	-0.4608005	-0.0000063	-0.0012120	-0.0000050
113	-0.0168627	-0.0076819	-0.6459331	-0.0000122	0.0026523	0.0000001
114	-0.0170725	-0.0077899	-0.8304824	-0.0000139	-0.0000090	0.0000012
115	-0.0173102	-0.0072617	-0.6436567	-0.0000156	-0.0026733	0.0000055
116	-0.0176188	-0.0062683	-0.4514229	-0.0000155	0.0011740	0.0000076
117	-0.0176694	-0.0048620	-0.4858242	-0.0000139	-0.0009539	0.0000138
118	-0.0184511	-0.0038439	-0.4727034	0.0000071	0.0008862	0.0000094
119	-0.0185552	-0.0031947	-0.4207957	0.0000035	-0.0013707	0.0000043
120	-0.0188505	-0.0017229	-0.6072362	0.0000005	0.0028157	0.0000027
121	-0.0190449	-0.0017090	-0.8034744	0.0000012	-0.0000082	0.0000010
122	-0.0192340	-0.0014997	-0.6051200	0.0000019	-0.0028363	-0.0000012
123	-0.0195277	-0.0024337	-0.4107465	0.0000112	0.0013251	-0.0000063
124	-0.0195744	-0.0036928	-0.4566888	0.0000199	-0.0009391	-0.0000125

SPOSTAMENTI NODI

CASO DI CARICO : 2 P.P.+Perm.(no masset

COMBINAZIONE

N. 3 CONDIZIONI ANALISI STATICA

1	Peso_proprio_____ +	1.00
2	Peso_copertura_____ +	1.00
6	Permanente_Tomp_____ +	1.00

1) +1.00*c001 +1.00*c002 +1.00*c006

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0187934	-0.0054102	-0.1997769	0.0000074	-0.0000199	-0.0000006
31	-0.0167201	-0.0050911	-0.2330896	0.0000038	-0.0000151	0.0000006
32	-0.0140561	-0.0052402	-0.2048634	0.0000077	0.0035589	0.0000057
37	-0.0168804	-0.0067414	-0.3101847	-0.0000206	0.0005886	-0.0000014
39	-0.0174344	-0.0059421	-0.3049209	-0.0000268	-0.0006185	0.0000022
42	-0.0175356	-0.0035275	-0.2135426	-0.0000048	-0.0000382	-0.0000006
69	-0.0195152	-0.0048239	-0.1771560	0.0000214	-0.0000361	0.0000006
75	-0.0189482	-0.0033265	-0.2558281	0.0000096	0.0005952	0.0000051
77	-0.0194121	-0.0028807	-0.2505540	0.0000122	-0.0006287	-0.0000022
78	-0.0128782	-0.0051997	-0.2079077	0.0000066	0.0035599	-0.0000035
79	-0.0224372	-0.0042271	-0.1800660	0.0000097	-0.0036066	0.0000051
80	-0.0127858	-0.0053359	-0.2114302	0.0000092	0.0035642	0.0000002

81	-0.0233106	-0.0043617	-0.1817057	0.0000121	-0.0036136	0.0000014
82	-0.0131642	-0.0050255	-0.2129016	0.0000035	0.0035644	0.0000014
83	-0.0237029	-0.0040493	-0.1830417	0.0000061	-0.0036142	0.0000003
84	-0.0236492	-0.0041787	-0.1769801	0.0000085	-0.0036064	-0.0000033
85	-0.0164895	-0.0037661	-1.2323276	0.0000039	0.0026660	0.0000034
86	-0.0211948	-0.0033628	-1.2184944	0.0000057	-0.0027123	-0.0000016
87	-0.0157494	-0.0046097	-1.2415157	0.0000038	0.0026680	0.0000014
88	-0.0211251	-0.0041274	-1.2265884	0.0000048	-0.0027177	0.0000002
89	-0.0153652	-0.0052660	-1.2399913	0.0000106	0.0026679	0.0000002
90	-0.0207313	-0.0047793	-1.2251148	0.0000117	-0.0027174	0.0000014
91	-0.0153232	-0.0060643	-1.2355547	0.0000107	0.0026662	-0.0000016
92	-0.0199888	-0.0055773	-1.2216688	0.0000119	-0.0027126	0.0000032
93	-0.0188369	-0.0032641	-1.6575647	0.0000071	-0.0000230	0.0000006
94	-0.0184415	-0.0042436	-1.6667799	0.0000040	-0.0000249	0.0000008
95	-0.0180474	-0.0051466	-1.6652498	0.0000115	-0.0000248	0.0000008
96	-0.0176638	-0.0061015	-1.6608056	0.0000090	-0.0000231	0.0000008
111	-0.0167184	-0.0060337	-0.4160587	-0.0000044	0.0006832	-0.0000047
112	-0.0167949	-0.0063319	-0.3855796	-0.0000125	-0.0009232	-0.0000029
113	-0.0170209	-0.0066610	-0.5246964	-0.0000222	0.0020050	0.0000004
114	-0.0171577	-0.0066936	-0.6641082	-0.0000237	-0.0000090	0.0000011
115	-0.0173125	-0.0063144	-0.5224208	-0.0000253	-0.0020260	0.0000038
116	-0.0175134	-0.0055966	-0.3762024	-0.0000195	0.0008851	0.0000052
117	-0.0175461	-0.0046482	-0.4017908	-0.0000121	-0.0007261	0.0000093
118	-0.0187932	-0.0042823	-0.3887093	0.0000081	0.0006583	0.0000064
119	-0.0188607	-0.0038245	-0.3456025	0.0000088	-0.0010820	0.0000031
120	-0.0190530	-0.0027967	-0.4860083	0.0000102	0.0021683	0.0000021
121	-0.0191799	-0.0027504	-0.6371045	0.0000109	-0.0000082	0.0000010
122	-0.0193033	-0.0025776	-0.4838851	0.0000116	-0.0021889	-0.0000005
123	-0.0194946	-0.0031078	-0.3355214	0.0000153	0.0010363	-0.0000038
124	-0.0195249	-0.0038863	-0.3726509	0.0000184	-0.0007113	-0.0000078

SPOSTAMENTI NODI

CASO DI CARICO : 3 C.2 +Pretens.

COMBINAZIONE

N. 2 CONDIZIONI ANALISI STATICA

8	pretensione	+	1.00
10	carichi_per_pretens	+	1.00
N. 1	CASI DI CARICO		
2	P.P.+Perm.(no masset		1.00

1) +1.00*c008 +1.00*c010 +1.00*c002.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0140683	-0.0079095	-0.1993262	0.0000175	-0.0000060	0.0000001
31	-0.0109642	-0.0038193	-0.2326345	-0.0000216	0.0000076	-0.0000001
32	0.0410897	-0.0057547	-0.2013545	0.0000179	-0.0001082	0.0000618
37	-0.0129903	-0.0280824	-0.3103982	0.0000234	0.0005907	-0.0000275
39	-0.0197288	-0.0226203	-0.3051427	0.0000063	-0.0006204	0.0000184
42	-0.0210070	0.0043602	-0.2130903	-0.0001583	-0.0000518	0.0000001
69	-0.0229137	-0.0120652	-0.1767033	0.0001625	-0.0000493	-0.0000001
75	-0.0160221	0.0148805	-0.2560438	-0.0000277	0.0005971	0.0000548
77	-0.0216140	0.0158884	-0.2507741	-0.0000255	-0.0006305	-0.0000378
78	0.0421300	-0.0052232	-0.2043978	0.0000063	-0.0001081	-0.0000541
79	-0.0782205	-0.0045039	-0.1765545	0.0000159	0.0000612	0.0000552
80	0.0479125	-0.0069715	-0.2069323	0.0000400	-0.0000800	-0.0000065
81	-0.0846077	-0.0062243	-0.1772050	0.0000478	0.0000305	0.0000077
82	0.0477425	-0.0030629	-0.2084041	-0.0000337	-0.0000794	0.0000077
83	-0.0849484	-0.0022773	-0.1785410	-0.0000280	0.0000296	-0.0000061
84	-0.0796844	-0.0038995	-0.1734685	0.0000023	0.0000606	-0.0000507
85	0.0103504	0.0099364	-0.1401191	-0.0000383	-0.0002614	0.0000329
86	-0.0486767	0.0092534	-0.1262985	-0.0000240	0.0002151	-0.0000299
87	0.0150869	-0.0006939	-0.1550447	-0.0000384	-0.0002416	0.0000082
88	-0.0523907	-0.0003783	-0.1401214	-0.0000354	0.0001918	-0.0000069
89	0.0153299	-0.0089574	-0.1534169	0.0000487	-0.0002419	-0.0000069
90	-0.0520303	-0.0085868	-0.1385525	0.0000515	0.0001924	0.0000082
91	0.0112420	-0.0190017	-0.1430770	0.0000494	-0.0002618	-0.0000294
92	-0.0472898	-0.0186291	-0.1292088	0.0000527	0.0002155	0.0000306
93	-0.0190962	0.0133777	-0.0765545	-0.0000026	-0.0000230	-0.0000025
94	-0.0187059	0.0010405	-0.0944602	-0.0000413	-0.0000249	0.0000005
95	-0.0183411	-0.0103303	-0.0927874	0.0000542	-0.0000248	0.0000006
96	-0.0181222	-0.0223504	-0.0794146	0.0000224	-0.0000231	0.0000006
111	-0.0109436	-0.0168735	-0.4158123	-0.0000066	0.0006850	-0.0000687
112	-0.0119100	-0.0217805	-0.3855525	0.0000084	-0.0009213	-0.0000460
113	-0.0146995	-0.0282216	-0.5250967	0.0000191	0.0020060	-0.0000049
114	-0.0163625	-0.0297859	-0.6645657	0.0000148	-0.0000091	0.0000045
115	-0.0182530	-0.0261586	-0.5228156	0.0000106	-0.0020270	0.0000389
116	-0.0207259	-0.0194367	-0.3761994	-0.0000486	0.0008833	0.0000560
117	-0.0211401	-0.0086299	-0.4015632	-0.0001035	-0.0007279	0.0001074
118	-0.0140648	0.0051648	-0.3884779	0.0000025	0.0006601	0.0000713
119	-0.0149160	0.0097705	-0.3455926	-0.0000126	-0.0010801	0.0000294
120	-0.0172777	0.0204037	-0.4863940	-0.0000271	0.0021692	0.0000167
121	-0.0188134	0.0198320	-0.6375450	-0.0000266	-0.0000082	0.0000026
122	-0.0203055	0.0208602	-0.4842692	-0.0000261	-0.0021899	-0.0000159
123	-0.0226545	0.0118899	-0.3355217	0.0000371	0.0010344	-0.0000571

124 -0.0230362 0.0009186 -0.3724260 0.0000998 -0.0007132 -0.0001083

SPOSTAMENTI NODI

CASO DI CARICO : 4 C.3+Nuovo Massetto

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
11 Nuovo_massetto_all. + 1.00
N. 1 CASI DI CARICO
3 C.2 +Pretens. 1.00

1) +1.00*c011 +1.00*c003.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0139202	-0.0079601	-0.2098148	0.0000190	-0.0000028	-0.0000001
31	-0.0108255	-0.0037917	-0.2431465	-0.0000223	0.0000097	0.0000001
32	0.0422536	-0.0057653	-0.2191279	0.0000181	0.0007319	0.0000630
37	-0.0128893	-0.0285187	-0.3328556	0.0000278	0.0006751	-0.0000281
39	-0.0197560	-0.0229679	-0.3275998	0.0000104	-0.0007048	0.0000187
42	-0.0210579	0.0045067	-0.2236012	-0.0001615	-0.0000537	-0.0000001
69	-0.0229329	-0.0122271	-0.1872157	0.0001655	-0.0000510	0.0000000
75	-0.0159103	0.0152458	-0.2784940	-0.0000319	0.0006815	0.0000558
77	-0.0216090	0.0162590	-0.2732322	-0.0000297	-0.0007148	-0.0000385
78	0.0432731	-0.0052217	-0.2221803	0.0000061	0.0007320	-0.0000551
79	-0.0793256	-0.0045226	-0.1943372	0.0000160	-0.0007789	0.0000562
80	0.0491770	-0.0070036	-0.2266207	0.0000406	0.0007616	-0.0000066
81	-0.0858186	-0.0062761	-0.1968935	0.0000485	-0.0008112	0.0000078
82	0.0490173	-0.0030226	-0.2280922	-0.0000344	0.0007623	0.0000079
83	-0.0861523	-0.0022559	-0.1982292	-0.0000285	-0.0008121	-0.0000062
84	-0.0807765	-0.0039092	-0.1912512	0.0000024	-0.0007795	-0.0000517
85	0.0109421	0.0102109	-0.4006557	-0.0000391	0.0003699	0.0000335
86	-0.0491915	0.0094984	-0.3868408	-0.0000245	-0.0004162	-0.0000304
87	0.0157536	-0.0006176	-0.4178664	-0.0000392	0.0003906	0.0000083
88	-0.0529884	-0.0003129	-0.4029418	-0.0000361	-0.0004404	-0.0000070
89	0.0159877	-0.0090351	-0.4162367	0.0000494	0.0003902	-0.0000071
90	-0.0526347	-0.0086744	-0.4013714	0.0000523	-0.0004398	0.0000083
91	0.0118100	-0.0192665	-0.4036209	0.0000500	0.0003695	-0.0000300
92	-0.0478190	-0.0189039	-0.3897523	0.0000534	-0.0004158	0.0000312
93	-0.0190565	0.0137083	-0.4385613	-0.0000027	-0.0000230	-0.0000025
94	-0.0186724	0.0011408	-0.4588829	-0.0000421	-0.0000249	0.0000004
95	-0.0183141	-0.0104420	-0.4572076	0.0000550	-0.0000248	0.0000006
96	-0.0181047	-0.0226865	-0.4414251	0.0000225	-0.0000231	0.0000006
111	-0.0108044	-0.0170930	-0.4522272	-0.0000056	0.0007837	-0.0000700
112	-0.0117888	-0.0220954	-0.4181483	0.0000111	-0.0010464	-0.0000469
113	-0.0146310	-0.0286639	-0.5776326	0.0000235	0.0022865	-0.0000050
114	-0.0163256	-0.0302609	-0.7366612	0.0000191	-0.0000091	0.0000045
115	-0.0182520	-0.0265692	-0.5753512	0.0000148	-0.0023075	0.0000396
116	-0.0207716	-0.0197278	-0.4087950	-0.0000469	0.0010084	0.0000570
117	-0.0211935	-0.0087226	-0.4379776	-0.0001042	-0.0008266	0.0001094
118	-0.0139165	0.0053548	-0.4248754	0.0000020	0.0007589	0.0000726
119	-0.0147837	0.0100434	-0.3781763	-0.0000149	-0.0012052	0.0000299
120	-0.0171899	0.0208690	-0.5389260	-0.0000313	0.0024498	0.0000169
121	-0.0187550	0.0202833	-0.7096386	-0.0000308	-0.0000082	0.0000027
122	-0.0202755	0.0213272	-0.5368043	-0.0000303	-0.0024704	-0.0000162
123	-0.0226688	0.0121820	-0.3681192	0.0000354	0.0011596	-0.0000582
124	-0.0230576	0.0010024	-0.4088425	0.0001004	-0.0008119	-0.0001103

SPOSTAMENTI NODI

CASO DI CARICO : 5 C.4 + Accid.

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
3 Carichi_accid_cop_ + 1.00
N. 1 CASI DI CARICO
4 C.3+Nuovo Massetto 1.00

1) +1.00*c003 +1.00*c004.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0135782	-0.0080770	-0.2340192	0.0000223	0.0000046	-0.0000004
31	-0.0105053	-0.0037279	-0.2674048	-0.0000239	0.0000145	0.0000004
32	0.0449396	-0.0057896	-0.2601435	0.0000188	0.0026707	0.0000656
37	-0.0126561	-0.0295254	-0.3846803	0.0000379	0.0008698	-0.0000293
39	-0.0198186	-0.0237699	-0.3794239	0.0000200	-0.0008994	0.0000195
42	-0.0211754	0.0048448	-0.2478571	-0.0001689	-0.0000582	-0.0000004
69	-0.0229771	-0.0126008	-0.2114750	0.0001726	-0.0000550	0.0000004
75	-0.0156523	0.0160888	-0.3303021	-0.0000416	0.0008762	0.0000581
77	-0.0215974	0.0171141	-0.3250585	-0.0000394	-0.0009095	-0.0000402
78	0.0459108	-0.0052184	-0.2632168	0.0000056	0.0026707	-0.0000575
79	-0.0818757	-0.0045660	-0.2353742	0.0000160	-0.0027176	0.0000585
80	0.0520952	-0.0070776	-0.2720556	0.0000417	0.0027039	-0.0000070
81	-0.0886132	-0.0063955	-0.2423283	0.0000502	-0.0027535	0.0000081

82	0.0519592	-0.0029296	-0.2735263	-0.0000362	0.0027046	0.0000081
83	-0.0889306	-0.0022065	-0.2436638	-0.0000298	-0.0027544	-0.0000065
84	-0.0832966	-0.0039316	-0.2322884	0.0000026	-0.0027182	-0.0000540
85	0.0123075	0.0108444	-1.0018940	-0.0000408	0.0018267	0.0000349
86	-0.0503794	0.0100637	-0.9880923	-0.0000255	-0.0018731	-0.0000318
87	0.0172922	-0.0004415	-1.0243781	-0.0000411	0.0018494	0.0000086
88	-0.0543676	-0.0001620	-1.0094504	-0.0000378	-0.0018992	-0.0000074
89	0.0175058	-0.0092142	-1.0227440	0.0000510	0.0018491	-0.0000074
90	-0.0540294	-0.0088764	-1.0078765	0.0000541	-0.0018986	0.0000086
91	0.0131208	-0.0198776	-1.0048760	0.0000514	0.0018263	-0.0000313
92	-0.0490404	-0.0195381	-0.9910066	0.0000550	-0.0018727	0.0000324
93	-0.0189649	0.0144714	-1.2739618	-0.0000028	-0.0000229	-0.0000027
94	-0.0185950	0.0013724	-1.2998584	-0.0000441	-0.0000249	0.0000004
95	-0.0182520	-0.0106999	-1.2981771	0.0000568	-0.0000248	0.0000006
96	-0.0180642	-0.0234621	-1.2768338	0.0000228	-0.0000231	0.0000006
111	-0.0104833	-0.0175993	-0.5362617	-0.0000033	0.0010115	-0.0000731
112	-0.0115092	-0.0228219	-0.4933692	0.0000173	-0.0013352	-0.0000490
113	-0.0144728	-0.0296848	-0.6988693	0.0000334	0.0029338	-0.0000053
114	-0.0162405	-0.0313572	-0.9030353	0.0000289	-0.0000091	0.0000046
115	-0.0182497	-0.0275166	-0.6965871	0.0000245	-0.0029548	0.0000042
116	-0.0208771	-0.0203995	-0.4840155	-0.0000430	0.0012972	0.0000594
117	-0.0213167	-0.0089363	-0.5220110	-0.0001060	-0.0010544	0.0001140
118	-0.0135744	0.0057932	-0.5088695	0.0000010	0.0009868	0.0000756
119	-0.0144782	0.0106733	-0.4533695	-0.0000203	-0.0014939	0.0000311
120	-0.0169875	0.0219428	-0.6601539	-0.0000410	0.0030971	0.0000176
121	-0.0186200	0.0213247	-0.8760085	-0.0000405	-0.0000082	0.0000027
122	-0.0202062	0.0224051	-0.6580392	-0.0000400	-0.0031177	-0.0000169
123	-0.0227020	0.0128561	-0.4433443	0.0000313	0.0014484	-0.0000608
124	-0.0231071	0.0011959	-0.4928804	0.0001019	-0.0010397	-0.0001150

SPOSTAMENTI NODI

CASO DI CARICO : 6 C.5 + Vx

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 4 Vento_X + 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c004 +1.00*c005.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	0.3748141	-0.0020386	-0.2181859	0.0000152	-0.0003240	0.0000319
31	0.3441419	0.0071478	-0.2523146	-0.0000973	-0.0002663	-0.0000348
32	0.4290854	0.0005168	-0.2533321	0.0000194	0.0026538	0.0000556
37	0.3416510	-0.0252225	-0.3671641	0.0000266	0.0009494	-0.0000469
39	0.3333243	-0.0281244	-0.4138298	0.0000279	-0.0008485	0.0000006
42	0.3321733	-0.0065780	-0.2609361	-0.0000865	0.0000947	-0.0000212
69	0.3637924	-0.0178844	-0.2258154	0.0001495	0.0001226	0.0000229
75	0.3722391	0.0185473	-0.3109946	-0.0000459	0.0009611	0.0000472
77	0.3649694	0.0147450	-0.3623389	-0.0000316	-0.0008538	-0.0000487
78	0.4099585	0.0052084	-0.2569524	-0.0000596	0.0026200	-0.0000755
79	0.2818117	-0.0153524	-0.2384787	0.0000866	-0.0026078	0.0000391
80	0.4245715	0.0020639	-0.2670044	-0.0000035	0.0026520	-0.0000224
81	0.2836643	-0.0156002	-0.2438444	0.0000967	-0.0026437	-0.0000075
82	0.4311163	0.0046115	-0.2689888	-0.0000579	0.0026532	-0.0000042
83	0.2900298	-0.0096679	-0.2444339	-0.0000141	-0.0026439	-0.0000186
84	0.3004311	-0.0098217	-0.2353673	-0.0000090	-0.0026139	-0.0000624
85	0.3962837	0.0140659	-0.9883778	-0.0000457	0.0018034	0.0000241
86	0.3333584	0.0068215	-0.9717082	-0.0000303	-0.0018404	-0.0000413
87	0.3963491	0.0033668	-1.0064056	-0.0000515	0.0018137	-0.0000040
88	0.3246108	-0.0039726	-0.9885973	-0.0000332	-0.0018597	-0.0000198
89	0.3898804	-0.0046852	-1.0043976	0.0000357	0.0018146	-0.0000226
90	0.3182646	-0.0134095	-0.9876669	0.0000704	-0.0018579	-0.0000068
91	0.3770104	-0.0147641	-0.9859793	0.0000316	0.0017947	-0.0000485
92	0.3146448	-0.0246330	-0.9720188	0.0000792	-0.0018298	0.0000142
93	0.3648584	0.0143486	-1.2549148	-0.0000076	-0.0000313	-0.0000138
94	0.3603986	0.0013434	-1.2749291	-0.0000469	-0.0000322	-0.0000124
95	0.3540563	-0.0106804	-1.2733888	0.0000573	-0.0000302	-0.0000145
96	0.3456946	-0.0233682	-1.2524402	0.0000250	-0.0000254	-0.0000161
111	0.3440876	-0.0089957	-0.5157757	-0.0000560	0.0009764	-0.0000917
112	0.3429441	-0.0164092	-0.4709277	-0.0000147	-0.0013273	-0.0000668
113	0.3396297	-0.0274893	-0.6937122	0.0000269	0.0030541	-0.0000227
114	0.3376058	-0.0312481	-0.9132033	0.0000272	0.0001200	-0.0000131
115	0.3352797	-0.0296109	-0.7212186	0.0000276	-0.0028489	0.0000225
116	0.3323860	-0.0270197	-0.5186256	-0.0000102	0.0012567	0.0000404
117	0.3320098	-0.0178774	-0.5480495	-0.0000484	-0.0011498	0.0000939
118	0.3746814	0.0106700	-0.4868593	-0.0000052	0.0009462	0.0000659
119	0.3736088	0.0143723	-0.4289466	-0.0000256	-0.0014875	0.0000211
120	0.3706663	0.0230826	-0.6541821	-0.0000424	0.0032278	0.0000071
121	0.3687313	0.0212485	-0.8867474	-0.0000388	0.0001329	-0.0000077
122	0.3667906	0.0210696	-0.6846126	-0.0000352	-0.0030016	-0.0000266
123	0.3639827	0.0094379	-0.4809024	0.0000288	0.0014049	-0.0000696
124	0.3636394	-0.0032318	-0.5212069	0.0000891	-0.0011426	-0.0001228

SPOSTAMENTI NODI

CASO DI CARICO : 7 C.5 + Vy

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 5 Vento_Y + 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c005 +1.00*c005.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0099449	0.2881672	-0.2337403	-0.0002088	0.0000090	0.0000033
31	-0.0141940	0.2930723	-0.2655948	-0.0009332	0.0000097	0.0000340
32	0.0470352	0.2901530	-0.2654859	-0.0009572	0.0026732	0.0000633
37	-0.0163800	0.2669062	-0.3846631	0.0068182	0.0008719	-0.0000320
39	-0.0236735	0.2712349	-0.3787977	0.0068035	-0.0009032	0.0000166
42	-0.0250587	0.2982923	-0.2456189	-0.0009713	-0.0000645	-0.0000339
69	-0.0191503	0.2795086	-0.2114845	-0.0007205	-0.0000491	-0.0000033
75	-0.0119867	0.3113581	-0.3299733	0.0013915	0.0008771	0.0000549
77	-0.0178163	0.3107591	-0.3253130	0.0013936	-0.0009088	-0.0000439
78	0.0434237	0.2912169	-0.2601924	-0.0008462	0.0026685	-0.0000593
79	-0.0842395	0.2882843	-0.2320324	-0.0007895	-0.0027170	0.0000543
80	0.0510828	0.2890280	-0.2634077	-0.0008748	0.0027005	-0.0000091
81	-0.0895451	0.2859393	-0.2333680	-0.0008049	-0.0027509	0.0000040
82	0.0524898	0.2929419	-0.2910264	-0.0010542	0.0027076	0.0000061
83	-0.0883725	0.2897441	-0.2616031	-0.0009799	-0.0027565	-0.0000111
84	-0.0811665	0.2879787	-0.2378110	-0.0008844	-0.0027194	-0.0000585
85	0.0144035	0.3060748	-1.0077319	-0.0009891	0.0018277	0.0000322
86	-0.0482538	0.3032877	-0.9939084	-0.0009419	-0.0018738	-0.0000359
87	0.0178273	0.2947754	-1.0425447	-0.0010383	0.0018510	0.0000061
88	-0.0538200	0.2931027	-1.0278212	-0.0010106	-0.0019000	-0.0000114
89	0.0165116	0.2862072	-1.0133365	-0.0008466	0.0018474	-0.0000099
90	-0.0549864	0.2846675	-0.9983566	-0.0008215	-0.0018974	0.0000048
91	0.0106585	0.2759719	-1.0013771	-0.0007865	0.0018253	-0.0000336
92	-0.0514372	0.2745127	-0.9874736	-0.0007662	-0.0018721	0.0000288
93	-0.0168538	0.3087938	-1.2799107	-0.0009347	-0.0000230	-0.0000060
94	-0.0180547	0.2957152	-1.3182982	-0.0010286	-0.0000245	-0.0000028
95	-0.0192295	0.2838799	-1.2884992	-0.0008295	-0.0000249	-0.0000026
96	-0.0204826	0.2715752	-1.2732034	-0.0008062	-0.0000231	-0.0000024
111	-0.0141749	0.2790694	-0.5352013	0.0016506	0.0010174	-0.0000829
112	-0.0152045	0.2736982	-0.4929443	0.0042344	-0.0013307	-0.0000473
113	-0.0182465	0.2663229	-0.6989858	0.0068146	0.0029340	-0.0000088
114	-0.0200519	0.2642793	-0.9030700	0.0068109	-0.0000105	0.0000016
115	-0.0220851	0.2677634	-0.6963617	0.0068072	-0.0029576	0.0000388
116	-0.0247579	0.2740338	-0.4828957	0.0042119	0.0012929	0.0000523
117	-0.0252085	0.2849856	-0.5203451	0.0016203	-0.0010591	0.0001185
118	-0.0099460	0.3016920	-0.5085202	0.0003246	0.0009863	0.0000698
119	-0.0108361	0.3062496	-0.4529902	0.0008581	-0.0014939	0.0000294
120	-0.0132977	0.3168108	-0.6599617	0.0013920	0.0030985	0.0000142
121	-0.0148970	0.3157850	-0.8759873	0.0013925	-0.0000067	-0.0000007
122	-0.0164504	0.3164619	-0.6581810	0.0013931	-0.0031165	-0.0000203
123	-0.0188902	0.3059871	-0.4436027	0.0006889	0.0014479	-0.0000660
124	-0.0192811	0.2938097	-0.4930400	-0.0000158	-0.0010408	-0.0001163

SPOSTAMENTI NODI

CASO DI CARICO : 8 C.5 + Dt

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 9 Carico_Termico_+/- 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c009 +1.00*c005.001
 2) -1.00*c009 +1.00*c005.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0445791	0.0037333	-0.1145115	0.0013111	0.0003973	-0.0000004
	0.0174226	-0.0198873	-0.3535269	-0.0012666	-0.0003881	-0.0000004
31	-0.0428851	0.0003771	-0.1478086	-0.0038308	0.0003995	0.0000004
	0.0218746	-0.0078330	-0.3870010	0.0037831	-0.0003704	0.0000004
32	0.0070002	-0.0152317	-0.1413495	0.0023364	0.0025169	0.0000816
	0.0828790	0.0036525	-0.3789374	-0.0022989	0.0028244	0.0000496
37	-0.0246935	-0.0232713	-0.2733052	0.0000035	0.0008927	-0.0000255
	-0.0006186	-0.0357796	-0.4960555	0.0000723	0.0008468	-0.0000331
39	-0.0066225	-0.0172291	-0.2681800	-0.0000151	-0.0009222	0.0000180
	-0.0330148	-0.0303108	-0.4906677	0.0000551	-0.0008766	0.0000210

42	0.0123497	0.0101245	-0.1281971	-0.0039865	-0.0004416	-0.0000004
	-0.0547004	-0.0004349	-0.3675172	0.0036486	0.0003252	-0.0000004
69	0.0090527	-0.0211089	-0.0917708	0.0040195	-0.0004427	0.0000003
	-0.0550068	-0.0040926	-0.3311792	-0.0036743	0.0003327	0.0000004
75	-0.0279052	0.0100042	-0.2190200	-0.0000216	0.0008990	0.0000348
	-0.0033995	0.0221734	-0.4415841	-0.0000616	0.0008535	0.0000813
77	-0.0097824	0.0076989	-0.2136835	0.0000021	-0.0009326	-0.0000384
	-0.0334125	0.0265293	-0.4364334	-0.0000810	-0.0008863	-0.0000420
78	0.0117305	-0.0050778	-0.1443723	-0.0020741	0.0025203	-0.0000502
	0.0800912	-0.0053590	-0.3820612	0.0020853	0.0028212	-0.0000648
79	-0.0476036	-0.0029924	-0.1164600	-0.0020644	-0.0025672	0.0000528
	-0.1161479	-0.0061396	-0.3542884	0.0020965	-0.0028680	0.0000642
80	0.0170126	-0.0090862	-0.1586335	-0.0005402	0.0025519	-0.0000038
	0.0871779	-0.0050691	-0.3854776	0.0006237	0.0028560	-0.0000101
81	-0.0547875	-0.0063963	-0.1295180	-0.0005728	-0.0026009	0.0000080
	-0.1224389	-0.0063948	-0.3551387	0.0006732	-0.0029060	0.0000083
82	0.0162016	-0.0073536	-0.1602782	0.0007068	0.0025530	0.0000094
	0.0877168	0.0014945	-0.3867744	-0.0007791	0.0028562	0.0000068
83	-0.0562046	-0.0038595	-0.1306790	0.0005938	-0.0026032	-0.0000028
	-0.1216565	-0.0005535	-0.3566485	-0.0006535	-0.0029056	-0.0000102
84	-0.0516926	-0.0081443	-0.1132907	0.0021012	-0.0025663	-0.0000483
	-0.1149005	0.0002810	-0.3512861	-0.0020960	-0.0028701	-0.0000596
85	-0.0084953	0.0050885	-0.8391760	0.0021876	0.0017112	0.0000396
	0.0331104	0.0166003	-1.1646119	-0.0022692	0.0019423	0.0000301
86	-0.0359946	0.0043215	-0.8254415	0.0021561	-0.0017577	-0.0000279
	-0.0647643	0.0158058	-1.1507431	-0.0022071	-0.0019884	-0.0000357
87	-0.0013930	-0.0043776	-0.8678415	0.0006639	0.0017356	0.0000109
	0.0359775	0.0034945	-1.1809148	-0.0007461	0.0019632	0.0000063
88	-0.0387988	-0.0027852	-0.8531352	0.0006252	-0.0017849	-0.0000051
	-0.0699364	0.0024611	-1.1657656	-0.0007008	-0.0020135	-0.0000097
89	-0.0004059	-0.0102963	-0.8658719	-0.0005450	0.0017348	-0.0000045
	0.0354175	-0.0081321	-1.1796160	0.0006470	0.0019633	-0.0000104
90	-0.0373526	-0.0088868	-0.8513615	-0.0005575	-0.0017833	0.0000090
	-0.0707062	-0.0088659	-1.1643915	0.0006657	-0.0020139	0.0000082
91	-0.0039162	-0.0177656	-0.8429170	-0.0020324	0.0017126	-0.0000262
	0.0301577	-0.0219897	-1.1668350	0.0021353	0.0019400	-0.0000364
92	-0.0318757	-0.0165560	-0.8290080	-0.0020310	-0.0017591	0.0000297
	-0.0662050	-0.0225201	-1.1530052	0.0021410	-0.0019862	0.0000351
93	-0.0220440	0.0083256	-1.0921901	0.0022101	-0.0000228	-0.0000048
	-0.0158857	0.0206172	-1.4557336	-0.0022157	-0.0000231	-0.0000006
94	-0.0202426	-0.0017984	-1.1245774	0.0006380	-0.0000245	0.0000025
	-0.0169474	0.0045432	-1.4751394	-0.0007262	-0.0000253	-0.0000017
95	-0.0188660	-0.0110352	-1.1225116	-0.0005468	-0.0000242	0.0000024
	-0.0176380	-0.0103645	-1.4738426	0.0006605	-0.0000254	-0.0000013
96	-0.0179861	-0.0203883	-1.0960687	-0.0020595	-0.0000232	0.0000022
	-0.0181423	-0.0265359	-1.4575990	0.0021050	-0.0000230	-0.0000010
111	-0.0360315	-0.0127046	-0.4193999	-0.0025527	0.0010343	-0.0000669
	0.0150650	-0.0224941	-0.6531236	0.0025462	0.0009887	-0.0000793
112	-0.0302808	-0.0172129	-0.3792461	-0.0012746	-0.0013124	-0.0000430
	0.0072624	-0.0284308	-0.6074922	0.0013092	-0.0013581	-0.0000550
113	-0.0201902	-0.0231334	-0.5895764	-0.0000012	0.0029456	-0.0000028
	-0.0087555	-0.0362363	-0.8081623	0.0000680	0.0029221	-0.0000078
114	-0.0156623	-0.0245211	-0.7944695	-0.0000058	-0.0000087	0.0000055
	-0.0168186	-0.0381934	-1.0116012	0.0000637	-0.0000094	0.0000038
115	-0.0113541	-0.0207950	-0.5873765	-0.0000104	-0.0029660	0.0000396
	-0.0251453	-0.0342381	-0.8057977	0.0000594	-0.0029437	0.0000429
116	-0.0009603	-0.0140996	-0.3700061	-0.0013389	0.0012740	0.0000564
	-0.0407939	-0.0266993	-0.5980249	0.0012529	0.0013205	0.0000624

117	0.0053851	-0.0031087	-0.4051882	-0.0026627	-0.0010780	0.0001095
	-0.0480184	-0.0147640	-0.6388338	0.0024507	-0.0010309	0.0001185
118	-0.0389637	0.0077284	-0.3921076	0.0008669	0.0010097	0.0000148
	0.0118149	0.0038579	-0.6256315	-0.0008649	0.0009639	0.0001365
119	-0.0330714	0.0078653	-0.3393504	0.0004227	-0.0014711	0.0000019
	0.0041151	0.0134812	-0.5673886	-0.0004633	-0.0015168	0.0000603
120	-0.0234408	0.0138099	-0.5509154	-0.0000156	0.0031084	0.0000068
	-0.0105341	0.0300758	-0.7693924	-0.0000664	0.0030859	0.0000284
121	-0.0190187	0.0123533	-0.7674349	-0.0000097	-0.0000084	-0.0000031
	-0.0182214	0.0302961	-0.9845821	-0.0000713	-0.0000080	0.0000086
122	-0.0145573	0.0128347	-0.5487530	-0.0000038	-0.0031294	-0.0000187
	-0.0258551	0.0319755	-0.7673254	-0.0000761	-0.0031060	-0.0000152
123	-0.0042614	0.0035917	-0.3291928	0.0013413	0.0014252	-0.0000586
	-0.0411426	0.0221205	-0.5574957	-0.0012788	0.0014715	-0.0000629
124	0.0020906	-0.0076561	-0.3759525	0.0026804	-0.0010629	-0.0001115
	-0.0483048	0.0100479	-0.6098082	-0.0024765	-0.0010166	-0.0001186

SPOSTAMENTI NODI

CASO DI CARICO : 9 C.5 + SX

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 12 Sisma X ++ 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c012 +1.00*c005.001
 2) -1.00*c012 +1.00*c005.001

Coefficiente moltiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	0.8120913	-0.0286500	-0.2043676	0.0000896	0.0010772	0.0000109
	-0.8392477	0.0124961	-0.2636707	-0.0000450	-0.0010680	-0.0000117
31	0.8930088	-0.0208655	-0.2347660	0.0000231	0.0010550	-0.0000118
	-0.9140193	0.0134096	-0.3000437	-0.0000708	-0.0010259	0.0000125
32	0.8873444	-0.0261997	-0.2512566	0.0001158	0.0028841	0.0000999
	-0.7974652	0.0146205	-0.2690303	-0.0000783	0.0024572	0.0000312
37	0.8902221	-0.0356928	-0.3360424	0.0000623	0.0010722	0.0000007
	-0.9155343	-0.0233581	-0.4333183	0.0000135	0.0006673	-0.0000593
39	0.8800821	-0.0164971	-0.4674500	-0.0000068	-0.0007558	0.0000460
	-0.9197193	-0.0310428	-0.2913978	0.0000468	-0.0010430	-0.0000070
42	0.8794785	0.0217384	-0.2804082	-0.0001849	0.0010472	-0.0000118
	-0.9218293	-0.0120488	-0.2153060	-0.0001530	-0.0011636	0.0000110
69	0.7999544	0.0103002	-0.2411228	0.0000498	0.0009627	0.0000115
	-0.8459086	-0.0355017	-0.1818272	0.0002954	-0.0010727	-0.0000108
75	0.8094082	0.0079683	-0.2856266	-0.0000325	0.0010622	0.0000917
	-0.8407129	0.0242093	-0.3749775	-0.0000507	0.0006903	0.0000244
77	0.8006477	0.0262584	-0.4056236	-0.0000508	-0.0007770	-0.0000009
	-0.8438426	0.0079698	-0.2444933	-0.0000280	-0.0010419	-0.0000796
78	0.9349329	-0.0225796	-0.2545433	0.0000567	0.0028920	-0.0000272
	-0.8431112	0.0121427	-0.2718903	-0.0000454	0.0024494	-0.0000877
79	0.8068407	0.0129371	-0.2438290	-0.0000114	-0.0024989	0.0000849
	-0.9705922	-0.0220690	-0.2269193	0.0000434	-0.0029363	0.0000321
80	0.9268931	-0.0252811	-0.2687433	0.0001109	0.0029127	0.0000241
	-0.8227027	0.0111258	-0.2753679	-0.0000274	0.0024951	-0.0000381
81	0.7863734	0.0126942	-0.2458642	-0.0000070	-0.0025450	0.0000386
	-0.9635998	-0.0254853	-0.2387925	0.0001074	-0.0029619	-0.0000224
82	0.9112265	-0.0224495	-0.2684187	0.0000489	0.0029119	0.0000415
	-0.8073081	0.0165904	-0.2786340	-0.0001213	0.0024973	-0.0000253
83	0.7705232	0.0184906	-0.2488499	-0.0001194	-0.0025475	0.0000275
	-0.9483843	-0.0229036	-0.2384776	0.0000597	-0.0029614	-0.0000405
84	0.7588276	0.0183673	-0.2408290	-0.0001094	-0.0025126	-0.0000160
	-0.9254208	-0.0262305	-0.2237479	0.0001146	-0.0029239	-0.0000919

85	0.8547475	0.0007232	-1.0196960	-0.0000106	0.0018238	0.0000690
	-0.8301325	0.0209657	-0.9840919	-0.0000709	0.0018297	0.0000008
86	0.7918552	0.0210685	-0.9717210	-0.0000678	-0.0018800	0.0000053
	-0.8926141	-0.0009412	-1.0044637	0.0000168	-0.0018661	-0.0000689
87	0.8767022	-0.0099571	-1.0436793	-0.0000121	0.0018381	0.0000418
	-0.8421177	0.0090740	-1.0050770	-0.0000701	0.0018608	-0.0000246
88	0.8051852	0.0103522	-0.9902393	-0.0000708	-0.0019104	0.0000264
	-0.9139203	-0.0106762	-1.0286616	-0.0000049	-0.0018880	-0.0000412
89	0.8924469	-0.0180557	-1.0434646	0.0000801	0.0018344	0.0000240
	-0.8574353	-0.0003727	-1.0020233	0.0000219	0.0018637	-0.0000388
90	0.8210555	0.0010352	-0.9873968	0.0000364	-0.0019132	0.0000393
	-0.9291144	-0.0187879	-1.0283562	0.0000718	-0.0018841	-0.0000222
91	0.9021927	-0.0281317	-1.0234375	0.0000777	0.0018208	-0.0000008
	-0.8759512	-0.0116235	-0.9863146	0.0000252	0.0018318	-0.0000618
92	0.8398015	-0.0100715	-0.9728886	0.0000494	-0.0018798	0.0000600
	-0.9378822	-0.0290046	-1.0091246	0.0000606	-0.0018655	0.0000048
93	0.8233883	0.0146469	-1.2749790	-0.0000087	-0.0000994	0.0000323
	-0.8613180	0.0142959	-1.2729447	0.0000031	0.0000535	-0.0000377
94	0.8409197	0.0018102	-1.2998909	-0.0000459	-0.0001089	0.0000337
	-0.8781097	0.0009346	-1.2998258	-0.0000423	0.0000591	-0.0000329
95	0.8567924	-0.0100998	-1.2982859	0.0000624	-0.0001137	0.0000319
	-0.8932965	-0.0112999	-1.2980683	0.0000513	0.0000642	-0.0000308
96	0.8709268	-0.0226143	-1.2771833	0.0000333	-0.0001048	0.0000303
	-0.9070552	-0.0243099	-1.2764843	0.0000123	0.0000586	-0.0000292
111	0.8929513	-0.0310758	-0.4851729	0.0000361	0.0008860	-0.0000429
	-0.9139178	-0.0041222	-0.5873506	-0.0000427	0.0011369	-0.0001032
112	0.8917173	-0.0326864	-0.4336680	0.0000492	-0.0013377	-0.0000183
	-0.9147358	-0.0129574	-0.5530703	-0.0000146	-0.0013328	-0.0000796
113	0.8879142	-0.0323322	-0.6820667	0.0000450	0.0032461	0.0000244
	-0.9168599	-0.0270375	-0.7156719	0.0000218	0.0026216	-0.0000350
114	0.8854907	-0.0304331	-0.9262610	0.0000277	0.0003300	0.0000331
	-0.9179716	-0.0322814	-0.8798097	0.0000301	-0.0003481	-0.0000239
115	0.8826661	-0.0233779	-0.7580752	0.0000105	-0.0026720	0.0000672
	-0.9191655	-0.0316552	-0.6350990	0.0000385	-0.0032377	0.0000153
116	0.8794484	-0.0098766	-0.5733190	-0.0000662	0.0011937	0.0000870
	-0.9212026	-0.0309223	-0.3947120	-0.0000198	0.0014007	0.0000318
117	0.8792563	0.0048739	-0.5888690	-0.0001255	-0.0013062	0.0001406
	-0.9218897	-0.0227466	-0.4551530	-0.0000864	-0.0008027	0.0000874
118	0.8120147	-0.0106571	-0.4621165	0.0000489	0.0008704	0.0001103
	-0.8391635	0.0222434	-0.5556225	-0.0000469	0.0011032	0.0000410
119	0.8109082	-0.0015910	-0.3985852	0.0000082	-0.0014969	0.0000661
	-0.8398645	0.0229376	-0.5081539	-0.0000488	-0.0014909	-0.0000039
120	0.8076124	0.0178651	-0.6446590	-0.0000371	0.0033831	0.0000526
	-0.8415873	0.0260206	-0.6756488	-0.0000450	0.0028112	-0.0000174
121	0.8053595	0.0215590	-0.8971629	-0.0000417	0.0003023	0.0000380
	-0.8425995	0.0210904	-0.8548540	-0.0000393	-0.0003186	-0.0000325
122	0.8029978	0.0268476	-0.7142382	-0.0000463	-0.0028585	0.0000201
	-0.8434103	0.0179626	-0.6018402	-0.0000337	-0.0033769	-0.0000540
123	0.7999350	0.0265641	-0.5251223	-0.0000173	0.0013535	-0.0000235
	-0.8453390	-0.0008520	-0.3615663	0.0000798	0.0015433	-0.0000980
124	0.7997520	0.0194026	-0.5540489	0.0000163	-0.0012710	-0.0000768
	-0.8459663	-0.0170108	-0.4317119	0.0001876	-0.0008085	-0.0001533

SPOSTAMENTI NODI

CASO DI CARICO : 10 C.5 + Sy

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 13 σ_{sima_Y} +- 1.00
 N. 1 CASI DI CARICO

5 C.4 + Accid. 1.00

- 1) +1.00*c013 +1.00*c005.001
- 2) -1.00*c013 +1.00*c005.001

Coefficiente multiplicativo: 1.000000

Nodo	SX	SY	SZ	RX	RY	RZ
26	-0.0009881 -0.0261683	1.2296817 -1.2458356	-0.2308720 -0.2371664	-0.0031668 0.0032113	0.0000201 -0.0000109	0.0000014 -0.0000022
31	-0.0233537 0.0023432	1.2344866 -1.2419425	-0.2707603 -0.2640494	-0.0042808 0.0042331	-0.0000053 0.0000344	0.0000033 -0.0000025
32	0.0524127 0.0374665	1.2305194 -1.2420986	-0.2822511 -0.2380359	-0.0046142 0.0046518	0.0026810 0.0026603	0.0000590 0.0000721
37	-0.0255995 0.0002873	1.2057494 -1.2648003	-0.3868804 -0.3824802	-0.0018009 0.0018766	0.0008642 0.0008753	-0.0000384 -0.0000202
39	-0.0332130 -0.0064242	1.2063447 -1.2538846	-0.3796939 -0.3791539	-0.0018056 0.0018456	-0.0008988 -0.0009001	0.0000076 0.0000314
42	-0.0346354 -0.0077153	1.2303740 -1.2206844	-0.2504685 -0.2452457	-0.0040558 0.0037179	-0.0000769 -0.0000395	-0.0000032 0.0000024
69	-0.0096226 -0.0363315	1.2113855 -1.2365870	-0.2091714 -0.2137786	-0.0040680 0.0044132	-0.0000350 -0.0000750	-0.0000013 0.0000020
75	-0.0029269 -0.0283778	1.2506328 -1.2184552	-0.3286083 -0.3319958	-0.0024274 0.0023442	0.0008821 0.0008704	0.0000485 0.0000676
77	-0.0083653 -0.0348295	1.2461717 -1.2119435	-0.3253630 -0.3247539	-0.0024189 0.0023401	-0.0009104 -0.0009085	-0.0000535 -0.0000270
78	0.0377641 0.0540576	1.2313741 -1.2418110	-0.2474937 -0.2789399	-0.0042354 0.0042467	0.0026615 0.0026800	-0.0000636 -0.0000514
79	-0.0900480 -0.0737035	1.2192972 -1.2284292	-0.2178684 -0.2528800	-0.0038666 0.0038986	-0.0027149 -0.0027203	0.0000436 0.0000735
80	0.0490247 0.0551658	1.2286336 -1.2427889	-0.2364376 -0.3076735	-0.0043907 0.0044742	0.0026900 0.0027179	-0.0000127 -0.0000012
81	-0.0916759 -0.0855506	1.2162808 -1.2290719	-0.2046711 -0.2799855	-0.0040352 0.0041356	-0.0027439 -0.0027630	-0.0000078 0.0000240
82	0.0541221 0.0497963	1.2324496 -1.2383088	-0.3442788 -0.2027738	-0.0048668 0.0047944	0.0027176 0.0026916	0.0000032 0.0000131
83	-0.0867831 -0.0910780	1.2197188 -1.2241318	-0.3174975 -0.1698300	-0.0045443 0.0044846	-0.0027620 -0.0027468	-0.0000241 0.0000111
84	-0.0756874 -0.0909057	1.2185623 -1.2264256	-0.2555554 -0.2090215	-0.0042410 0.0042462	-0.0027232 -0.0027133	-0.0000707 -0.0000372
85	0.0197645 0.0048506	1.2450232 -1.2233344	-1.0261246 -0.9776634	-0.0045527 0.0044711	0.0018310 0.0018225	0.0000266 0.0000431
86	-0.0427834 -0.0579755	1.2373907 -1.2172634	-1.0125208 -0.9636638	-0.0043979 0.0043469	-0.0018758 -0.0018704	-0.0000465 -0.0000171
87	0.0194435 0.0151409	1.2332120 -1.2340951	-1.0981554 -0.9506009	-0.0047752 0.0046930	0.0018568 0.0018421	0.0000012 0.0000160
88	-0.0522208 -0.0565143	1.2267794 -1.2271034	-1.0847425 -0.9341583	-0.0046583 0.0045826	-0.0019015 -0.0018969	-0.0000224 0.0000076
89	0.0144485 0.0205632	1.2245897 -1.2430181	-0.9840143 -1.0614737	-0.0042743 0.0043763	0.0018419 0.0018562	-0.0000150 0.0000002
90	-0.0571215 -0.0509373	1.2183899 -1.2361426	-0.9682301 -1.0475229	-0.0041461 0.0042542	-0.0018948 -0.0019024	-0.0000055 0.0000226
91	0.0050079 0.0212336	1.2147200 -1.2544752	-0.9872129 -1.0225391	-0.0040785 0.0041814	0.0018222 0.0018304	-0.0000392 -0.0000235
92	-0.0572337 -0.0408470	1.2086517 -1.2477278	-0.9728478 -1.0091654	-0.0039453 0.0040554	-0.0018712 -0.0018741	0.0000191 0.0000458
93	-0.0114384 -0.0264913	1.2456806 -1.2167378	-1.2987991 -1.2491245	-0.0044432 0.0044375	-0.0000228 -0.0000231	-0.0000141 0.0000087
94	-0.0164469 -0.0207431	1.2321694 -1.2294246	-1.3751015 -1.2246152	-0.0047187 0.0046305	-0.0000224 -0.0000274	-0.0000108 0.0000116
95	-0.0213283 -0.0151758	1.2202976 -1.2416974	-1.2581838 -1.3381704	-0.0042042 0.0043178	-0.0000263 -0.0000233	-0.0000104 0.0000115

96	-0.0262107	1.2083115	-1.2585158	-0.0040407	-0.0000237	-0.0000101
	-0.0099177	-1.2552357	-1.2951518	0.0040862	-0.0000224	0.0000113
111	-0.0233056	1.2196543	-0.5393540	-0.0034542	0.0010090	-0.0000810
	0.0023391	-1.2548530	-0.5331695	0.0034476	0.0010139	-0.0000651
112	-0.0243756	1.2134727	-0.4961068	-0.0026275	-0.0013388	-0.0000571
	0.0013571	-1.2591165	-0.4906315	0.0026621	-0.0013316	-0.0000409
113	-0.0275309	1.2044336	-0.7003811	-0.0018021	0.0029281	-0.0000151
	-0.0014148	-1.2638033	-0.6973576	0.0018689	0.0029396	0.0000045
114	-0.0294292	1.2015486	-0.9039013	-0.0018033	-0.0000139	-0.0000062
	-0.0030517	-1.2642630	-0.9021693	0.0018611	-0.0000043	0.0000155
115	-0.0315451	1.2040068	-0.6969918	-0.0018045	-0.0029575	0.0000295
	-0.0049543	-1.2590399	-0.6961824	0.0018534	-0.0029522	0.0000530
116	-0.0343549	1.2082378	-0.4846770	-0.0025557	0.0013027	0.0000465
	-0.0073993	-1.2490367	-0.4833540	0.0024697	0.0012917	0.0000723
117	-0.0348049	1.2181161	-0.5235308	-0.0033057	-0.0010460	0.0001009
	-0.0078285	-1.2359888	-0.5204912	0.0030938	-0.0010629	0.0001270
118	-0.0010048	1.2425051	-0.5061095	-0.0029203	0.0009902	0.0000670
	-0.0261441	-1.2309188	-0.5116296	0.0029223	0.0009834	0.0000843
119	-0.0018484	1.2463391	-0.4510696	-0.0026738	-0.0014896	0.0000221
	-0.0271079	-1.2249925	-0.4556694	0.0026332	-0.0014983	0.0000401
120	-0.0041473	1.2553032	-0.6591903	-0.0024253	0.0031032	0.0000072
	-0.0298277	-1.2114175	-0.6611175	0.0023432	0.0030911	0.0000280
121	-0.0056392	1.2533614	-0.8757222	-0.0024232	-0.0000032	-0.0000087
	-0.0316009	-1.2107120	-0.8762948	0.0023422	-0.0000131	0.0000141
122	-0.0070859	1.2530218	-0.6582260	-0.0024211	-0.0031150	-0.0000294
	-0.0333265	-1.2082116	-0.6578524	0.0023411	-0.0031203	-0.0000045
123	-0.0093545	1.2402881	-0.4431984	-0.0029686	0.0014422	-0.0000750
	-0.0360495	-1.2145759	-0.4434901	0.0030311	0.0014546	-0.0000466
124	-0.0097326	1.2268699	-0.4917813	-0.0035183	-0.0010490	-0.0001296
	-0.0364816	-1.2244781	-0.4939794	0.0037222	-0.0010304	-0.0001005

SOLLECITAZIONI ASTE:

SOLLECITAZIONI ASTE BARRE DYWIDAG

CASO DI CARICO : 1 P.P.+ Perm.

COMBINAZIONE

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio_____	+	1.00
2	Peso_copertura_____	+	1.00
6	Permanente_Tomp_____	+	1.00
7	Perm._in_Copertura_	+	1.00

1) +1.00*c001 +1.00*c002 +1.00*c006 +1.00*c007

Asta	188	190	191	193	194	196	197	199	200	201	204	205	207
PROGR.	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM	NORM
0.0	10292.71	10292.71	10265.85	10265.84	10265.89	10265.91	10290.42	10290.39	10327.16	10327.16	10300.28	10300.27	10300.27
150.7	10292.71	10292.71	10265.85	10265.84	10265.89	10265.91	10290.42	10290.39	10327.16	10327.16	10300.28	10300.27	10300.27
301.5	10292.71	10292.71	10265.85	10265.84	10265.89	10265.91	10290.42	10290.39	10327.16	10327.16	10300.28	10300.27	10300.27
nodi	78	79	80	100	82	101	32	104	97	105	99	108	102
TYT	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ	TZZ
0.82	-0.07	0.07	0.82	0.00	0.82	-0.01	0.82	-0.82	0.33	-0.33	0.33	0.01	0.01
0.82	-0.07	0.07	0.82	0.00	0.82	-0.01	0.82	-0.82	0.33	-0.33	0.33	0.01	0.01
0.82	-0.07	0.07	0.82	0.00	0.82	-0.01	0.82	-0.82	0.33	-0.33	0.33	0.01	0.01
TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS	TORS
1.69	1.69	-1.75	0.24	-0.30	-0.29	0.23	-1.88	1.67	0.61	-0.76	0.10	-0.24	-0.24
1.69	1.69	-1.75	0.24	-0.30	-0.29	0.23	-1.88	1.67	0.61	-0.76	0.10	-0.24	-0.24
1.69	1.69	-1.75	0.24	-0.30	-0.29	0.23	-1.88	1.67	0.61	-0.76	0.10	-0.24	-0.24
MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT	MYT
0.00	0.00	20.38	0.00	1.30	0.00	-2.50	0.00	-17.67	22.87	13.76	3.10	3.44	3.44
0.00	0.00	20.38	0.00	1.30	0.00	-2.50	0.00	-17.67	22.87	13.76	3.10	3.44	3.44
0.00	0.00	20.38	0.00	1.30	0.00	-2.50	0.00	-17.67	22.87	13.76	3.10	3.44	3.44
MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT	MZT
0.00	123.29	246.61	0.00	123.49	0.00	123.51	123.26	246.60	246.58	345.11	247.00	345.52	246.99
0.00	123.29	246.61	0.00	123.49	0.00	123.51	123.26	246.60	246.58	345.11	247.00	345.52	246.99
0.00	123.29	246.61	0.00	123.49	0.00	123.51	123.26	246.60	246.58	345.11	247.00	345.52	246.99

PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	10300.33	0.33	0.01	-0.23	-1.63	247.01
150.2	10300.33	0.33	0.01	-0.23	-2.53	296.27
300.4	10300.33	0.33	0.01	-0.23	-3.42	345.53
Asta	208	nodt	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	10300.33	-0.33	0.00	0.12	-3.42	345.53
150.2	10300.33	-0.33	0.00	0.12	-3.06	296.27
300.4	10300.33	-0.33	0.00	0.12	-2.71	247.01
Asta	210	nodt	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	10324.84	0.33	-0.04	-0.62	-26.75	246.52
150.2	10324.84	0.33	-0.04	-0.62	-20.59	295.81
300.4	10324.84	0.33	-0.04	-0.62	-14.43	345.10
Asta	211	nodt	110	104		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	10324.84	-0.33	0.01	0.82	-14.35	345.10
150.2	10324.84	-0.33	0.01	0.82	-16.35	295.85
300.4	10324.84	-0.33	0.01	0.82	-18.34	246.60

SOLLECITAZIONI ASTE

CASO DI CARICO : 2 P.P.+Perm.(no masset COMBINAZIONE

N. 3 CONDIZIONI ANALISI STATICA

1	Peso_proprio	+	1.00
2	Peso_copertura	+	1.00
6	Permanente_Tomp	+	1.00

1) +1.00*c001 +1.00*c002 +1.00*c006

Asta	188	nodt	78	97		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6677.19	0.53	-0.05	1.09	0.00	0.00
150.7	6677.19	0.53	-0.05	1.09	7.27	80.01
301.5	6677.19	0.53	-0.05	1.09	14.55	160.01
Asta	190	nodt	98	79		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6677.19	-0.53	0.04	-1.14	13.01	160.04
150.7	6677.19	-0.53	0.04	-1.14	6.50	80.02
301.5	6677.19	-0.53	0.04	-1.14	0.00	0.00
Asta	191	nodt	80	99		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6659.31	0.53	-0.01	0.15	0.00	0.00
150.7	6659.31	0.53	-0.01	0.15	1.03	80.14
301.5	6659.31	0.53	-0.01	0.15	2.05	160.27
Asta	193	nodt	100	81		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6659.31	-0.53	0.00	-0.20	0.68	160.26
150.7	6659.31	-0.53	0.00	-0.20	0.34	80.13
301.5	6659.31	-0.53	0.00	-0.20	0.00	0.00
Asta	194	nodt	82	102		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6659.53	0.53	0.00	-0.19	0.00	0.00
150.7	6659.53	0.53	0.00	-0.19	-0.39	80.14
301.5	6659.53	0.53	0.00	-0.19	-0.78	160.29
Asta	196	nodt	101	83		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6659.54	-0.53	-0.01	0.14	-1.77	160.29
150.7	6659.54	-0.53	-0.01	0.14	-0.89	80.15
301.5	6659.54	-0.53	-0.01	0.14	0.00	0.00
Asta	197	nodt	32	103		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6675.38	0.53	0.06	-1.22	0.00	0.00
150.7	6675.38	0.53	0.06	-1.22	-8.36	79.98
301.5	6675.38	0.53	0.06	-1.22	-16.71	159.96
Asta	199	nodt	104	84		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6675.37	-0.53	-0.04	1.07	-11.58	160.03
150.7	6675.37	-0.53	-0.04	1.07	-5.79	80.02
301.5	6675.37	-0.53	-0.04	1.07	0.00	0.00
Asta	200	nodt	97	105		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	6699.52	0.21	0.02	0.38	15.00	160.01

150.2	6699.52	0.21	0.02	0.38	11.96	191.90
300.4	6699.52	0.21	0.02	0.38	8.91	223.79
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6699.52	-0.21	-0.02	-0.51	8.91	223.79
150.2	6699.52	-0.21	-0.02	-0.51	11.17	191.92
300.4	6699.52	-0.21	-0.02	-0.51	13.42	160.04
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6681.63	0.21	0.00	0.05	2.20	160.27
150.2	6681.63	0.21	0.00	0.05	2.21	192.16
300.4	6681.63	0.21	0.00	0.05	2.23	224.05
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6681.63	-0.21	0.00	-0.17	2.23	224.05
150.2	6681.63	-0.21	0.00	-0.17	1.51	192.16
300.4	6681.63	-0.21	0.00	-0.17	0.78	160.26
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6681.85	0.21	0.00	-0.16	-0.89	160.29
150.2	6681.85	0.21	0.00	-0.16	-1.55	192.18
300.4	6681.85	0.21	0.00	-0.16	-2.22	224.06
Asta	208	nod	109	101		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6681.86	-0.21	0.00	0.06	-2.21	224.06
150.2	6681.86	-0.21	0.00	0.06	-2.06	192.18
300.4	6681.86	-0.21	0.00	0.06	-1.91	160.29
Asta	210	nod	103	110		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6697.70	0.21	-0.03	-0.41	-17.19	159.96
150.2	6697.70	0.21	-0.03	-0.41	-13.27	191.87
300.4	6697.70	0.21	-0.03	-0.41	-9.34	223.78
Asta	211	nod	110	104		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	6697.70	-0.21	0.01	0.52	-9.30	223.78
150.2	6697.70	-0.21	0.01	0.52	-10.66	191.91
300.4	6697.70	-0.21	0.01	0.52	-12.02	160.03

SOLLECITAZIONI ASTE

CASO DI CARICO : 3 C.2 +Pretens.

COMBINAZIONE

N. 2 CONDIZIONI ANALISI STATICA
 8 pretensione_____ + 1.00
 10 carichi_per_pretens + 1.00
 N. 1 CASI DI CARICO
 2 P.P.+Perm.(no masset 1.00

1) +1.00*c008 +1.00*c010 +1.00*c002.001

Asta	188	nod	78	97		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52690.24	0.11	-0.58	13.93	0.00	0.00
150.7	52690.24	0.11	-0.58	13.93	88.11	16.00
301.5	52690.24	0.11	-0.58	13.93	176.22	31.99
Asta	190	nod	98	79		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52690.23	-0.11	0.57	-14.08	171.00	32.03
150.7	52690.23	-0.11	0.57	-14.08	85.50	16.01
301.5	52690.23	-0.11	0.57	-14.08	0.00	0.00
Asta	191	nod	80	99		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52407.70	0.11	-0.06	2.10	0.00	0.00
150.7	52407.70	0.11	-0.06	2.10	9.40	16.57
301.5	52407.70	0.11	-0.06	2.10	18.80	33.14
Asta	193	nod	100	81		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52407.70	-0.11	0.05	-2.24	15.16	33.14
150.7	52407.70	-0.11	0.05	-2.24	7.58	16.57
301.5	52407.70	-0.11	0.05	-2.24	0.00	0.00
Asta	194	nod	82	102		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52404.16	0.11	0.05	-2.22	0.00	0.00
150.7	52404.16	0.11	0.05	-2.22	-8.24	16.59
301.5	52404.16	0.11	0.05	-2.22	-16.47	33.17

Asta	196	nod	101	83		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52404.31	-0.11	-0.05	2.04	-15.91	33.18
150.7	52404.31	-0.11	-0.05	2.04	-7.96	16.59
301.5	52404.31	-0.11	-0.05	2.04	0.00	0.00
Asta	197	nod	32	103		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52679.63	0.11	0.72	-15.21	0.00	0.00
150.7	52679.63	0.11	0.72	-15.21	-108.36	15.99
301.5	52679.63	0.11	0.72	-15.21	-216.72	31.97
Asta	199	nod	104	84		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52679.27	-0.11	-0.46	13.74	-139.63	32.06
150.7	52679.27	-0.11	-0.46	13.74	-69.82	16.03
301.5	52679.27	-0.11	-0.46	13.74	0.00	0.00
Asta	200	nod	97	105		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52489.14	-0.40	0.23	5.41	181.77	31.99
150.2	52489.14	-0.40	0.23	5.41	147.01	-28.47
300.4	52489.14	-0.40	0.23	5.41	112.26	-88.93
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52489.17	0.40	-0.21	-5.82	112.26	-88.93
150.2	52489.17	0.40	-0.21	-5.82	144.34	-28.45
300.4	52489.17	0.40	-0.21	-5.82	176.42	32.03
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52206.42	-0.40	-0.03	1.24	20.42	33.14
150.2	52206.42	-0.40	-0.03	1.24	24.19	-26.77
300.4	52206.42	-0.40	-0.03	1.24	27.97	-86.69
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52206.41	0.40	0.04	-1.55	27.98	-86.69
150.2	52206.41	0.40	0.04	-1.55	22.33	-26.77
300.4	52206.41	0.40	0.04	-1.55	16.68	33.14
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52202.94	-0.40	0.03	-1.47	-18.02	33.17
150.2	52202.94	-0.40	0.03	-1.47	-22.99	-26.74
300.4	52202.94	-0.40	0.03	-1.47	-27.96	-86.65
Asta	208	nod	109	101		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52202.97	0.40	-0.03	1.32	-27.93	-86.65
150.2	52202.97	0.40	-0.03	1.32	-22.72	-26.73
300.4	52202.97	0.40	-0.03	1.32	-17.51	33.18
Asta	210	nod	103	110		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52478.28	-0.40	-0.35	-4.71	-222.90	31.97
150.2	52478.28	-0.40	-0.35	-4.71	-170.29	-28.45
300.4	52478.28	-0.40	-0.35	-4.71	-117.68	-88.87
Asta	211	nod	110	104		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	52478.21	0.40	0.09	7.03	-117.09	-88.87
150.2	52478.21	0.40	0.09	7.03	-131.02	-28.40
300.4	52478.21	0.40	0.09	7.03	-144.96	32.06

SOLLECITAZIONI ASTE

CASO DI CARICO : 4 C.3+Nuovo Massetto COMBINAZIONE

- N. 1 CONDIZIONI ANALISI STATICA
 11 Nuovo_massetto_all. + 1.00
 N. 1 CASI DI CARICO
 3 C.2 +Pretens. 1.00

1) +1.00*c011 +1.00*c003.001

Asta	188	nod	78	97		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	54256.96	0.23	-0.60	14.19	0.00	0.00
150.7	54256.96	0.23	-0.60	14.19	89.76	34.75
301.5	54256.96	0.23	-0.60	14.19	179.52	69.50
Asta	190	nod	98	79		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ

0.0	54256.95	-0.23	0.58	-14.35	174.20	69.54
150.7	54256.95	-0.23	0.58	-14.35	87.10	34.77
301.5	54256.95	-0.23	0.58	-14.35	0.00	0.00
Asta	191	nodj	80	99		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53970.53	0.23	-0.06	2.14	0.00	0.00
150.7	53970.53	0.23	-0.06	2.14	9.58	35.36
301.5	53970.53	0.23	-0.06	2.14	19.16	70.72
Asta	193	nodj	100	81		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53970.53	-0.23	0.05	-2.28	15.43	70.72
150.7	53970.53	-0.23	0.05	-2.28	7.72	35.36
301.5	53970.53	-0.23	0.05	-2.28	0.00	0.00
Asta	194	nodj	82	102		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53966.92	0.23	0.06	-2.26	0.00	0.00
150.7	53966.92	0.23	0.06	-2.26	-8.38	35.38
301.5	53966.92	0.23	0.06	-2.26	-16.77	70.75
Asta	196	nodj	101	83		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53967.07	-0.23	-0.05	2.08	-16.23	70.76
150.7	53967.07	-0.23	-0.05	2.08	-8.11	35.38
301.5	53967.07	-0.23	-0.05	2.08	0.00	0.00
Asta	197	nodj	32	103		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54246.14	0.23	0.73	-15.50	0.00	0.00
150.7	54246.14	0.23	0.73	-15.50	-110.37	34.74
301.5	54246.14	0.23	0.73	-15.50	-220.75	69.48
Asta	199	nodj	104	84		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54245.77	-0.23	-0.47	14.00	-142.27	69.57
150.7	54245.77	-0.23	-0.47	14.00	-71.13	34.79
301.5	54245.77	-0.23	-0.47	14.00	0.00	0.00
Asta	200	nodj	97	105		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54061.11	-0.35	0.24	5.51	185.18	69.50
150.2	54061.11	-0.35	0.24	5.51	149.77	16.57
300.4	54061.11	-0.35	0.24	5.51	114.36	-36.36
Asta	201	nodj	105	98		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54061.14	0.35	-0.22	-5.92	114.37	-36.36
150.2	54061.14	0.35	-0.22	-5.92	147.04	16.59
300.4	54061.14	0.35	-0.22	-5.92	179.71	69.54
Asta	204	nodj	99	108		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53774.50	-0.35	-0.03	1.26	20.81	70.72
150.2	53774.50	-0.35	-0.03	1.26	24.65	18.34
300.4	53774.50	-0.35	-0.03	1.26	28.49	-34.05
Asta	205	nodj	108	100		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53774.49	0.35	0.04	-1.59	28.50	-34.05
150.2	53774.49	0.35	0.04	-1.59	22.74	18.33
300.4	53774.49	0.35	0.04	-1.59	16.97	70.72
Asta	207	nodj	102	109		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53770.94	-0.35	0.03	-1.50	-18.34	70.75
150.2	53770.94	-0.35	0.03	-1.50	-23.41	18.37
300.4	53770.94	-0.35	0.03	-1.50	-28.49	-34.01
Asta	208	nodj	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	53770.98	0.35	-0.04	1.34	-28.45	-34.01
150.2	53770.98	0.35	-0.04	1.34	-23.15	18.37
300.4	53770.98	0.35	-0.04	1.34	-17.85	70.76
Asta	210	nodj	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54050.04	-0.35	-0.36	-4.80	-227.05	69.48
150.2	54050.04	-0.35	-0.36	-4.80	-173.46	16.59
300.4	54050.04	-0.35	-0.36	-4.80	-119.88	-36.30
Asta	211	nodj	110	104		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	54049.97	0.35	0.09	7.16	-119.28	-36.30
150.2	54049.97	0.35	0.09	7.16	-133.49	16.64
300.4	54049.97	0.35	0.09	7.16	-147.70	69.57

SOLLECITAZIONI ASTE

CASO DI CARICO : 5 C.4 + Accid.

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 3 Carichi_accid_cop_ + 1.00
 N. 1 CASI DI CARICO
 4 C.3+Nuovo Massetto 1.00

1) +1.00*c003 +1.00*c004.001

Asta	188	nod	78	97		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57872.49	0.52	-0.62	14.79	0.00	0.00
150.7	57872.49	0.52	-0.62	14.79	93.57	78.04
301.5	57872.49	0.52	-0.62	14.79	187.15	156.07
Asta	190	nod	98	79		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57872.47	-0.52	0.60	-14.96	181.57	156.11
150.7	57872.47	-0.52	0.60	-14.96	90.78	78.05
301.5	57872.47	-0.52	0.60	-14.96	0.00	0.00
Asta	191	nod	80	99		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57577.07	0.52	-0.07	2.23	0.00	0.00
150.7	57577.07	0.52	-0.07	2.23	10.00	78.72
301.5	57577.07	0.52	-0.07	2.23	20.00	157.45
Asta	193	nod	100	81		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57577.07	-0.52	0.05	-2.38	16.06	157.44
150.7	57577.07	-0.52	0.05	-2.38	8.03	78.72
301.5	57577.07	-0.52	0.05	-2.38	0.00	0.00
Asta	194	nod	82	102		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57573.28	0.52	0.06	-2.36	0.00	0.00
150.7	57573.28	0.52	0.06	-2.36	-8.72	78.74
301.5	57573.28	0.52	0.06	-2.36	-17.44	157.48
Asta	196	nod	101	83		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57573.44	-0.52	-0.06	2.16	-16.95	157.48
150.7	57573.44	-0.52	-0.06	2.16	-8.48	78.74
301.5	57573.44	-0.52	-0.06	2.16	0.00	0.00
Asta	197	nod	32	103		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57861.18	0.52	0.76	-16.16	0.00	0.00
150.7	57861.18	0.52	0.76	-16.16	-115.02	78.02
301.5	57861.18	0.52	0.76	-16.16	-230.04	156.05
Asta	199	nod	104	84		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57860.79	-0.52	-0.49	14.59	-148.36	156.14
150.7	57860.79	-0.52	-0.49	14.59	-74.18	78.07
301.5	57860.79	-0.52	-0.49	14.59	0.00	0.00
Asta	200	nod	97	105		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57688.75	-0.24	0.25	5.74	193.04	156.07
150.2	57688.75	-0.24	0.25	5.74	156.13	120.51
300.4	57688.75	-0.24	0.25	5.74	119.21	84.96
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57688.78	0.24	-0.23	-6.18	119.22	84.96
150.2	57688.78	0.24	-0.23	-6.18	153.27	120.53
300.4	57688.78	0.24	-0.23	-6.18	187.31	156.11
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57393.15	-0.23	-0.03	1.32	21.72	157.45
150.2	57393.15	-0.23	-0.03	1.32	25.71	122.43
300.4	57393.15	-0.23	-0.03	1.32	29.70	87.42
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57393.14	0.23	0.04	-1.65	29.71	87.42
150.2	57393.14	0.23	0.04	-1.65	23.69	122.43
300.4	57393.14	0.23	0.04	-1.65	17.66	157.44
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57389.42	-0.23	0.04	-1.57	-19.08	157.48

150.2	57389.42	-0.23	0.04	-1.57	-24.39	122.47
300.4	57389.42	-0.23	0.04	-1.57	-29.70	87.46
Asta	208	nodì	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57389.46	0.23	-0.04	1.40	-29.66	87.46
150.2	57389.46	0.23	-0.04	1.40	-24.15	122.47
300.4	57389.46	0.23	-0.04	1.40	-18.65	157.48
Asta	210	nodì	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57677.18	-0.24	-0.37	-5.01	-236.60	156.05
150.2	57677.18	-0.24	-0.37	-5.01	-180.78	120.53
300.4	57677.18	-0.24	-0.37	-5.01	-124.96	85.02
Asta	211	nodì	110	104		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57677.11	0.24	0.10	7.46	-124.34	85.02
150.2	57677.11	0.24	0.10	7.46	-139.18	120.58
300.4	57677.11	0.24	0.10	7.46	-154.02	156.14

SOLLECITAZIONI ASTE

CASO DI CARICO : 6 C.5 + Vx

COMBINAZIONE

N.	1	CONDIZIONI ANALISI STATICA		
	4	Vento X	+	1.00
N.	1	CASI DI CARICO		
	5	C.4 + Accid.		1.00

1) +1.00*c004 +1.00*c005.001

Asta	188	nodì	78	97		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57751.14	0.51	-0.75	13.64	0.00	0.00
150.7	57751.14	0.51	-0.75	13.64	113.28	76.99
301.5	57751.14	0.51	-0.75	13.64	226.55	153.99
Asta	190	nodì	98	79		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57750.43	-0.50	0.46	-15.73	138.19	150.60
150.7	57750.43	-0.50	0.46	-15.73	69.09	75.30
301.5	57750.43	-0.50	0.46	-15.73	0.00	0.00
Asta	191	nodì	80	99		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57459.30	0.52	-0.15	1.47	0.00	0.00
150.7	57459.30	0.52	-0.15	1.47	22.16	77.74
301.5	57459.30	0.52	-0.15	1.47	44.33	155.47
Asta	193	nodì	100	81		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57458.44	-0.50	-0.03	-3.09	-8.72	151.78
150.7	57458.44	-0.50	-0.03	-3.09	-4.36	75.89
301.5	57458.44	-0.50	-0.03	-3.09	0.00	0.00
Asta	194	nodì	82	102		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57455.49	0.52	0.04	-2.71	0.00	0.00
150.7	57455.49	0.52	0.04	-2.71	-5.30	77.82
301.5	57455.49	0.52	0.04	-2.71	-10.61	155.64
Asta	196	nodì	101	83		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57454.71	-0.50	-0.08	1.73	-23.12	151.68
150.7	57454.71	-0.50	-0.08	1.73	-11.56	75.84
301.5	57454.71	-0.50	-0.08	1.73	0.00	0.00
Asta	197	nodì	32	103		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57766.06	0.52	0.79	-16.03	0.00	0.00
150.7	57766.06	0.52	0.79	-16.03	-119.38	77.99
301.5	57766.06	0.52	0.79	-16.03	-238.75	155.98
Asta	199	nodì	104	84		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57764.40	-0.50	-0.45	14.28	-135.35	150.47
150.7	57764.40	-0.50	-0.45	14.28	-67.68	75.24
301.5	57764.40	-0.50	-0.45	14.28	0.00	0.00
Asta	200	nodì	97	105		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57567.12	-0.24	0.39	2.69	233.37	153.99
150.2	57567.12	-0.24	0.39	2.69	175.34	118.52
300.4	57567.12	-0.24	0.39	2.69	117.31	83.06

Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57566.99	0.22	-0.08	-9.04	117.31	83.06
150.2	57566.99	0.22	-0.08	-9.04	130.06	116.83
300.4	57566.99	0.22	-0.08	-9.04	142.82	150.60
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57275.03	-0.23	0.06	-0.62	46.68	155.47
150.2	57275.03	-0.23	0.06	-0.62	37.98	120.48
300.4	57275.03	-0.23	0.06	-0.62	29.29	85.48
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57274.84	0.22	0.12	-3.55	29.35	85.48
150.2	57274.84	0.22	0.12	-3.55	10.78	118.63
300.4	57274.84	0.22	0.12	-3.55	-7.80	151.78
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57271.25	-0.23	0.06	-2.24	-11.98	155.64
150.2	57271.25	-0.23	0.06	-2.24	-20.60	120.58
300.4	57271.25	-0.23	0.06	-2.24	-29.23	85.52
Asta	208	nod	109	101		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57271.08	0.22	-0.01	0.68	-29.10	85.52
150.2	57271.08	0.22	-0.01	0.68	-27.06	118.60
300.4	57271.08	0.22	-0.01	0.68	-25.02	151.68
Asta	210	nod	103	110		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57581.57	-0.24	-0.41	-4.45	-245.35	155.98
150.2	57581.57	-0.24	-0.41	-4.45	-184.01	119.79
300.4	57581.57	-0.24	-0.41	-4.45	-122.67	83.61
Asta	211	nod	110	104		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57581.20	0.22	0.06	7.78	-121.93	83.61
150.2	57581.20	0.22	0.06	7.78	-131.33	117.04
300.4	57581.20	0.22	0.06	7.78	-140.73	150.47

SOLLECITAZIONI ASTE

CASO DI CARICO : 7 C.5 + Vy

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 5 Vento_Y + 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c005 +1.00*c005.001

Asta	188	nod	78	97		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57873.74	0.52	-0.65	14.08	0.00	0.00
150.7	57873.74	0.52	-0.65	14.08	97.24	77.98
301.5	57873.74	0.52	-0.65	14.08	194.47	155.96
Asta	190	nod	98	79		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57873.76	-0.52	0.55	-15.05	166.78	156.09
150.7	57873.76	-0.52	0.55	-15.05	83.39	78.04
301.5	57873.76	-0.52	0.55	-15.05	0.00	0.00
Asta	191	nod	80	99		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57575.04	0.52	-0.11	1.44	0.00	0.00
150.7	57575.04	0.52	-0.11	1.44	16.03	78.65
301.5	57575.04	0.52	-0.11	1.44	32.06	157.29
Asta	193	nod	100	81		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57575.06	-0.52	-0.01	-2.65	-1.92	157.32
150.7	57575.06	-0.52	-0.01	-2.65	-0.96	78.66
301.5	57575.06	-0.52	-0.01	-2.65	0.00	0.00
Asta	194	nod	82	102		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57577.57	0.52	0.02	-3.28	0.00	0.00
150.7	57577.57	0.52	0.02	-3.28	-2.38	78.80
301.5	57577.57	0.52	0.02	-3.28	-4.76	157.60
Asta	196	nod	101	83		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57577.74	-0.52	-0.12	1.91	-37.47	157.60

150.7	57577.74	-0.52	-0.12	1.91	-18.74	78.80
301.5	57577.74	-0.52	-0.12	1.91	0.00	0.00
Asta	197	nod	32	103		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57864.67	0.52	0.70	-17.22	0.00	0.00
150.7	57864.67	0.52	0.70	-17.22	-105.94	78.09
301.5	57864.67	0.52	0.70	-17.22	-211.89	156.18
Asta	199	nod	104	84		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57864.27	-0.52	-0.58	14.13	-173.61	156.19
150.7	57864.27	-0.52	-0.58	14.13	-86.81	78.09
301.5	57864.27	-0.52	-0.58	14.13	0.00	0.00
Asta	200	nod	97	105		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57690.00	-0.24	0.28	4.68	200.56	155.96
150.2	57690.00	-0.24	0.28	4.68	158.59	120.43
300.4	57690.00	-0.24	0.28	4.68	116.62	84.91
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57690.04	0.24	-0.18	-6.98	116.67	84.91
150.2	57690.04	0.24	-0.18	-6.98	144.38	120.50
300.4	57690.04	0.24	-0.18	-6.98	172.08	156.09
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57391.11	-0.23	0.02	-0.06	34.09	157.29
150.2	57391.11	-0.23	0.02	-0.06	30.66	122.31
300.4	57391.11	-0.23	0.02	-0.06	27.24	87.33
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57391.11	0.23	0.09	-2.78	27.31	87.33
150.2	57391.11	0.23	0.09	-2.78	13.22	122.33
300.4	57391.11	0.23	0.09	-2.78	-0.87	157.32
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57393.71	-0.23	0.09	-3.09	-6.07	157.60
150.2	57393.71	-0.23	0.09	-3.09	-19.32	122.56
300.4	57393.71	-0.23	0.09	-3.09	-32.57	87.52
Asta	208	nod	109	101		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57393.75	0.23	0.02	0.16	-32.47	87.52
150.2	57393.75	0.23	0.02	0.16	-36.13	122.56
300.4	57393.75	0.23	0.02	0.16	-39.78	157.60
Asta	210	nod	103	110		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57680.68	-0.24	-0.30	-6.95	-217.97	156.18
150.2	57680.68	-0.24	-0.30	-6.95	-172.80	120.62
300.4	57680.68	-0.24	-0.30	-6.95	-127.63	85.06
Asta	211	nod	110	104		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57680.60	0.24	0.18	5.78	-126.91	85.06
150.2	57680.60	0.24	0.18	5.78	-153.47	120.62
300.4	57680.60	0.24	0.18	5.78	-180.03	156.19

SOLLECITAZIONI ASTE

CASO DI CARICO : 8 C.5 + Dt

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 9 Carico_Termico +- 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c009 +1.00*c005.001
 2) -1.00*c009 +1.00*c005.001

Asta	188	nod	78	97		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59487.61	0.50	-0.56	13.19	0.00	0.00
	56257.36	0.54	-0.68	16.40	0.00	0.00
150.7	59487.61	0.50	-0.56	13.19	85.12	75.20
	56257.36	0.54	-0.68	16.40	102.03	80.87
301.5	59487.61	0.50	-0.56	13.19	170.24	150.40
	56257.36	0.54	-0.68	16.40	204.06	161.74
Asta	190	nod	98	79		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ

0.0	59487.55	-0.50	0.53	-13.17	158.39	150.43
	56257.40	-0.54	0.68	-16.74	204.74	161.78
150.7	59487.55	-0.50	0.53	-13.17	79.20	75.22
	56257.40	-0.54	0.68	-16.74	102.37	80.89
301.5	59487.55	-0.50	0.53	-13.17	0.00	0.00
	56257.40	-0.54	0.68	-16.74	0.00	0.00
Asta	191	nod	80	99		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59201.66	0.50	-0.02	2.16	0.00	0.00
	55952.48	0.54	-0.11	2.30	0.00	0.00
150.7	59201.66	0.50	-0.02	2.16	3.40	75.84
	55952.48	0.54	-0.11	2.30	16.60	81.61
301.5	59201.66	0.50	-0.02	2.16	6.80	151.68
	55952.48	0.54	-0.11	2.30	33.20	163.22
Asta	193	nod	100	81		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59201.64	-0.50	0.07	-1.53	19.75	151.71
	55952.50	-0.54	0.04	-3.23	12.37	163.18
150.7	59201.64	-0.50	0.07	-1.53	9.87	75.85
	55952.50	-0.54	0.04	-3.23	6.18	81.59
301.5	59201.64	-0.50	0.07	-1.53	0.00	0.00
	55952.50	-0.54	0.04	-3.23	0.00	0.00
Asta	194	nod	82	102		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59187.80	0.50	0.14	-1.12	0.00	0.00
	55958.77	0.54	-0.03	-3.60	0.00	0.00
150.7	59187.80	0.50	0.14	-1.12	-21.55	75.86
	55958.77	0.54	-0.03	-3.60	4.12	81.61
301.5	59187.80	0.50	0.14	-1.12	-43.11	151.73
	55958.77	0.54	-0.03	-3.60	8.23	163.23
Asta	196	nod	101	83		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59188.12	-0.50	0.06	2.91	18.11	151.80
	55958.76	-0.54	-0.17	1.41	-52.02	163.16
150.7	59188.12	-0.50	0.06	2.91	9.06	75.90
	55958.76	-0.54	-0.17	1.41	-26.01	81.58
301.5	59188.12	-0.50	0.06	2.91	0.00	0.00
	55958.76	-0.54	-0.17	1.41	0.00	0.00
Asta	197	nod	32	103		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59501.82	0.50	1.19	-16.75	0.00	0.00
	56220.54	0.54	0.33	-15.56	0.00	0.00
150.7	59501.82	0.50	1.19	-16.75	-179.60	75.11
	56220.54	0.54	0.33	-15.56	-50.43	80.94
301.5	59501.82	0.50	1.19	-16.75	-359.21	150.22
	56220.54	0.54	0.33	-15.56	-100.87	161.87
Asta	199	nod	104	84		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59501.53	-0.50	-0.20	16.17	-59.43	150.44
	56220.05	-0.54	-0.79	13.01	-237.29	161.84
150.7	59501.53	-0.50	-0.20	16.17	-29.72	75.22
	56220.05	-0.54	-0.79	13.01	-118.64	80.92
301.5	59501.53	-0.50	-0.20	16.17	0.00	0.00
	56220.05	-0.54	-0.79	13.01	0.00	0.00
Asta	200	nod	97	105		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59295.90	-0.26	0.24	4.95	175.42	150.40
	56081.60	-0.22	0.26	6.54	210.66	161.74
150.2	59295.90	-0.26	0.24	4.95	140.02	111.58
	56081.60	-0.22	0.26	6.54	172.23	129.44
300.4	59295.90	-0.26	0.24	4.95	104.62	72.77
	56081.60	-0.22	0.26	6.54	133.81	97.15
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59295.92	0.26	-0.20	-5.51	104.57	72.77
	56081.64	0.22	-0.26	-6.84	133.87	97.15
150.2	59295.92	0.26	-0.20	-5.51	133.97	111.60
	56081.64	0.22	-0.26	-6.84	172.56	129.46
300.4	59295.92	0.26	-0.20	-5.51	163.38	150.43
	56081.64	0.22	-0.26	-6.84	211.25	161.78
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	59009.81	-0.25	-0.06	1.88	8.00	151.68
	55776.48	-0.21	0.00	0.75	35.44	163.22
150.2	59009.81	-0.25	-0.06	1.88	16.53	113.40
	55776.48	-0.21	0.00	0.75	34.89	131.46
300.4	59009.81	-0.25	-0.06	1.88	25.06	75.13
	55776.48	-0.21	0.00	0.75	34.34	99.71

Asta	205	nodì	108	100		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	59009.81	0.25	0.01	-0.62	25.00	75.13
	55776.48	0.21	0.07	-2.68	34.42	99.71
150.2	59009.81	0.25	0.01	-0.62	23.19	113.42
	55776.48	0.21	0.07	-2.68	24.18	131.44
300.4	59009.81	0.25	0.01	-0.62	21.38	151.71
	55776.48	0.21	0.07	-2.68	13.95	163.18

Asta	207	nodì	102	109		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	58996.05	-0.25	-0.05	0.89	-45.62	151.73
	55782.78	-0.21	0.12	-4.03	7.46	163.23
150.2	58996.05	-0.25	-0.05	0.89	-37.54	113.49
	55782.78	-0.21	0.12	-4.03	-11.23	131.45
300.4	58996.05	-0.25	-0.05	0.89	-29.47	75.24
	55782.78	-0.21	0.12	-4.03	-29.92	99.67

Asta	208	nodì	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	58996.14	0.25	-0.16	3.84	-29.53	75.24
	55782.77	0.21	0.08	-1.05	-29.78	99.67
150.2	58996.14	0.25	-0.16	3.84	-6.15	113.52
	55782.77	0.21	0.08	-1.05	-42.16	131.42
300.4	58996.14	0.25	-0.16	3.84	17.23	151.80
	55782.77	0.21	0.08	-1.05	-54.53	163.16

Asta	210	nodì	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	59310.07	-0.26	-0.80	0.71	-367.76	150.22
	56044.30	-0.21	0.06	-10.72	-105.45	161.87
150.2	59310.07	-0.26	-0.80	0.71	-247.40	111.43
	56044.30	-0.21	0.06	-10.72	-114.17	129.64
300.4	59310.07	-0.26	-0.80	0.71	-127.04	72.64
	56044.30	-0.21	0.06	-10.72	-122.88	97.41

Asta	211	nodì	110	104		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	59309.97	0.26	-0.21	13.34	-125.68	72.64
	56044.25	0.21	0.41	1.57	-123.00	97.41
150.2	59309.97	0.26	-0.21	13.34	-94.34	111.54
	56044.25	0.21	0.41	1.57	-184.02	129.62
300.4	59309.97	0.26	-0.21	13.34	-63.01	150.44
	56044.25	0.21	0.41	1.57	-245.04	161.84

SOLLECITAZIONI ASTE

CASO DI CARICO : 9 C.5 + SX

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 12 $\frac{\text{Sisma}_X}{\dots}$ +- 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

1) +1.00*c012 +1.00*c005.001
 2) -1.00*c012 +1.00*c005.001

Asta	188	nodì	78	97		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57870.66	0.57	-0.56	15.09	0.00	0.00
	57874.32	0.46	-0.68	14.49	0.00	0.00
150.7	57870.66	0.57	-0.56	15.09	84.41	86.17
	57874.32	0.46	-0.68	14.49	102.73	69.91
301.5	57870.66	0.57	-0.56	15.09	168.83	172.33
	57874.32	0.46	-0.68	14.49	205.46	139.81

Asta	190	nodì	98	79		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57861.71	-0.46	0.63	-13.59	188.68	139.96
	57883.23	-0.57	0.58	-16.33	174.45	172.26
150.7	57861.71	-0.46	0.63	-13.59	94.34	69.98
	57883.23	-0.57	0.58	-16.33	87.23	86.13
301.5	57861.71	-0.46	0.63	-13.59	0.00	0.00
	57883.23	-0.57	0.58	-16.33	0.00	0.00

Asta	191	nodì	80	99		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57586.78	0.58	0.03	3.29	0.00	0.00
	57567.36	0.47	-0.16	1.17	0.00	0.00
150.7	57586.78	0.58	0.03	3.29	-4.47	86.72
	57567.36	0.47	-0.16	1.17	24.46	70.73
301.5	57586.78	0.58	0.03	3.29	-8.93	173.44
	57567.36	0.47	-0.16	1.17	48.93	141.45

Asta	193	nodì	100	81		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ

0.0	57577.88	-0.47	0.14	-1.14	43.54	141.47
	57576.26	-0.58	-0.04	-3.62	-11.42	173.41
150.7	57577.88	-0.47	0.14	-1.14	21.77	70.74
	57576.26	-0.58	-0.04	-3.62	-5.71	86.71
301.5	57577.88	-0.47	0.14	-1.14	0.00	0.00
	57576.26	-0.58	-0.04	-3.62	0.00	0.00
Asta	194	nod	82	102		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57582.82	0.57	0.20	-0.80	0.00	0.00
	57563.75	0.47	-0.09	-3.92	0.00	0.00
150.7	57582.82	0.57	0.20	-0.80	-30.29	86.56
	57563.75	0.47	-0.09	-3.92	12.85	70.91
301.5	57582.82	0.57	0.20	-0.80	-60.59	173.13
	57563.75	0.47	-0.09	-3.92	25.71	141.83
Asta	196	nod	101	83		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57574.26	-0.47	0.09	3.54	27.64	141.85
	57572.62	-0.57	-0.20	0.78	-61.54	173.11
150.7	57574.26	-0.47	0.09	3.54	13.82	70.93
	57572.62	-0.57	-0.20	0.78	-30.77	86.55
301.5	57574.26	-0.47	0.09	3.54	0.00	0.00
	57572.62	-0.57	-0.20	0.78	0.00	0.00
Asta	197	nod	32	103		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57863.37	0.57	0.93	-13.97	0.00	0.00
	57858.98	0.47	0.60	-18.34	0.00	0.00
150.7	57863.37	0.57	0.93	-13.97	-140.28	85.79
	57858.98	0.47	0.60	-18.34	-89.76	70.26
301.5	57863.37	0.57	0.93	-13.97	-280.56	171.59
	57858.98	0.47	0.60	-18.34	-179.51	140.51
Asta	199	nod	104	84		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57854.56	-0.47	-0.29	15.77	-88.11	140.96
	57867.03	-0.57	-0.69	13.41	-208.61	171.32
150.7	57854.56	-0.47	-0.29	15.77	-44.05	70.48
	57867.03	-0.57	-0.69	13.41	-104.31	85.66
301.5	57854.56	-0.47	-0.29	15.77	0.00	0.00
	57867.03	-0.57	-0.69	13.41	0.00	0.00
Asta	200	nod	97	105		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57683.43	-0.29	0.20	6.91	173.95	172.33
	57694.07	-0.18	0.29	4.58	212.13	139.81
150.2	57683.43	-0.29	0.20	6.91	143.92	128.68
	57694.07	-0.18	0.29	4.58	168.33	112.35
300.4	57683.43	-0.29	0.20	6.91	113.90	85.03
	57694.07	-0.18	0.29	4.58	124.53	84.89
Asta	201	nod	105	98		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57681.50	0.18	-0.27	-4.47	113.71	85.03
	57696.07	0.29	-0.18	-7.89	124.72	84.89
150.2	57681.50	0.18	-0.27	-4.47	154.17	112.49
	57696.07	0.29	-0.18	-7.89	152.36	128.57
300.4	57681.50	0.18	-0.27	-4.47	194.63	139.96
	57696.07	0.29	-0.18	-7.89	179.99	172.26
Asta	204	nod	99	108		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57399.38	-0.29	-0.12	3.76	-8.13	173.44
	57386.91	-0.18	0.07	-1.13	51.57	141.45
150.2	57399.38	-0.29	-0.12	3.76	10.24	130.42
	57386.91	-0.18	0.07	-1.13	41.18	114.44
300.4	57399.38	-0.29	-0.12	3.76	28.61	87.40
	57386.91	-0.18	0.07	-1.13	30.78	87.44
Asta	205	nod	108	100		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57397.44	0.18	-0.06	0.91	28.45	87.40
	57388.85	0.29	0.14	-4.22	30.97	87.44
150.2	57397.44	0.18	-0.06	0.91	37.19	114.44
	57388.85	0.29	0.14	-4.22	10.18	130.43
300.4	57397.44	0.18	-0.06	0.91	45.94	141.47
	57388.85	0.29	0.14	-4.22	-10.61	173.41
Asta	207	nod	102	109		
PROGR.	NORM	TY	TZZ	TORS	MY	MZZ
0.0	57395.55	-0.29	-0.12	2.07	-63.39	173.13
	57383.28	-0.18	0.19	-5.21	25.23	141.83
150.2	57395.55	-0.29	-0.12	2.07	-45.94	130.28
	57383.28	-0.18	0.19	-5.21	-2.83	114.65
300.4	57395.55	-0.29	-0.12	2.07	-28.49	87.44
	57383.28	-0.18	0.19	-5.21	-30.90	87.48

Asta	208	nod	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57393.69	0.18	-0.19	4.92	-28.61	87.44
	57385.22	0.29	0.11	-2.13	-30.70	87.48
150.2	57393.69	0.18	-0.19	4.92	-0.69	114.65
	57385.22	0.29	0.11	-2.13	-47.62	130.29
300.4	57393.69	0.18	-0.19	4.92	27.23	141.85
	57385.22	0.29	0.11	-2.13	-64.53	173.11

Asta	210	nod	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57676.08	-0.29	-0.56	-0.38	-288.33	171.59
	57678.28	-0.19	-0.18	-9.64	-184.88	140.51
150.2	57676.08	-0.29	-0.56	-0.38	-203.87	128.37
	57678.28	-0.19	-0.18	-9.64	-157.70	112.70
300.4	57676.08	-0.29	-0.56	-0.38	-119.41	85.15
	57678.28	-0.19	-0.18	-9.64	-130.52	84.89

Asta	211	nod	110	104		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57674.16	0.19	-0.09	11.54	-118.92	85.15
	57680.06	0.29	0.29	3.38	-129.76	84.89
150.2	57674.16	0.19	-0.09	11.54	-105.45	113.05
	57680.06	0.29	0.29	3.38	-172.91	128.11
300.4	57674.16	0.19	-0.09	11.54	-91.98	140.96
	57680.06	0.29	0.29	3.38	-216.07	171.32

SOLLECITAZIONI ASTE

CASO DI CARICO : 10 C.5 + Sy

COMBINAZIONE

N. 1 CONDIZIONI ANALISI STATICA
 13 Sisma_Y +- 1.00
 N. 1 CASI DI CARICO
 5 C.4 + Accid. 1.00

- 1) +1.00*c013 +1.00*c005.001
- 2) -1.00*c013 +1.00*c005.001

Asta	188	nod	78	97		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57863.43	0.52	-0.86	10.50	0.00	0.00
	57881.54	0.52	-0.38	19.09	0.00	0.00
150.7	57863.43	0.52	-0.86	10.50	129.53	77.82
	57881.54	0.52	-0.38	19.09	57.61	78.25
301.5	57863.43	0.52	-0.86	10.50	259.06	155.65
	57881.54	0.52	-0.38	19.09	115.23	156.50

Asta	190	nod	98	79		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57863.47	-0.52	0.27	-16.91	82.33	155.97
	57881.47	-0.52	0.93	-13.00	280.81	156.25
150.7	57863.47	-0.52	0.27	-16.91	41.16	77.98
	57881.47	-0.52	0.93	-13.00	140.40	78.12
301.5	57863.47	-0.52	0.27	-16.91	0.00	0.00
	57881.47	-0.52	0.93	-13.00	0.00	0.00

Asta	191	nod	80	99		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57560.86	0.52	-0.29	-2.13	0.00	0.00
	57593.28	0.52	0.16	6.59	0.00	0.00
150.7	57560.86	0.52	-0.29	-2.13	43.93	78.43
	57593.28	0.52	0.16	6.59	-23.93	79.02
301.5	57560.86	0.52	-0.29	-2.13	87.86	156.86
	57593.28	0.52	0.16	6.59	-47.87	158.04

Asta	193	nod	100	81		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57560.91	-0.52	-0.27	-4.05	-82.74	156.93
	57593.24	-0.52	0.38	-0.71	114.85	157.96
150.7	57560.91	-0.52	-0.27	-4.05	-41.37	78.46
	57593.24	-0.52	0.38	-0.71	57.43	78.98
301.5	57560.91	-0.52	-0.27	-4.05	0.00	0.00
	57593.24	-0.52	0.38	-0.71	0.00	0.00

Asta	194	nod	82	102		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57587.27	0.52	-0.13	-6.74	0.00	0.00
	57559.29	0.52	0.25	2.02	0.00	0.00
150.7	57587.27	0.52	-0.13	-6.74	19.77	78.99
	57559.29	0.52	0.25	2.02	-37.21	78.49
301.5	57587.27	0.52	-0.13	-6.74	39.55	157.97
	57559.29	0.52	0.25	2.02	-74.42	156.98

Asta	196	nod	101	83		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ

0.0	57587.45	-0.52	-0.38	1.09	-113.23	157.96
	57559.44	-0.52	0.26	3.24	79.32	157.00
150.7	57587.45	-0.52	-0.38	1.09	-56.61	78.98
	57559.44	-0.52	0.26	3.24	39.66	78.50
301.5	57587.45	-0.52	-0.38	1.09	0.00	0.00
	57559.44	-0.52	0.26	3.24	0.00	0.00
Asta	197	nodI	32	103		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57875.51	0.52	0.50	-20.85	0.00	0.00
	57846.85	0.52	1.03	-11.46	0.00	0.00
150.7	57875.51	0.52	0.50	-20.85	-75.26	78.27
	57846.85	0.52	1.03	-11.46	-154.78	77.77
301.5	57875.51	0.52	0.50	-20.85	-150.51	156.55
	57846.85	0.52	1.03	-11.46	-309.56	155.55
Asta	199	nodI	104	84		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57875.09	-0.52	-0.86	12.61	-259.24	156.37
	57846.50	-0.52	-0.12	16.58	-37.48	155.91
150.7	57875.09	-0.52	-0.86	12.61	-129.62	78.18
	57846.50	-0.52	-0.12	16.58	-18.74	77.96
301.5	57875.09	-0.52	-0.86	12.61	0.00	0.00
	57846.50	-0.52	-0.12	16.58	0.00	0.00
Asta	200	nodI	97	105		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57679.68	-0.24	0.53	-2.01	266.92	155.65
	57697.83	-0.24	-0.03	13.49	119.17	156.50
150.2	57679.68	-0.24	0.53	-2.01	187.83	120.23
	57697.83	-0.24	-0.03	13.49	124.42	120.80
300.4	57679.68	-0.24	0.53	-2.01	108.75	84.82
	57697.83	-0.24	-0.03	13.49	129.67	85.10
Asta	201	nodI	105	98		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57679.72	0.24	0.08	-12.90	109.16	84.82
	57697.84	0.24	-0.53	0.55	129.28	85.10
150.2	57679.72	0.24	0.08	-12.90	97.12	120.39
	57697.84	0.24	-0.53	0.55	209.41	120.67
300.4	57679.72	0.24	0.08	-12.90	85.08	155.97
	57697.84	0.24	-0.53	0.55	289.54	156.25
Asta	204	nodI	99	108		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57376.93	-0.23	0.25	-6.31	91.37	156.86
	57409.37	-0.23	-0.30	8.94	-47.93	158.04
150.2	57376.93	-0.23	0.25	-6.31	54.41	121.99
	57409.37	-0.23	-0.30	8.94	-2.99	122.87
300.4	57376.93	-0.23	0.25	-6.31	17.44	87.13
	57409.37	-0.23	-0.30	8.94	41.95	87.70
Asta	205	nodI	108	100		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57376.93	0.23	0.34	-8.07	17.83	87.13
	57409.36	0.23	-0.26	4.76	41.59	87.70
150.2	57376.93	0.23	0.34	-8.07	-33.16	122.03
	57409.36	0.23	-0.26	4.76	80.53	122.83
300.4	57376.93	0.23	0.34	-8.07	-84.15	156.93
	57409.36	0.23	-0.26	4.76	119.47	157.96
Asta	207	nodI	102	109		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57403.42	-0.23	0.28	-8.69	39.39	157.97
	57375.41	-0.23	-0.21	5.55	-77.55	156.98
150.2	57403.42	-0.23	0.28	-8.69	-2.28	122.84
	57375.41	-0.23	-0.21	5.55	-46.49	122.09
300.4	57403.42	-0.23	0.28	-8.69	-43.96	87.71
	57375.41	-0.23	-0.21	5.55	-15.43	87.21
Asta	208	nodI	109	101		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57403.46	0.23	0.25	-4.31	-43.59	87.71
	57375.45	0.23	-0.32	7.10	-15.73	87.21
150.2	57403.46	0.23	0.25	-4.31	-80.71	122.83
	57375.45	0.23	-0.32	7.10	32.40	122.10
300.4	57403.46	0.23	0.25	-4.31	-117.82	157.96
	57375.45	0.23	-0.32	7.10	80.52	157.00
Asta	210	nodI	103	110		
PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
0.0	57691.53	-0.24	-0.06	-13.53	-154.98	156.55
	57662.84	-0.24	-0.68	3.51	-318.23	155.55
150.2	57691.53	-0.24	-0.06	-13.53	-146.10	120.87
	57662.84	-0.24	-0.68	3.51	-215.47	120.20
300.4	57691.53	-0.24	-0.06	-13.53	-137.22	85.19
	57662.84	-0.24	-0.68	3.51	-112.71	84.85

Asta	211	nod	110	104		
PROGR.	NORM	TTY	TZZ	TORS	MYT	MZZ
0.0	57691.45	0.24	0.44	0.14	-136.20	85.19
	57662.78	0.24	-0.24	14.77	-112.48	84.85
150.2	57691.45	0.24	0.44	0.14	-202.21	120.78
	57662.78	0.24	-0.24	14.77	-76.15	120.38
300.4	57691.45	0.24	0.44	0.14	-268.22	156.37
	57662.78	0.24	-0.24	14.77	-39.82	155.91

MEMBRATURE:

PROGETTO ELEMENTI IN CEMENTO ARMATO

lavoro : SCIPR3

Unita' di misura : Kgf ; cm ; Kgf/cm² ; Kgf*cm

TRAVATA : N. 1 T001

CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
46	0.0	360.0	30	33
47	360.0	840.0	33	34
48	840.0	1200.0	34	35

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
a T	0.0	1200.0	1200.0	70.0	110.0	20.0	30.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ARMATURE Long. : TOT												ASTA 46		
	N	A	%	SUP	N	A	%	INF	N	A	%			
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10			
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10			
fine	6	12.1	0.29		4	8.0	0.20		2	4.0	0.10			
TENSIONI Max. :	Sa 2009.3 P 360.				Sc -45.0 P 360.				Ty -4.0 P 360.					
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 19					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m		
	360.0	19	19.0	5.3										

ARMATURE Long. : TOT												ASTA 47		
	N	A	%	SUP	N	A	%	INF	N	A	%			
inizio	8	16.1	0.39		6	12.1	0.29		2	4.0	0.10			
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10			
fine	7	14.1	0.34		5	10.1	0.25		2	4.0	0.10			
TENSIONI Max. :	Sa 2060.8 P 840.				Sc -49.6 P 840.				Ty -3.9 P 840.					
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 25					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m		
	480.0	25	19.0	5.3										

ARMATURE Long. : TOT												ASTA 48		
	N	A	%	SUP	N	A	%	INF	N	A	%			
inizio	7	14.1	0.34		5	10.1	0.25		2	4.0	0.10			
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10			
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10			
TENSIONI Max. :	Sa 2141.9 P 930.				Sc -49.7 P 840.				Ty 3.9 P 840.					
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 20					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m		
	360.0	20	19.0	5.3										

TRAVATA : N. 2 T002

CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
110	0.0	1200.0	1	44

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
Rett.	0.0	1200.0	1200.0	30.0	90.0	0.0	0.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1

4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ASTA 110												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
campata	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
fine	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
TENSIONI Max. :	Sa 1619.0 P 600.				Sc -22.6 P 600.				Ty -1.1 P 0.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 50			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	225.0	12	19.0	5.3	750.0	25	30.0	3.4	225.0	13	19.0	5.3

TRAVATA : N. 3 T003 CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
111	0.0	1200.0	4	46

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
Rett.	0.0	1200.0	1200.0	30.0	90.0	0.0	0.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ASTA 111												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
campata	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
fine	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
TENSIONI Max. :	Sa 1923.1 P 600.				Sc -27.0 P 600.				Ty -1.2 P 0.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 50			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	225.0	12	19.0	5.3	750.0	25	30.0	3.4	225.0	13	19.0	5.3

TRAVATA : N. 4 T004 CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
112	0.0	1200.0	7	48

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
Rett.	0.0	1200.0	1200.0	30.0	90.0	0.0	0.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ASTA 112												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
campata	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
fine	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15	
TENSIONI Max. :	Sa 1885.8 P 600.				Sc -26.5 P 600.				Ty -1.1 P 0.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 50			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	225.0	12	19.0	5.3	750.0	25	30.0	3.4	225.0	13	19.0	5.3

TRAVATA : N. 5 T005 CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
113	0.0	1200.0	10	50

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
Rett.	0.0	1200.0	1200.0	30.0	90.0	0.0	0.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ARMATURE Long. : TOT												ASTA			113
inizio	N	A	%	SUP	N	A	%	INF	N	A	%				
campata	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15				
fine	4	8.0	0.30		2	4.0	0.15		2	4.0	0.15				
TENSIONI Max. :	Sa 1652.6 P 600.				Sc	-23.1 P 600.			Ty	-1.1 P 0.					
ARMATURE Tras. :	Diam. 8				N. braccia 2			N. tot. 50							
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m			
	225.0	12	19.0	5.3	750.0	25	30.0	3.4	225.0	13	19.0	5.3			

TRAVATA : N. 6 T006

CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
107	0.0	360.0	24	72
108	360.0	840.0	72	73
109	840.0	1200.0	73	52

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
a T	0.0	1200.0	1200.0	70.0	110.0	20.0	30.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ARMATURE Long. : TOT												ASTA			107
inizio	N	A	%	SUP	N	A	%	INF	N	A	%				
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
TENSIONI Max. :	Sa 2198.4 P 315.				Sc	-37.9 P 360.			Ty	-3.5 P 360.					
ARMATURE Tras. :	Diam. 8				N. braccia 2			N. tot. 19							
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m			
	360.0	19	19.0	5.3											

ARMATURE Long. : TOT												ASTA			108
inizio	N	A	%	SUP	N	A	%	INF	N	A	%				
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
TENSIONI Max. :	Sa 2028.5 P 360.				Sc	-39.1 P 840.			Ty	-3.5 P 840.					
ARMATURE Tras. :	Diam. 8				N. braccia 2			N. tot. 25							
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m			
	480.0	25	19.0	5.3											

ARMATURE Long. : TOT												ASTA			109
inizio	N	A	%	SUP	N	A	%	INF	N	A	%				
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10				
TENSIONI Max. :	Sa 1893.5 P 840.				Sc	-39.2 P 840.			Ty	3.5 P 840.					
ARMATURE Tras. :	Diam. 8				N. braccia 2			N. tot. 20							
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m			
	360.0	20	19.0	5.3											

TRAVATA : N. 7 T007

CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
36	0.0	240.0	30	14
37	240.0	480.0	14	1
38	480.0	720.0	1	16
39	720.0	960.0	16	4
40	960.0	1200.0	4	18
41	1200.0	1440.0	18	7

42	1440.0	1680.0	7	20
43	1680.0	1920.0	20	10
44	1920.0	2040.0	10	22
45	2040.0	2400.0	22	24

Sez.	Progr. I.	Progr. F.	L	B	H	S1	S2	S3	S4
a T	0.0	2400.0	2400.0	70.0	110.0	20.0	30.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soil
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Masetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ASTA 36												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
TENSIONI Max. :	Sa 1432.0 P 180.				Sc -12.2 P 180.				Ty 2.0 P 0.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 37												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
TENSIONI Max. :	Sa 1796.3 P 480.				Sc -17.5 P 480.				Ty -2.4 P 480.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 38												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
TENSIONI Max. :	Sa 1890.7 P 480.				Sc -17.3 P 480.				Ty 2.2 P 480.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 39												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	12.1	0.29		4	8.0	0.20		2	4.0	0.10	
TENSIONI Max. :	Sa 2124.8 P 930.				Sc -34.6 P 930.				Ty -3.3 P 960.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 40												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	6	12.1	0.29		4	8.0	0.20		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
TENSIONI Max. :	Sa 2074.3 P 1170.				Sc -35.9 P 1020.				Ty 2.7 P 960.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 41												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	6	12.1	0.29		4	8.0	0.20		2	4.0	0.10	
TENSIONI Max. :	Sa 2011.9 P 1440.				Sc -43.6 P 1440.				Ty -5.1 P 1440.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	195.0	10	19.0	5.3	45.0	3	15.0	6.7				

ASTA 42												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	6	12.1	0.29		4	8.0	0.20		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
fine	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
TENSIONI Max. :	Sa 2188.5 P 1560.				Sc -45.1 P 1440.				Ty 3.6 P 1440.			
ARMATURE Tras. :	Diam. 8				N. braccia 2				N. tot. 13			
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 43												
ARMATURE Long. : TOT	N	A	%	SUP	N	A	%	INF	N	A	%	
inizio	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	
campata	4	8.0	0.20		2	4.0	0.10		2	4.0	0.10	

fine	4	8.0	0.20	2	4.0	0.10	2	4.0	0.10			
TENSIONI Max.	Sa	2022.1	P1920.	Sc	-22.6	P1920.	Ty	-2.5	P1920.			
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 13					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 44												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
TENSIONI Max.	Sa	1948.0	P1920.		Sc	-22.8	P1920.		Ty	2.4	P1920.	
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 6					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	120.0	6	19.0	5.3								

ASTA 45												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
TENSIONI Max.	Sa	1166.5	P2220.		Sc	-10.1	P2220.		Ty	-1.6	P2400.	
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 20					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	360.0	20	19.0	5.3								

TRAVATA : N. 8 T008

CRITERI : 1

Asta	Progr.I.	Progr.F.	Nodo I.	Nodo F.
62	0.0	240.0	35	43
63	240.0	480.0	43	44
64	480.0	720.0	44	45
65	720.0	960.0	45	46
66	960.0	1200.0	46	47
67	1200.0	1440.0	47	48
68	1440.0	1680.0	48	49
69	1680.0	1920.0	49	50
104	1920.0	2160.0	50	66
105	2160.0	2400.0	66	52

Sez.	Progr.I.	Progr.F.	L	B	H	S1	S2	S3	S4
a T	0.0	2400.0	2400.0	70.0	110.0	20.0	30.0	3.0	1.0

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

ASTA 62												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
TENSIONI Max.	Sa	1571.8	P 210.		Sc	-13.4	P 210.		Ty	2.1	P 0.	
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 13					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 63												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
TENSIONI Max.	Sa	1704.0	P 480.		Sc	-16.0	P 480.		Ty	-2.4	P 480.	
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 13					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 64												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
TENSIONI Max.	Sa	1812.3	P 480.		Sc	-16.0	P 480.		Ty	2.2	P 480.	
ARMATURE Tras.	Diam. 8			N. braccia 2			N. tot. 13					
	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m	Lung.	N.	Ps	A/m
	240.0	13	19.0	5.3								

ASTA 65												
ARMATURE Long.	TOT	N	A	%	SUP	N	A	%	INF	N	A	%
inizio		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
campata		4	8.0	0.20		2	4.0	0.10		2	4.0	0.10
fine		6	12.1	0.29		4	8.0	0.20		2	4.0	0.10
TENSIONI Max.	Sa	1956.0	P 930.		Sc	-41.7	P 930.		Ty	-3.4	P 960.	

ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 13 19.0 5.3

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 66
 inizio 6 | 12.1 | 0.29 | 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 |
 campata 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 fine 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 2099.3 P1020. | Sc -37.9 P1020. | Ty 2.6 P 960.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 13 19.0 5.3

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 67
 inizio 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 campata 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 fine 6 | 12.1 | 0.29 | 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 2090.1 P1380. | Sc -44.6 P1440. | Ty -5.0 P1440.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 195.0 10 19.0 5.3 45.0 3 15.0 6.7

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 68
 inizio 7 | 14.1 | 0.34 | 4 | 8.0 | 0.20 | 3 | 6.0 | 0.15 |
 campata 5 | 10.1 | 0.25 | 2 | 4.0 | 0.10 | 3 | 6.0 | 0.15 |
 fine 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 2199.6 P1530. | Sc -45.2 P1440. | Ty 3.6 P1440.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 13 19.0 5.3

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 69
 inizio 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 campata 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 fine 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 1942.6 P1920. | Sc -21.0 P1920. | Ty -2.5 P1920.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 13 19.0 5.3

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 104
 inizio 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 campata 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 fine 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 1849.9 P1920. | Sc -21.1 P1920. | Ty 2.4 P1920.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 13 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 13 19.0 5.3

ARMATURE Long. : TOT N A % SUP N A % INF N A % ASTA 105
 inizio 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 campata 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 fine 4 | 8.0 | 0.20 | 2 | 4.0 | 0.10 | 2 | 4.0 | 0.10 |
 TENSIONI Max. : Sa 1144.7 P2220. | Sc -9.9 P2220. | Ty -1.6 P2400.
 ARMATURE Tras. : Diam. 8 | N. braccia 2 | N. tot. 14 |
 Lung. N. Ps A/m | Lung. N. Ps A/m | Lung. N. Ps A/m |
 240.0 14 19.0 5.3

VERIFICA ASTE IN ACCIAIO:

VERIFICA ELEMENTI IN ACCIAIO
 lavoro : SCIPR3

Unita di misura : Kgf ; cm ; Kgf/cm² ; Kgf*cm

MATERIALI
 Fe360: Mod.El.= 2100000.; samm= 1600.(1400. per sp>40 mm)

CASI DI CARICO

N	Descrizione	solli.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

CARATTERISTICHE GEOMETRICHE

P_HEB140_S004 (4) :
 A = 42.9619E+00 Jz= 1.5094E+03 Jy=549.6706E+00 Jt= 16.5832E+00

U_HEB140+T100 (10) :
 A = 63.7519E+00 Jz= 4.4882E+03 Jy=642.3245E+00 Jt= 24.5003E+00

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 21
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	7-1	0.0	0.0	0.0	-478.6	0.0	630.5
	6-1	0.0	0.0	0.0	3.5	-118.6	630.5
	1-1	0.0	0.0	0.0	2.1	0.0	630.5

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	7-1	1	Sx	-11.1	0.0	0.0	11.1
	6-1	6	Tz	0.1	-19.6	0.0	33.9
	1-1	9	Ty	0.0	0.0	-73.2	126.8
	7-1	9	Si	-11.1	0.0	-73.2	127.3

SOLLECITAZIONI : PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	37828.4	7114.3	0.0	3.5	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	266.1	0.0	0.0	266.1
6-1	si	5	Tz	-155.3	0.0	0.0	155.3

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	0.0	0.0	-478.6	0.0	-630.5
6-1	0.0	0.0	0.0	3.5	118.6	-630.5
1-1	0.0	0.0	0.0	2.1	0.0	-630.5

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx	-11.1	0.0	0.0	11.1
6-1	si	6	Tz	0.1	19.6	0.0	33.9
1-1	si	9	Ty	0.0	0.0	73.2	126.8
7-1	si	9	Si	-11.1	0.0	73.2	127.3

VERIFICA STABILITA' :

Caso 7-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 1 | om = 1.42 | csz = 1.00 | csy = 1.00
 Infless. Y

Ncrz = 543125.2 | Ncry = 197787.6
 Nmax = -478.6 | Mzeq = 32784.6 | Myeq = 0.0
 Ss = -168.1

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 22
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	7-1	0.0	0.0	0.0	-472.9	0.0	630.5
	6-1	0.0	0.0	0.0	3.1	-118.6	630.5
	1-1	0.0	0.0	0.0	2.0	0.0	630.5

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-11.0	0.0	0.0	11.0
6-1	si	6	Tz	0.1	-19.6	0.0	33.9
1-1	si	9	Ty	0.0	0.0	-73.2	126.8
7-1	si	9	Si	-11.0	0.0	-73.2	127.3

SOLLECITAZIONI : PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	37828.4	7114.3	0.0	3.1	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	266.1	0.0	0.0	266.1
6-1	si	5	Tz	-155.3	0.0	0.0	155.3

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	0.0	0.0	-472.9	0.0	-630.5
6-1	0.0	0.0	0.0	3.1	118.6	-630.5
1-1	0.0	0.0	0.0	2.0	0.0	-630.5

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx	-11.0	0.0	0.0	11.0
6-1	si	6	Tz	0.1	19.6	0.0	33.9
1-1	si	9	Ty	0.0	0.0	73.2	126.8
7-1	si	9	Si	-11.0	0.0	73.2	127.3

VERIFICA STABILITA` :

Caso 7- 1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |
 Infless. Y
 Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -472.9 | Mzeq = 32784.6 | Myeq = 0.0 |
 Ss = -167.9

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 23
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	0.0	0.0	0.0	-386.8	0.0	630.5
6- 1	0.0	0.0	0.0	3.0	-118.6	630.5
1- 1	0.0	0.0	0.0	-4.8	0.0	630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	1	Sx	-9.0	0.0	0.0	9.0
6- 1	si	6	Tz	0.1	-19.6	0.0	33.9
1- 1	si	9	Ty	-0.1	0.0	-73.2	126.8
7- 1	si	9	Si	-9.0	0.0	-73.2	127.2

PROGR. 120.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	37828.4	7114.3	0.0	3.0	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	266.1	0.0	0.0	266.1
6- 1	si	5	Tz	-155.3	0.0	0.0	155.3

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	0.0	0.0	0.0	-386.8	0.0	-630.5
6- 1	0.0	0.0	0.0	3.0	118.6	-630.5
1- 1	0.0	0.0	0.0	-4.8	0.0	-630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	1	Sx	-9.0	0.0	0.0	9.0
6- 1	si	6	Tz	0.1	19.6	0.0	33.9
1- 1	si	9	Ty	-0.1	0.0	73.2	126.8
7- 1	si	9	Si	-9.0	0.0	73.2	127.2

VERIFICA STABILITA` :

Caso 7- 1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 1 | om = 1.42 | csz = 1.00 | csy = 1.00 |
 Infless. Y
 Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -386.8 | Mzeq = 32784.6 | Myeq = 0.0 |
 Ss = -165.0

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 24
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	0.0	0.0	0.0	-381.4	0.0	630.5
6- 1	0.0	0.0	0.0	2.5	-118.6	630.5
1- 1	0.0	0.0	0.0	-5.3	0.0	630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	1	Sx	-8.9	0.0	0.0	8.9
6- 1	si	6	Tz	0.1	-19.6	0.0	33.9
1- 1	si	9	Ty	-0.1	0.0	-73.2	126.8
7- 1	si	9	Si	-8.9	0.0	-73.2	127.2

PROGR. 120.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	37828.4	7114.3	0.0	2.5	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	266.1	0.0	0.0	266.1
6- 1	si	5	Tz	-155.3	0.0	0.0	155.3

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	0.0	0.0	0.0	-381.4	0.0	-630.5
6- 1	0.0	0.0	0.0	2.5	118.6	-630.5
1- 1	0.0	0.0	0.0	-5.3	0.0	-630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	2	Sx	-8.9	0.0	0.0	8.9
6- 1	si	6	Tz	0.1	19.6	0.0	33.9
1- 1	si	9	Ty	-0.1	0.0	73.2	126.8
7- 1	si	9	Si	-8.9	0.0	73.2	127.2

VERIFICA STABILITA' :

Caso 7- 1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00
 Influss. Y | Ncrz = 543125.2 | Ncry = 197787.6
 | Nmax = -381.4 | Mzeq = 32784.6 | Myeq = 0.0
 Ss = -164.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 25
 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	0.0	0.0	0.0	-1063.0	0.0	630.5
6- 1	0.0	0.0	0.0	-7.3	-118.6	630.5
1- 1	0.0	0.0	0.0	-12.1	0.0	630.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	1	Sx	-24.7	0.0	0.0
6- 1	si	6	Tz	-0.2	-19.6	0.0
1- 1	si	9	Ty	-0.3	0.0	-73.2
8- 1	si	9	si	-24.7	0.0	-73.2
						129.2

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00
 Influss. Y | Ncrz = 543125.2 | Ncry = 197787.6
 | Nmax = -7.3 | Mzeq = 32784.6 | Myeq = 6165.7
 Ss = -230.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 26
 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
10- 1	0.0	0.0	0.0	-3596.7	0.0	630.5
6- 1	0.0	0.0	0.0	-44.0	-118.6	630.5
1- 1	0.0	0.0	0.0	-12.1	0.0	630.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
10- 1	si	1	Sx	-83.7	0.0	0.0
6- 1	si	6	Tz	-1.0	-19.6	0.0
1- 1	si	9	Ty	-0.3	0.0	-73.2
10- 1	si	9	si	-83.7	0.0	-73.2
						152.0

VERIFICA STABILITA' :

Caso10- 1 | LO = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 1 | om = 1.42 | csz = 1.01 | csy = 1.03 |
 Infless. Y

| Ncrz = 543125.2 | Ncry = 197787.6 |
 | Nmax = -3596.7 | Mzeq = 32784.6 | Myeq = 0.0 |
 Ss = -272.5

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 27
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 2	0.0	0.0	0.0	-239.6	0.0	630.5
6- 1	0.0	0.0	0.0	-9.6	-118.6	630.5
1- 1	0.0	0.0	0.0	-11.5	0.0	630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	1	Sx	-5.6	0.0	0.0	5.6
6- 1	si	6	Tz	-0.2	-19.6	0.0	33.9
1- 1	si	9	Ty	-0.3	0.0	-73.2	126.8
8- 2	si	9	Si	-5.6	0.0	-73.2	127.0

PROGR. 120.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	37828.4	7114.3	0.0	-9.6	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	2	Sx	-266.3	0.0	0.0	266.3
6- 1	si	5	Tz	-155.6	0.0	0.0	155.6

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 2	0.0	0.0	0.0	-239.6	0.0	-630.5
6- 1	0.0	0.0	0.0	-9.6	118.6	-630.5
1- 1	0.0	0.0	0.0	-11.5	0.0	-630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	1	Sx	-5.6	0.0	0.0	5.6
6- 1	si	6	Tz	-0.2	19.6	0.0	33.9
1- 1	si	9	Ty	-0.3	0.0	73.2	126.8
8- 2	si	9	Si	-5.6	0.0	73.2	127.0

VERIFICA STABILITA' :

Caso 6- 1 | LO = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |
 Infless. Y

| Ncrz = 543125.2 | Ncry = 197787.6 |
 | Nmax = -9.6 | Mzeq = 32784.6 | Myeq = 6165.7 |
 Ss = -230.9

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 28
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10- 1	0.0	0.0	0.0	-269.0	0.0	630.5
6- 1	0.0	0.0	0.0	-9.1	-118.6	630.5
1- 1	0.0	0.0	0.0	-11.2	0.0	630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10- 1	si	1	Sx	-6.3	0.0	0.0	6.3
6- 1	si	6	Tz	-0.2	-19.6	0.0	33.9
1- 1	si	9	Ty	-0.3	0.0	-73.2	126.8
10- 1	si	9	Si	-6.3	0.0	-73.2	127.0

PROGR. 120.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	37828.4	7114.3	0.0	-9.1	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	2	Sx	-266.2	0.0	0.0	266.2
6- 1	si	5	Tz	-155.6	0.0	0.0	155.6

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10- 1	0.0	0.0	0.0	-269.0	0.0	-630.5
6- 1	0.0	0.0	0.0	-9.1	118.6	-630.5
1- 1	0.0	0.0	0.0	-11.2	0.0	-630.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10- 1	si	1	Sx	-6.3	0.0	0.0	6.3
6- 1	si	6	Tz	-0.2	19.6	0.0	33.9
1- 1	si	9	Ty	-0.3	0.0	73.2	126.8
10- 1	si	9	Si	-6.3	0.0	73.2	127.0

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00
 Infless. Y | Ncrz = 543125.2 | Ncry = 197787.6
 | Nmax = -9.1 | Mzeq = 32784.6 | Myeq = 6165.7
 Ss = -230.9

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 29
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
10- 2		0.0	0.0	0.0	-146.3	0.0	315.2
6- 1		0.0	0.0	0.0	-2.8	-59.3	315.2
1- 1		0.0	0.0	0.0	-1.3	0.0	315.2

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
10- 2	si	1	0.0	0.0	3.4
6- 1	si	6	-3.4	0.0	17.0
1- 1	si	9	-0.1	-9.8	63.4
10- 2	si	9	0.0	0.0	63.5

SOLLECITAZIONI : PROGR. 60.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
6- 1		9457.1	1778.6	0.0	-2.8	0.0	0.0
10- 1		9457.1	0.0	0.0	143.0	0.0	0.0

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
6- 1	si	2	-66.6	0.0	66.6
6- 1	si	5	-38.9	0.0	38.9
10- 1	si	9	3.3	0.0	3.3

SOLLECITAZIONI : PROGR. 120.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
10- 2		0.0	0.0	0.0	-146.3	0.0	-315.2
6- 1		0.0	0.0	0.0	-2.8	59.3	-315.2
2- 1		0.0	0.0	0.0	-0.4	0.0	-315.2

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
10- 2	si	1	-3.4	0.0	3.4
6- 1	si	6	-0.1	9.8	17.0
2- 1	si	9	0.0	0.0	63.4
10- 2	si	9	-3.4	0.0	63.5

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.6 | Im = 33.5
 Nodo 2 | om = 1.09 | csz = 1.00 | csy = 1.00
 Infless. Y | Ncrz = 2172500.9 | Ncry = 791150.5
 | Nmax = -2.8 | Mzeq = 8196.2 | Myeq = 1541.4
 Ss = -57.7

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 30
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
7- 1		0.0	0.0	0.0	134.5	0.0	945.7
6- 1		0.0	0.0	0.0	-1.5	-177.9	945.7
1- 1		0.0	0.0	0.0	-0.3	0.0	945.7

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
7- 1	si	1	3.1	0.0	3.1
6- 1	si	6	0.0	-29.4	50.9
1- 1	si	9	0.0	0.0	190.3
7- 1	si	9	3.1	0.0	190.3

SOLLECITAZIONI : PROGR. 180.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
6- 1		85114.0	16007.1	0.0	-1.5	0.0	0.0
9- 1		85114.0	0.0	0.0	-2.9	0.0	0.0

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
6- 1	si	2	-598.6	0.0	598.6
6- 1	si	6	-439.9	0.0	439.9
9- 1	si	9	-0.1	0.0	0.1

SOLLECITAZIONI : PROGR. 360.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
7- 1		0.0	0.0	0.0	134.5	0.0	-945.7
6- 1		0.0	0.0	0.0	-1.5	177.9	-945.7
1- 1		0.0	0.0	0.0	-0.3	0.0	-945.7

TENSIONI		Sx	Tz	Ty	Si
Caso	Ve				
7- 1	si	3	3.1	0.0	3.1

6-1	si	6	Tz	0.0	29.4	0.0	50.9
1-1	si	9	Ty	0.0	0.0	109.9	190.3
7-1	si	9	Si	3.1	0.0	109.9	190.3

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 360.0 | Lc = 360.0 | Ro = 3.6 | Im = 100.6 |
 Nodo 2 | om = 2.02 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 241389.0 | Ncry = 87905.6 |
 | Nmax = -1.5 | Mzeq = 73765.5 | Myeq = 13872.8 |
 | Ss = -518.8 |

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 31
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-12686.2	0.0	1260.9
6-1	0.0	0.0	0.0	-480.7	-237.1	1260.9
1-1	0.0	0.0	0.0	-49.4	0.0	1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-295.3	0.0	0.0	295.3
6-1	si	6	Tz	-11.2	-39.2	0.0	68.8
1-1	si	9	Ty	-1.1	0.0	-146.5	253.7
8-1	si	9	Si	-295.3	0.0	-146.5	389.3

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	151313.8	28457.1	0.0	-480.7	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-1075.3	0.0	0.0	1075.3
6-1	si	5	Tz	-632.7	0.0	0.0	632.7

PROGR. 480.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-12686.2	0.0	-1260.9
6-1	0.0	0.0	0.0	-480.7	237.1	-1260.9
1-1	0.0	0.0	0.0	-49.4	0.0	-1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-295.3	0.0	0.0	295.3
6-1	si	6	Tz	-11.2	39.2	0.0	68.8
1-1	si	9	Ty	-1.1	0.0	146.5	253.7
8-1	si	9	Si	-295.3	0.0	146.5	389.3

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 1 | om = 2.93 | csz = 1.16 | csy = 1.63 |
 Infless. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -12686.2 | Mzeq = 131138.6 | Myeq = 0.0 |
 | Ss = -1571.8 |

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 32
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	-2103.5	0.0	1260.9
6-1	0.0	0.0	0.0	-21.8	-237.1	1260.9
1-1	0.0	0.0	0.0	4.0	0.0	1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	-49.0	0.0	0.0	49.0
6-1	si	6	Tz	-0.5	-39.2	0.0	67.9
1-1	si	9	Ty	0.1	0.0	-146.5	253.7
10-2	si	9	Si	-49.0	0.0	-146.5	258.4

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	151313.8	28457.1	0.0	-21.8	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-1064.6	0.0	0.0	1064.6
6-1	si	5	Tz	-622.0	0.0	0.0	622.0

PROGR. 480.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	-2103.5	0.0	-1260.9
6-1	0.0	0.0	0.0	-21.8	237.1	-1260.9
1-1	0.0	0.0	0.0	4.0	0.0	-1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	-49.0	0.0	0.0	49.0

6-1	si	6	Tz	-0.5	39.2	0.0	67.9
1-1	si	9	Ty	0.1	0.0	146.5	253.7
10-2	si	9	Si	-49.0	0.0	146.5	258.4

VERIFICA STABILITA' :

Caso 6-1 | LO = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 2 | om = 2.93 | csz = 1.00 | csy = 1.00 |
 Influss. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -21.8 | Mzeq = 131138.6 | Myeq = 24662.8 |
 | Ss = -924.1 |

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 33
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	3897.7	0.0	1260.9
6-1	0.0	0.0	0.0	-40.7	-237.1	1260.9
1-1	0.0	0.0	0.0	8.3	0.0	1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	90.7	0.0	0.0	90.7
6-1	si	6	Tz	-0.9	-39.2	0.0	67.9
1-1	si	9	Ty	0.2	0.0	-146.5	253.7
10-2	si	9	Si	90.7	0.0	-146.5	269.4

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	151313.8	28457.1	0.0	-40.7	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-1065.1	0.0	0.0	1065.1
6-1	si	5	Tz	-622.4	0.0	0.0	622.4

SOLLECITAZIONI : PROGR. 480.00

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	3897.7	0.0	-1260.9
6-1	0.0	0.0	0.0	-40.7	237.1	-1260.9
1-1	0.0	0.0	0.0	8.3	0.0	-1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	90.7	0.0	0.0	90.7
6-1	si	6	Tz	-0.9	39.2	0.0	67.9
1-1	si	9	Ty	0.2	0.0	146.5	253.7
10-2	si	9	Si	90.7	0.0	146.5	269.4

VERIFICA STABILITA' :

Caso 6-1 | LO = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 2 | om = 2.93 | csz = 1.00 | csy = 1.00 |
 Influss. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -40.7 | Mzeq = 131138.6 | Myeq = 24662.8 |
 | Ss = -925.7 |

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 34
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-2140.1	0.0	1260.9
6-1	0.0	0.0	0.0	-50.5	-237.1	1260.9
1-1	0.0	0.0	0.0	1.4	0.0	1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-49.8	0.0	0.0	49.8
6-1	si	6	Tz	-1.2	-39.2	0.0	67.9
1-1	si	9	Ty	0.0	0.0	-146.5	253.7
8-1	si	9	Si	-49.8	0.0	-146.5	258.5

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	151313.8	28457.1	0.0	-50.5	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-1065.3	0.0	0.0	1065.3
6-1	si	5	Tz	-622.7	0.0	0.0	622.7

SOLLECITAZIONI : PROGR. 480.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-2140.1	0.0	-1260.9
6-1	0.0	0.0	0.0	-50.5	237.1	-1260.9
1-1	0.0	0.0	0.0	1.4	0.0	-1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-49.8	0.0	0.0	49.8

6-1	si	6	Tz	-1.2	39.2	0.0	67.9
1-1	si	9	Ty	0.0	0.0	146.5	253.7
8-1	si	9	Si	-49.8	0.0	146.5	258.5

VERIFICA STABILITA' :

Caso 6-1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 2 | om = 2.93 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -50.5 | Mzeq = 131138.6 | Myeq = 24662.8 |
 | Ss = -926.5

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 35
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-455.0	0.0	1260.9
6-1	0.0	0.0	0.0	-11.9	-237.1	1260.9
1-1	0.0	0.0	0.0	-1.8	0.0	1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-10.6	0.0	0.0	10.6
6-1	si	6	Tz	-0.3	-39.2	0.0	67.9
1-1	si	9	Ty	0.0	0.0	-146.5	253.7
8-1	si	9	Si	-10.6	0.0	-146.5	253.9

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	151313.8	28457.1	0.0	-11.9	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-1064.4	0.0	0.0	1064.4
6-1	si	5	Tz	-621.8	0.0	0.0	621.8

PROGR. 480.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-455.0	0.0	-1260.9
6-1	0.0	0.0	0.0	-11.9	237.1	-1260.9
1-1	0.0	0.0	0.0	-1.8	0.0	-1260.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-10.6	0.0	0.0	10.6
6-1	si	6	Tz	-0.3	39.2	0.0	67.9
1-1	si	9	Ty	0.0	0.0	146.5	253.7
8-1	si	9	Si	-10.6	0.0	146.5	253.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 2 | om = 2.93 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -11.9 | Mzeq = 131138.6 | Myeq = 24662.8 |
 | Ss = -923.3

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 56
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	0.0	0.0	0.0	-502.9	0.0	1535.7
7-1	0.0	0.0	0.0	-9.2	186.4	1535.7
1-1	0.0	0.0	0.0	-5.8	0.0	1535.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	-11.7	0.0	0.0	11.7
7-1	si	5	Tz	-0.2	43.4	0.0	75.2
1-1	si	9	Ty	-0.1	0.0	-178.4	309.0
6-1	si	9	Si	-11.7	0.0	-178.4	309.2

PROGR. 180.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	138211.1	-16777.9	0.0	-9.2	0.0	0.0
9-2	138211.1	0.0	0.0	-6.9	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-854.8	0.0	0.0	854.8
7-1	si	5	Tz	-688.5	0.0	0.0	688.5
9-2	si	9	Ty	-0.2	0.0	0.0	0.2

PROGR. 360.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	0.0	0.0	0.0	-502.9	0.0	-1535.7
7-1	0.0	0.0	0.0	-9.2	-186.4	-1535.7
1-1	0.0	0.0	0.0	-5.8	0.0	-1535.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	-11.7	0.0	0.0	11.7
7-1	si	5	Tz	-0.2	-43.4	0.0	75.2
1-1	si	9	Ty	-0.1	0.0	178.4	309.0
6-1	si	9	Si	-11.7	0.0	178.4	309.2

VERIFICA STABILITA' :

Caso 7-1 | L0 = 360.0 | Lc = 360.0 | Ro = 3.6 | Im = 100.6
 Nodo 1 | om = 2.02 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 241389.0 | Ncry = 87905.6 |
 | Nmax = -9.2 | Mzeq = 119783.0 | Myeq = -14540.8 |
 | Ss = -741.2

P_HEB140_s004 (4) - metodo: tensioni ammissibili - ASTA 57
 PROGR. 0.00

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	1	Sx	138.1	0.0	0.0	138.1
7-1	si	5	Tz	0.0	57.9	0.0	100.2
1-1	si	9	Ty	0.6	0.0	-237.8	411.9
9-2	si	9	Si	138.1	0.0	-237.8	434.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	1	Sx	138.1	0.0	0.0	138.1
7-1	si	5	Tz	0.0	57.9	0.0	100.2
1-1	si	9	Ty	0.6	0.0	-237.8	411.9
9-2	si	9	Si	138.1	0.0	-237.8	434.5

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	3	Sx	1519.4	0.0	0.0	1519.4
1-1	si	9	Ty	-1223.6	0.0	0.0	1223.6
1-1	si	9	Si	0.6	0.0	0.0	0.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	3	Sx	1519.4	0.0	0.0	1519.4
1-1	si	9	Ty	-1223.6	0.0	0.0	1223.6
1-1	si	9	Si	0.6	0.0	0.0	0.6

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	1	Sx	138.1	0.0	0.0	138.1
7-1	si	5	Tz	0.0	-57.9	0.0	100.2
1-1	si	9	Ty	0.6	0.0	237.8	411.9
9-2	si	9	Si	138.1	0.0	237.8	434.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	1	Sx	138.1	0.0	0.0	138.1
7-1	si	5	Tz	0.0	-57.9	0.0	100.2
1-1	si	9	Ty	0.6	0.0	237.8	411.9
9-2	si	9	Si	138.1	0.0	237.8	434.5

VERIFICA STABILITA' :

Caso 9-1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 1 | om = 2.93 | csz = 1.07 | csy = 1.22 |
 Infless. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -5883.6 | Mzeq = 212947.5 | Myeq = 0.0 |
 | Ss = -1457.2

P_HEB140_s004 (4) - metodo: tensioni ammissibili - ASTA 58
 PROGR. 0.00

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	1.7	0.0	0.0	1.7
7-1	si	5	Tz	-0.2	43.4	0.0	75.2
1-1	si	9	Ty	-0.1	0.0	-178.4	309.0
6-1	si	9	Si	1.7	0.0	-178.4	309.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	1.7	0.0	0.0	1.7
7-1	si	5	Tz	-0.2	43.4	0.0	75.2
1-1	si	9	Ty	-0.1	0.0	-178.4	309.0
6-1	si	9	Si	1.7	0.0	-178.4	309.0

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-854.8	0.0	0.0	854.8
9-1	si	5	Tz	-688.5	0.0	0.0	688.5
9-1	si	9	Ty	0.1	0.0	0.0	0.1

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-854.8	0.0	0.0	854.8
9-1	si	5	Tz	-688.5	0.0	0.0	688.5
9-1	si	9	Ty	0.1	0.0	0.0	0.1

SOLLECITAZIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	138211.1	0.0	0.0	138211.1
9-1	si	5	Tz	0.0	0.0	0.0	0.0
9-1	si	9	Ty	0.0	0.0	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	138211.1	0.0	0.0	138211.1
9-1	si	5	Tz	0.0	0.0	0.0	0.0
9-1	si	9	Ty	0.0	0.0	0.0	0.0

6-1	0.0	0.0	0.0	72.2	0.0	-1535.7	
7-1	0.0	0.0	0.0	-7.7	-186.4	-1535.7	
1-1	0.0	0.0	0.0	-5.5	0.0	-1535.7	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	1.7	0.0	0.0	1.7
7-1	si	5	Tz	-0.2	-43.4	0.0	75.2
1-1	si	9	Ty	-0.1	0.0	178.4	309.0
6-1	si	9	Si	1.7	0.0	178.4	309.0

VERIFICA STABILITA' :

Caso 7- 1 | L0 = 360.0 | Lc = 360.0 | Ro = 3.6 | lm= 100.6 |
 Nodo 1 | om = 2.02 | csz= 1.00 | csy= 1.00 |
 Infless. Y | Ncrz = 241389.0 | Ncry= 87905.6 |
 | Nmax = -7.7 | Mzeq= 119783.0 | Myeq= -14540.8 |
 | Ss = -741.1

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 89
 PROGR. 0.00

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	-573.9	0.0	1241.4	
6-1	0.0	0.0	0.0	-21.1	-78.0	1241.4	
1-1	0.0	0.0	0.0	-5.3	0.0	1241.4	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-13.4	0.0	0.0	13.4
6-1	si	6	Tz	-0.5	-32.0	0.0	55.4
1-1	si	9	Ty	-0.1	0.0	-144.2	249.7
8-1	si	9	Si	-13.4	0.0	-144.2	250.1

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	148963.7	9358.3	0.0	-21.1	0.0	0.0
1-1	148963.7	0.0	0.0	-5.3	0.0	0.0

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-810.5	0.0	0.0	810.5
1-1	si	5	Tz	-691.0	0.0	0.0	691.0

SOLLECITAZIONI : PROGR. 480.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-573.9	0.0	-1241.4
6-1	0.0	0.0	0.0	-21.1	78.0	-1241.4
1-1	0.0	0.0	0.0	-5.3	0.0	-1241.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx	-13.4	0.0	0.0	13.4
6-1	si	6	Tz	-0.5	32.0	0.0	55.4
1-1	si	9	Ty	-0.1	0.0	144.2	249.7
8-1	si	9	Si	-13.4	0.0	144.2	250.1

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | lm= 134.2 |
 Nodo 2 | om = 2.93 | csz= 1.00 | csy= 1.00 |
 Infless. Y | Ncrz = 135781.3 | Ncry= 49446.9 |
 | Nmax = -21.1 | Mzeq= 129101.9 | Myeq= 8110.5 |
 | Ss = -703.7

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 90
 PROGR. 0.00

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	-2584.3	0.0	1241.4	
6-1	0.0	0.0	0.0	46.3	-78.0	1241.4	
1-1	0.0	0.0	0.0	-2.0	0.0	1241.4	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-60.2	0.0	0.0	60.2
6-1	si	6	Tz	1.1	-32.0	0.0	55.4
1-1	si	9	Ty	0.0	0.0	-144.2	249.7
8-1	si	9	Si	-60.2	0.0	-144.2	256.9

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	148963.7	9358.3	0.0	46.3	0.0	0.0
9-1	148963.7	0.0	0.0	-6.6	0.0	0.0

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	811.1	0.0	0.0	811.1
9-1	si	5	Tz	-691.0	0.0	0.0	691.0

PROGR. 480.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	-2584.3	0.0	-1241.4
6-1	0.0	0.0	0.0	46.3	78.0	-1241.4
1-1	0.0	0.0	0.0	-2.0	0.0	-1241.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-60.2	0.0	0.0	60.2
6-1	si	6	Tz	1.1	32.0	0.0	55.4
1-1	si	9	Ty	0.0	0.0	144.2	249.7
8-1	si	9	Si	-60.2	0.0	144.2	256.9

VERIFICA STABILITA' :

Caso 8-1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 1 | om = 2.93 | csz = 1.03 | csy = 1.09 |
 Infless. Y

Ncrz = 135781.3 | Ncry = 49446.9 |
 Nmax = -2584.3 | Mzeq = 129101.9 | Myeq = 0.0 |
 Ss = -792.4

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 91
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-2	0.0	0.0	0.0	4600.2	0.0	1241.4
6-1	0.0	0.0	0.0	62.2	-78.0	1241.4
1-1	0.0	0.0	0.0	6.5	0.0	1241.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-2	si	1	Sx	107.1	0.0	0.0	107.1
6-1	si	6	Tz	1.4	-32.0	0.0	55.4
1-1	si	9	Ty	0.2	0.0	-144.2	249.7
8-2	si	9	Si	107.1	0.0	-144.2	271.7

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	148963.7	9358.3	0.0	62.2	0.0	0.0
9-1	148963.7	0.0	0.0	22.4	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	811.5	0.0	0.0	811.5
9-1	si	5	Tz	-690.3	0.0	0.0	690.3

PROGR. 480.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-2	0.0	0.0	0.0	4600.2	0.0	-1241.4
6-1	0.0	0.0	0.0	62.2	78.0	-1241.4
1-1	0.0	0.0	0.0	6.5	0.0	-1241.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-2	si	1	Sx	107.1	0.0	0.0	107.1
6-1	si	6	Tz	1.4	32.0	0.0	55.4
1-1	si	9	Ty	0.2	0.0	144.2	249.7
8-2	si	9	Si	107.1	0.0	144.2	271.7

VERIFICA STABILITA' :

Caso 8-1 | L0 = 480.0 | Lc = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 1 | om = 2.93 | csz = 1.05 | csy = 1.16 |
 Infless. Y

Ncrz = 135781.3 | Ncry = 49446.9 |
 Nmax = -4543.0 | Mzeq = 129101.9 | Myeq = 0.0 |
 Ss = -940.0

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 92
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	-2635.7	0.0	1241.4
6-1	0.0	0.0	0.0	20.1	-78.0	1241.4
1-1	0.0	0.0	0.0	1.9	0.0	1241.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	-61.3	0.0	0.0	61.3
6-1	si	6	Tz	0.5	-32.0	0.0	55.4
1-1	si	9	Ty	0.0	0.0	-144.2	249.7
10-2	si	9	Si	-61.3	0.0	-144.2	257.2

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	148963.7	9358.3	0.0	20.1	0.0	0.0
9-2	148963.7	0.0	0.0	-97.5	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	810.5	0.0	0.0	810.5

| 9- 2|si| 5| Tz | -693.1| 0.0| 0.0| 693.1|
 SOLLECITAZIONI :
 10- 2| MZ | MY | MT | N | TZ | TY |
 6- 1| 0.0| 0.0| 0.0| -2635.7| 0.0| -1241.4|
 1- 1| 0.0| 0.0| 0.0| 20.1| 78.0| -1241.4|
 1- 1| 0.0| 0.0| 0.0| 1.9| 0.0| -1241.4|

TENSIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 10- 2|si| 1| Sx | -61.3 | 0.0 | 0.0 | 61.3 |
 6- 1|si| 6| Tz | 0.5 | 32.0 | 0.0 | 55.4 |
 1- 1|si| 9| Ty | 0.0 | 0.0 | 144.2 | 249.7 |
 10- 2|si| 9| Si | -61.3 | 0.0 | 144.2 | 257.2 |

VERIFICA STABILITA` :

Caso10- 2 | L0 = 480.0| Lc = 480.0| Ro = 3.6 | Im = 134.2|
 Nodo 1 | om = 2.93| csz = 1.03| csy = 1.09|
 Infless. Y | Ncrz = 135781.3| Ncry = 49446.9|
 | Nmax = -2635.7| Mzeq = 129101.9| Myeq = 0.0|
 Ss = -796.3

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 93
 PROGR. 0.00

SOLLECITAZIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 8- 1|si| 1| Sx | -13.4 | 0.0 | 0.0 | 13.4 |
 6- 1|si| 6| Tz | -0.5 | -32.0 | 0.0 | 55.4 |
 1- 1|si| 9| Ty | -0.1 | 0.0 | -144.2 | 249.7 |
 8- 1|si| 9| Si | -13.4 | 0.0 | -144.2 | 250.1 |

SOLLECITAZIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 6- 1|si| 1| Sx | 9358.3 | 0.0 | -21.2 | 0.0 |
 1- 1|si| 6| Tz | 0.0 | 0.0 | -3.4 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 6- 1|si| 2| Sx | -810.5 | 0.0 | 0.0 | 810.5 |
 1- 1|si| 5| Tz | -690.9 | 0.0 | 0.0 | 690.9 |

SOLLECITAZIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 8- 1|si| 1| Sx | -13.4 | 0.0 | -574.0 | 0.0 | -1241.4 |
 6- 1|si| 6| Tz | 0.0 | 0.0 | -21.2 | 78.0 | -1241.4 |
 1- 1|si| 9| Ty | 0.0 | 0.0 | -3.4 | 0.0 | -1241.4 |

TENSIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 8- 1|si| 1| Sx | -13.4 | 0.0 | 0.0 | 13.4 |
 6- 1|si| 6| Tz | -0.5 | 32.0 | 0.0 | 55.4 |
 1- 1|si| 9| Ty | -0.1 | 0.0 | 144.2 | 249.7 |
 8- 1|si| 9| Si | -13.4 | 0.0 | 144.2 | 250.1 |

VERIFICA STABILITA` :

Caso 6- 1 | L0 = 480.0| Lc = 480.0| Ro = 3.6 | Im = 134.2|
 Nodo 2 | om = 2.93| csz = 1.00| csy = 1.00|
 Infless. Y | Ncrz = 135781.3| Ncry = 49446.9|
 | Nmax = -21.2| Mzeq = 129101.9| Myeq = 8110.5|
 Ss = -703.7

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 94
 PROGR. 0.00

SOLLECITAZIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 7- 1|si| 1| Sx | -11.5 | 0.0 | -495.4 | 11.5 |
 6- 1|si| 6| Tz | 0.2 | -6.9 | 8.4 | 11.9 |
 1- 1|si| 9| Ty | 0.1 | 0.0 | 3.6 | 45.6 |
 7- 1|si| 9| Si | -11.5 | 0.0 | -26.3 | 47.0 |

SOLLECITAZIONI :
 Caso|Ve|No|massimi| Sx | Tz | Ty | Si |
 6- 1|si| 1| Sx | 13601.9 | 2339.6 | 0.0 | 8.4 | 0.0 | 0.0 |

6-1	si	4	Sx	Si	93.1	0.0	0.0	93.1
6-1	si	5	Tz		-56.3	0.0	0.0	56.3

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	0.0	0.0	-495.4	0.0	-226.7
6-1	0.0	0.0	0.0	8.4	39.0	-226.7
1-1	0.0	0.0	0.0	3.6	0.0	-226.7

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-11.5	0.0	0.0	11.5
6-1	si	6	Tz	0.2	6.9	0.0	11.9
1-1	si	9	Ty	0.1	0.0	26.3	45.6
7-1	si	9	Si	-11.5	0.0	26.3	47.0

VERIFICA STABILITA` :

Caso 7-1 |LO = 240.0|Lc = 240.0|Ro = 3.6|Im= 67.1|
 Nodo 1 |om = 1.42|csz= 1.00|csy= 1.00|
 Infless. Y |Ncrz = 543125.2|Ncry= 197787.6|
|Nmax = -495.4|Mzeq= 11788.3|Myeq= 0.0|
|Ss = -71.1|

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 95
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	0.0	0.0	-490.3	0.0	226.7
6-1	0.0	0.0	0.0	8.8	-39.0	226.7
1-1	0.0	0.0	0.0	3.8	0.0	226.7

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-11.4	0.0	0.0	11.4
6-1	si	6	Tz	0.2	-6.9	0.0	11.9
1-1	si	9	Ty	0.1	0.0	-26.3	45.6
7-1	si	9	Si	-11.4	0.0	-26.3	47.0

SOLLECITAZIONI : PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	13601.9	2339.6	0.0	8.8	0.0	0.0
1-1	13601.9	0.0	0.0	3.8	0.0	0.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	4	Sx	93.1	0.0	0.0	93.1
1-1	si	5	Tz	-63.0	0.0	0.0	63.0

SOLLECITAZIONI : PROGR. 240.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	0.0	0.0	-490.3	0.0	-226.7
6-1	0.0	0.0	0.0	8.8	39.0	-226.7
1-1	0.0	0.0	0.0	3.8	0.0	-226.7

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-11.4	0.0	0.0	11.4
6-1	si	6	Tz	0.2	6.9	0.0	11.9
1-1	si	9	Ty	0.1	0.0	26.3	45.6
7-1	si	9	Si	-11.4	0.0	26.3	47.0

VERIFICA STABILITA` :

Caso 7-1 |LO = 240.0|Lc = 240.0|Ro = 3.6|Im= 67.1|
 Nodo 1 |om = 1.42|csz= 1.00|csy= 1.00|
 Infless. Y |Ncrz = 543125.2|Ncry= 197787.6|
|Nmax = -490.3|Mzeq= 11788.3|Myeq= 0.0|
|Ss = -71.0|

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 96
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	469.7	0.0	226.7
6-1	0.0	0.0	0.0	-8.4	-39.0	226.7
1-1	0.0	0.0	0.0	1.2	0.0	226.7

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	10.9	0.0	0.0	10.9
6-1	si	6	Tz	-0.2	-6.9	0.0	11.9
1-1	si	9	Ty	0.0	0.0	-26.3	45.6
8-1	si	9	Si	10.9	0.0	-26.3	46.9

SOLLECITAZIONI : PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	13601.9	2339.6	0.0	-8.4	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx Si	-93.1	0.0	0.0	93.1
6-1	si	5	Tz	-56.7	0.0	0.0	56.7

PROGR. 240.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
8-1		0.0		0.0	0.0	469.7	0.0 -226.7
6-1		0.0		0.0	0.0	-8.4	39.0 -226.7
1-1		0.0		0.0	0.0	1.2	0.0 -226.7

TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	10.9	0.0	0.0	10.9
6-1	si	6	Tz	-0.2	6.9	0.0	11.9
1-1	si	9	Ty	0.0	0.0	26.3	45.6
8-1	si	9	Si	10.9	0.0	26.3	46.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00
 Inflex. Y | Ncrz = 543125.2 | Ncry = 197787.6
 | Nmax = -8.4 | Mzeq = 11788.3 | Myeq = 2027.6
 | Ss = -80.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 97
 PROGR. 0.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
8-1		0.0		0.0	0.0	466.2	0.0 226.7
6-1		0.0		0.0	0.0	-8.8	-39.0 226.7
1-1		0.0		0.0	0.0	1.0	0.0 226.7

TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	10.9	0.0	0.0	10.9
6-1	si	6	Tz	-0.2	-6.9	0.0	11.9
1-1	si	9	Ty	0.0	0.0	-26.3	45.6
8-1	si	9	Si	10.9	0.0	-26.3	46.9

PROGR. 120.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
6-1		13601.9		2339.6	0.0	-8.8	0.0 0.0

TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx Si	-93.1	0.0	0.0	93.1
6-1	si	5	Tz	-56.7	0.0	0.0	56.7

PROGR. 240.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
8-1		0.0		0.0	0.0	466.2	0.0 -226.7
6-1		0.0		0.0	0.0	-8.8	39.0 -226.7
1-1		0.0		0.0	0.0	1.0	0.0 -226.7

TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx	10.9	0.0	0.0	10.9
6-1	si	6	Tz	-0.2	6.9	0.0	11.9
1-1	si	9	Ty	0.0	0.0	26.3	45.6
8-1	si	9	Si	10.9	0.0	26.3	46.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00
 Inflex. Y | Ncrz = 543125.2 | Ncry = 197787.6
 | Nmax = -8.8 | Mzeq = 11788.3 | Myeq = 2027.6
 | Ss = -80.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 98
 PROGR. 0.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
10-2		0.0		0.0	0.0	-858.5	0.0 226.7
6-1		0.0		0.0	0.0	-51.4	-39.0 226.7
1-1		0.0		0.0	0.0	-3.8	0.0 226.7

TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	-20.0	0.0	0.0	20.0
6-1	si	6	Tz	-1.2	-6.9	0.0	12.0
1-1	si	9	Ty	-0.1	0.0	-26.3	45.6
10-2	si	9	Si	-20.0	0.0	-26.3	49.8

PROGR. 120.00

SOLLECITAZIONI :							
Caso		MZ		MY	MT	N	TZ TY
6-1		13601.9		2339.6	0.0	-51.4	0.0 0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-94.1	0.0	0.0	94.1
6-1	si	5	Tz	-57.7	0.0	0.0	57.7

PROGR. 240.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-2	0.0	0.0	0.0	-858.5	0.0	-226.7
6-1	0.0	0.0	0.0	-51.4	39.0	-226.7
1-1	0.0	0.0	0.0	-3.8	0.0	-226.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-2	si	1	Sx	-20.0	0.0	0.0	20.0
6-1	si	6	Tz	-1.2	6.9	0.0	12.0
1-1	si	9	Ty	-0.1	0.0	26.3	45.6
10-2	si	9	Si	-20.0	0.0	26.3	49.8

VERIFICA STABILITA' :

Caso 10-2 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.01 |
 Infless. Y | Ncrz = 543125.2 | Ncry = 197787.6 |
 | Nmax = -858.5 | Mzeq = 11788.3 | Myeq = 0.0 |
 | Ss = -83.2

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 99
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-1	0.0	0.0	0.0	-4361.8	0.0	226.7
6-1	0.0	0.0	0.0	-22.2	-39.0	226.7
1-1	0.0	0.0	0.0	-10.1	0.0	226.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	Sx	-101.5	0.0	0.0	101.5
6-1	si	6	Tz	-0.5	-6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	-26.3	45.6
10-1	si	9	Si	-101.5	0.0	-26.3	111.3

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-1	13601.9	0.0	0.0	-4361.8	0.0	0.0
6-1	13601.9	2339.6	0.0	-22.2	0.0	0.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	Sx	-164.6	0.0	0.0	164.6
6-1	si	5	Tz	-57.0	0.0	0.0	57.0

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-1	0.0	0.0	0.0	-4361.8	0.0	-226.7
6-1	0.0	0.0	0.0	-22.2	39.0	-226.7
1-1	0.0	0.0	0.0	-10.1	0.0	-226.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	Sx	-101.5	0.0	0.0	101.5
6-1	si	6	Tz	-0.5	6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	26.3	45.6
10-1	si	9	Si	-101.5	0.0	26.3	111.3

VERIFICA STABILITA' :

Caso 10-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 1 | om = 1.42 | csz = 1.01 | csy = 1.03 |
 Infless. Y | Ncrz = 543125.2 | Ncry = 197787.6 |
 | Nmax = -4361.8 | Mzeq = 11788.3 | Myeq = 0.0 |
 | Ss = -199.6

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 100
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10-1	0.0	0.0	0.0	-546.4	0.0	226.7
6-1	0.0	0.0	0.0	-9.1	-39.0	226.7
1-1	0.0	0.0	0.0	-7.9	0.0	226.7

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	Sx	-12.7	0.0	0.0	12.7
6-1	si	6	Tz	-0.2	-6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	-26.3	45.6
10-1	si	9	Si	-12.7	0.0	-26.3	47.3

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	13601.9	2339.6	0.0	-9.1	0.0	0.0

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
6-1	si	2	Sx	-93.1	0.0	0.0	93.1
6-1	si	5	Tz	-56.7	0.0	0.0	56.7

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	-546.4	0.0	-226.7	
6-1	0.0	0.0	0.0	-9.1	39.0	-226.7	
1-1	0.0	0.0	0.0	-7.9	0.0	-226.7	

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
10-1	si	2	Sx	-12.7	0.0	0.0	12.7
6-1	si	6	Tz	-0.2	6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	26.3	45.6
10-1	si	9	Si	-12.7	0.0	26.3	47.3

VERIFICA STABILITA' :

Caso 6-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |
 Infless. Y

Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -9.1 | Mzeq = 11788.3 | Myeq = 2027.6 |
 Ss = -80.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 101
 PROGR. 0.00

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	-554.7	0.0	226.7	
6-1	0.0	0.0	0.0	-9.0	-39.0	226.7	
1-1	0.0	0.0	0.0	-7.7	0.0	226.7	

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
10-1	si	1	Sx	-12.9	0.0	0.0	12.9
6-1	si	6	Tz	-0.2	-6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	-26.3	45.6
10-1	si	9	Si	-12.9	0.0	-26.3	47.4

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
6-1	13601.9	2339.6	0.0	-9.0	0.0	0.0	

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
6-1	si	2	Sx	-93.1	0.0	0.0	93.1
6-1	si	5	Tz	-56.7	0.0	0.0	56.7

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	-554.7	0.0	-226.7	
6-1	0.0	0.0	0.0	-9.0	39.0	-226.7	
1-1	0.0	0.0	0.0	-7.7	0.0	-226.7	

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
10-1	si	1	Sx	-12.9	0.0	0.0	12.9
6-1	si	6	Tz	-0.2	6.9	0.0	11.9
1-1	si	9	Ty	-0.2	0.0	26.3	45.6
10-1	si	9	Si	-12.9	0.0	26.3	47.4

VERIFICA STABILITA' :

Caso 6-1 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |
 Infless. Y

Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -9.0 | Mzeq = 11788.3 | Myeq = 2027.6 |
 Ss = -80.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 102
 PROGR. 0.00

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	105.9	0.0	226.7	
6-1	0.0	0.0	0.0	6.4	-39.0	226.7	
1-1	0.0	0.0	0.0	0.5	0.0	226.7	

TENSIONI				Sx	Tz	Ty	Si
Caso	Ve	No	massimi				
8-1	si	1	Sx	2.5	0.0	0.0	2.5
6-1	si	6	Tz	0.1	-6.9	0.0	11.9
1-1	si	9	Ty	0.0	0.0	-26.3	45.6
8-1	si	9	Si	2.5	0.0	-26.3	45.7

SOLLECITAZIONI							PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
6-1	13601.9	2339.6	0.0	6.4	0.0	0.0	

1-1	13601.9	0.0	0.0	0.5	0.0	0.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
6-1	si	4	Sx	93.0	0.0	0.0
1-1	si	5	Tz	-63.1	0.0	0.0

PROGR. 240.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	105.9	0.0	-226.7
6-1	0.0	0.0	0.0	6.4	39.0	-226.7
1-1	0.0	0.0	0.0	0.5	0.0	-226.7

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	1	Sx	2.5	0.0	0.0
6-1	si	6	Tz	0.1	6.9	0.0
1-1	si	9	Ty	0.0	0.0	26.3
8-1	si	9	Si	2.5	0.0	26.3

VERIFICA STABILITA` :

Caso 8- 2 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |

Infless. Y

Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -93.2 | Mzeq = 11788.3 | Myeq = 0.0 |
 Ss = -57.8

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 103
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	113.0	0.0	226.7
6-1	0.0	0.0	0.0	6.5	-39.0	226.7
1-1	0.0	0.0	0.0	1.0	0.0	226.7

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	1	Sx	2.6	0.0	0.0
6-1	si	6	Tz	0.2	-6.9	0.0
1-1	si	9	Ty	0.0	0.0	-26.3
8-1	si	9	Si	2.6	0.0	-26.3

PROGR. 120.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
6-1	13601.9	2339.6	0.0	6.5	0.0	0.0

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
6-1	si	4	Sx	93.0	0.0	0.0
6-1	si	5	Tz	-56.3	0.0	0.0

PROGR. 240.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	0.0	0.0	0.0	113.0	0.0	-226.7
6-1	0.0	0.0	0.0	6.5	39.0	-226.7
1-1	0.0	0.0	0.0	1.0	0.0	-226.7

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	2	Sx	2.6	0.0	0.0
6-1	si	6	Tz	0.2	6.9	0.0
1-1	si	9	Ty	0.0	0.0	26.3
8-1	si	9	Si	2.6	0.0	26.3

VERIFICA STABILITA` :

Caso 8- 2 | L0 = 240.0 | Lc = 240.0 | Ro = 3.6 | Im = 67.1 |
 Nodo 2 | om = 1.42 | csz = 1.00 | csy = 1.00 |

Infless. Y

Ncrz = 543125.2 | Ncry = 197787.6 |
 Nmax = -99.2 | Mzeq = 11788.3 | Myeq = 0.0 |
 Ss = -58.0

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 118
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
6-1	0.0	0.0	0.0	-674.6	0.0	340.0
7-1	0.0	0.0	0.0	-4.4	66.2	340.0
1-1	0.0	0.0	0.0	-2.3	0.0	340.0

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
6-1	si	1	Sx	-15.7	0.0	0.0
7-1	si	5	Tz	-0.1	10.7	0.0
1-1	si	9	Ty	-0.1	0.0	-39.5
6-1	si	9	Si	-15.7	0.0	-39.5

PROGR. 180.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY

7-1	30604.2	-5954.9	0.0	-4.4	0.0	0.0
9-2	30604.2	0.0	0.0	-32.8	0.0	0.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	1	Sx	-217.9	0.0	0.0
7-1	si	5	Tz	-158.8	0.0	0.0
9-2	si	9	Ty	-0.8	0.0	0.0

PROGR. 360.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
6-1	0.0	0.0	0.0	-674.6	0.0	-340.0
7-1	0.0	0.0	0.0	-4.4	-66.2	-340.0
1-1	0.0	0.0	0.0	-2.3	0.0	-340.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
6-1	si	3	Sx	-15.7	0.0	0.0
7-1	si	5	Tz	-0.1	-10.7	0.0
1-1	si	9	Ty	-0.1	0.0	39.5
6-1	si	9	Si	-15.7	0.0	39.5

VERIFICA STABILITA` :

Caso 7-1 | LO = 360.0 | LC = 360.0 | Ro = 3.6 | Im = 100.6 |
 Nodo 1 | om = 2.02 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 241389.0 | Ncry = 87905.6 |
 | Nmax = -4.4 | Mzeq = 26523.7 | Myeq = -5160.9 |
 | Ss = -188.9

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 122
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9-2	0.0	0.0	0.0	5433.0	0.0	453.4
7-1	0.0	0.0	0.0	5.5	88.2	453.4
1-1	0.0	0.0	0.0	30.3	0.0	453.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
9-2	si	1	Sx	126.5	0.0	0.0
7-1	si	5	Tz	0.1	14.2	0.0
1-1	si	9	Ty	0.7	0.0	-52.7
9-2	si	9	Si	126.5	0.0	-52.7

PROGR. 240.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	54407.5	-10586.5	0.0	5.5	0.0	0.0
9-1	54407.5	0.0	0.0	-5372.4	0.0	0.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	3	Sx	387.3	0.0	0.0
9-1	si	5	Tz	-377.4	0.0	0.0

PROGR. 480.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9-2	0.0	0.0	0.0	5433.0	0.0	-453.4
7-1	0.0	0.0	0.0	5.5	-88.2	-453.4
1-1	0.0	0.0	0.0	30.3	0.0	-453.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
9-2	si	1	Sx	126.5	0.0	0.0
7-1	si	5	Tz	0.1	-14.2	0.0
1-1	si	9	Ty	0.7	0.0	52.7
9-2	si	9	Si	126.5	0.0	52.7

VERIFICA STABILITA` :

Caso 9-1 | LO = 480.0 | LC = 480.0 | Ro = 3.6 | Im = 134.2 |
 Nodo 1 | om = 2.93 | csz = 1.06 | csy = 1.19 |
 Infless. Y | Ncrz = 135781.3 | Ncry = 49446.9 |
 | Nmax = -5372.4 | Mzeq = 47153.2 | Myeq = 0.0 |
 | Ss = -598.6

P_HEB140_S004 (4) - metodo: tensioni ammissibili - ASTA 123
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
6-1	0.0	0.0	0.0	69.9	0.0	340.0
7-1	0.0	0.0	0.0	-4.4	66.2	340.0
1-1	0.0	0.0	0.0	-2.0	0.0	340.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
6-1	si	1	Sx	1.6	0.0	0.0
7-1	si	5	Tz	-0.1	10.7	0.0
1-1	si	9	Ty	0.0	0.0	-39.5
6-1	si	9	Si	1.6	0.0	-39.5

SOLLECITAZIONI :----- PROGR. 180.00

Caso	MZ	MY	MT	N	TZ	TY
7- 1	30604.2	-5954.9	0.0	-4.4	0.0	0.0
9- 1	30604.2	0.0	0.0	-12.7	0.0	0.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	1	Sx	-217.9	0.0	0.0	217.9
7- 1	si	5	Tz	-158.8	0.0	0.0	158.8
9- 1	si	9	Ty	-0.3	0.0	0.0	0.3

SOLLECITAZIONI :----- PROGR. 360.00

Caso	MZ	MY	MT	N	TZ	TY
6- 1	0.0	0.0	0.0	69.9	0.0	-340.0
7- 1	0.0	0.0	0.0	-4.4	-66.2	-340.0
1- 1	0.0	0.0	0.0	-2.0	0.0	-340.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	3	Sx	1.6	0.0	0.0	1.6
7- 1	si	5	Tz	-0.1	-10.7	0.0	18.5
1- 1	si	9	Ty	0.0	0.0	39.5	68.4
6- 1	si	9	Si	1.6	0.0	39.5	68.4

VERIFICA STABILITA' :

Caso 7- 1 | L0 = 360.0 | Lc = 360.0 | Ro = 3.6 | Im = 100.6 |
 Nodo 1 | om = 2.02 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 241389.0 | Ncry = 87905.6 |
 | Nmax = -4.4 | Mzeq = 26523.7 | Myeq = -5160.9 |
 Ss = -188.9

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 213
 PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8- 2	0.0	0.0	0.0	16501.1	-12.0	3571.5

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	1	Sx	258.8	0.0	0.0	258.8

SOLLECITAZIONI :----- PROGR. 60.00

Caso	MZ	MY	MT	N	TZ	TY
8- 2	165159.4	719.6	0.0	16501.1	-12.0	1933.8

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	18	Sx	720.9	0.0	0.0	720.9

SOLLECITAZIONI :----- PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
8- 2	232058.9	1439.1	0.0	16501.1	-12.0	296.2

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	18	Sx	911.3	0.0	0.0	911.3

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo 9 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y | Ncrz = 6459971.1 | Ncry = 924508.7 |
 | Nmax = -16452.0 | Mzeq = 193413.8 | Myeq = 1060.7 |
 Ss = -802.1

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 215
 PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8- 2	232058.9	1439.1	0.0	15393.1	19.4	296.2

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	18	Sx	894.0	0.0	0.0	894.0

SOLLECITAZIONI :----- PROGR. 60.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	200689.4	268.6	0.0	-17682.4	19.1	-1341.6

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	9	Sx	-798.8	0.0	0.0	798.8

SOLLECITAZIONI :----- PROGR. 120.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	71065.8	-877.1	0.0	-17682.4	19.1	-2979.2

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	8	Sx	-470.5	0.0	0.0	470.5

VERIFICA STABILITA' :

Caso 8- 1 | LO = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo 9 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y

Ncrz = 6459971.1 | Ncry = 924508.7 |
 Nmax = -17682.4 | Mzeq = 233423.9 | Myeq = 1060.7 |
 Ss = -927.6

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 216
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | 71065.8 | -877.1 | 0.0 | -17864.7 | -17.9 | -2979.2 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | si | 8 | Sx | Si | -473.4 | 0.0 | 0.0 | 473.4 |
 PROGR. 60.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | -156817.8 | 195.9 | 0.0 | -17864.7 | -17.9 | -4616.9 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | si | 17 | Sx | Si | -715.1 | 0.0 | 0.0 | 715.1 |
 PROGR. 120.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | -482961.5 | 1268.9 | 0.0 | -17864.7 | -17.9 | -6254.6 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | no | 17 | Sx | Si | -1624.8 | 0.0 | 0.0 | 1624.8 |
 tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)

VERIFICA STABILITA' :

Caso 8- 1 | LO = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo 17 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y

Ncrz = 6459971.1 | Ncry = 924508.7 |
 Nmax = -17864.7 | Mzeq = -362221.1 | Myeq = 951.7 |
 Ss = -1326.1

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 217
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | -488891.1 | 1268.4 | 0.0 | -19074.0 | 16.9 | 6552.6 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | no | 17 | Sx | Si | -1660.1 | 0.0 | 0.0 | 1660.1 |
 tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)
 PROGR. 60.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | -144862.3 | 255.1 | 0.0 | -19074.0 | 16.9 | 4915.0 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | si | 17 | Sx | Si | -701.5 | 0.0 | 0.0 | 701.5 |
 PROGR. 120.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | 100906.5 | -758.3 | 0.0 | -19074.0 | 16.9 | 3277.3 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 8- 1 | si | 8 | Sx | Si | -568.2 | 0.0 | 0.0 | 568.2 |

VERIFICA STABILITA' :

Caso 8- 1 | LO = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo 17 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y

Ncrz = 6459971.1 | Ncry = 924508.7 |
 Nmax = -19074.0 | Mzeq = -366668.3 | Myeq = 951.3 |
 Ss = -1360.0

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 219
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 8- 1 | 100906.5 | -758.3 | 0.0 | -19046.7 | -14.2 | 3277.3 |

TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |

| 8-1|si| 8|Sx Si| -567.7| 0.0| 0.0| 567.7|
 ----- PROGR. 60.00

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 248415.2 93.8 0.0 -19046.7 -14.2 1639.6
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 9|Sx Si| Sx Ty Si
 -941.6 0.0 0.0 941.6

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 297663.9 945.8 0.0 -19046.7 -14.2 2.0
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 9|Sx Si| Sx Ty Si
 -1078.2 0.0 0.0 1078.2

VERIFICA STABILITA' :

Caso 8-1 |L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 9 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -19046.7|Mzeq= 297663.9|Myeq= 709.4|
 Ss = -1114.5

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 221
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 297663.9 945.8 0.0 -19291.7 9.4 2.0
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 9|Sx Si| Sx Ty Si
 -1082.0 0.0 0.0 1082.0

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 248652.6 382.7 0.0 -19291.7 9.4 -1635.7
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 9|Sx Si| Sx Ty Si
 -949.2 0.0 0.0 949.2

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 101381.3 -180.3 0.0 -19291.7 9.4 -3273.4
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 8|Sx Si| Sx Ty Si
 -566.5 0.0 0.0 566.5

VERIFICA STABILITA' :

Caso 8-1 |L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 9 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -19291.7|Mzeq= 297663.9|Myeq= 709.4|
 Ss = -1118.9

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 222
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 101381.3 -180.3 0.0 -18819.3 1.0 -3273.4
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 8|Sx Si| Sx Ty Si
 -559.1 0.0 0.0 559.1

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 -144150.1 -242.2 0.0 -18819.3 1.0 -4911.0
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|si| 18|Sx Si| Sx Ty Si
 -695.4 0.0 0.0 695.4

SOLLECITAZIONI :
 Caso 8-1 MZ MY MT N TZ TY
 -487941.4 -304.1 0.0 -18819.3 1.0 -6548.7
 TENSIONI :
 Caso 8-1|Ve|No|massimi|
 8-1|no|18|Sx Si| Sx Ty Si
 -1646.0 0.0 0.0 1646.0

tenzione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tenzione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)

VERIFICA STABILITA' :

Caso 8-1 |L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|

Nodo18 | om = 1.12 | csz= 1.00 | csy= 1.03 |
 Infless. Y | Ncrz = 6459971.1 | Ncry= 924508.7 |
 | Nmax = -18819.3 | Mzeq= -365956.1 | Myeq= -304.1 |
 Ss = -1348.3

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 223
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 -482120.4 -303.8 0.0 -17781.1 -12.3 6252.2
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 1|no|18|Sx Si -1613.6 0.0 0.0 1613.6
 tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)

PROGR. 60.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 -156116.9 431.7 0.0 -17781.1 -12.3 4614.6
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 1|si|17|Sx Si -713.7 0.0 0.0 713.7

PROGR. 120.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 71626.5 1167.2 0.0 -17781.1 -12.3 2976.9
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 1|si|9|Sx Si -476.7 0.0 0.0 476.7

VERIFICA STABILITA` :

Caso 8- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.2 | Im= 37.8 |
 Nodo17 | om = 1.12 | csz= 1.00 | csy= 1.03 |
 Infless. Y | Ncrz = 6459971.1 | Ncry= 924508.7 |
 | Nmax = -17781.1 | Mzeq= -361590.3 | Myeq= 875.4 |
 Ss = -1322.3

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 225
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 71626.5 1167.2 0.0 -17018.9 9.5 2976.9
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 1|si|9|Sx Si -464.7 0.0 0.0 464.7

PROGR. 60.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 201063.0 630.6 0.0 16038.1 10.0 1339.5
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 2|si|18|Sx Si 812.1 0.0 0.0 812.1

PROGR. 120.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 232302.0 32.1 0.0 16038.1 10.0 -298.2
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 2|si|18|Sx Si 893.8 0.0 0.0 893.8

VERIFICA STABILITA` :

Caso 8- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.2 | Im= 37.8 |
 Nodo 9 | om = 1.12 | csz= 1.00 | csy= 1.03 |
 Infless. Y | Ncrz = 6459971.1 | Ncry= 924508.7 |
 | Nmax = -17018.9 | Mzeq= 233739.3 | Myeq= 875.4 |
 Ss = -914.6

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 226
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 232302.0 32.1 0.0 16643.4 0.3 -298.2
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si
 8- 2|si|18|Sx Si 903.3 0.0 0.0 903.3

PROGR. 60.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 165281.0 16.0 0.0 16643.4 0.3 -1935.9
 TENSIONI :
 Caso|Ve|No|massimi Sx Tz Ty Si

| 8- 2|si|18|Sx Si | 717.9| 0.0| 0.0| 717.9|
 ----- PROGR. 120.00

SOLLECITAZIONI :
 Caso 8- 2 MZ 0.0 MY 0.0 MT 0.0 N 16643.4 TZ 0.3 TY -3573.5
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si| 8|Sx Si | 261.1| 0.0| 0.0| 261.1|

VERIFICA STABILITA' :

Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 9 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -16328.1|Mzeq= 193596.0|Myeq= 19.6|
 Ss = -788.7

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 227
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 8- 2 MZ 0.0 MY 0.0 MT 0.0 N 17841.9 TZ 17.2 TY 3791.8
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si| 1|Sx Si | 279.9| 0.0| 0.0| 279.9|

SOLLECITAZIONI :
 Caso 8- 2 MZ 175255.3 MY -1029.4 MT 0.0 N 17841.9 TZ 17.2 TY 2050.1
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si|17|Sx Si | 772.2| 0.0| 0.0| 772.2|

SOLLECITAZIONI :
 Caso 8- 2 MZ 246008.1 MY -2058.9 MT 0.0 N 17841.9 TZ 17.2 TY 308.4
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si|17|Sx Si | 975.7| 0.0| 0.0| 975.7|

VERIFICA STABILITA' :

Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 8 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -17833.4|Mzeq= 205192.1|Myeq= -465.9|
 Ss = -850.4

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 229
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 8- 2 MZ 246008.1 MY -2058.9 MT 0.0 N 15507.9 TZ -20.0 TY 308.4
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si|17|Sx Si | 939.1| 0.0| 0.0| 939.1|

SOLLECITAZIONI :
 Caso 8- 2 MZ 212258.5 MY -857.0 MT 0.0 N 15507.9 TZ -20.0 TY -1433.3
 TENSIONI :
 Caso 8- 2|Ve|No|massimi| Sx Ty Si
 8- 2|si|17|Sx Si | 836.5| 0.0| 0.0| 836.5|

SOLLECITAZIONI :
 Caso 8- 1 MZ 74014.0 MY 332.9 MT 0.0 N -17524.4 TZ -8.0 TY -3175.0
 TENSIONI :
 Caso 8- 1|Ve|No|massimi| Sx Ty Si
 8- 1|si| 9|Sx Si | -469.7| 0.0| 0.0| 469.7|

VERIFICA STABILITA' :

Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 8 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -17524.4|Mzeq= 247372.0|Myeq= -465.9|
 Ss = -954.3

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 230
 ----- PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	74014.0	332.9	0.0	-18334.4	-0.6	-3175.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	9	Si	-482.5	0.0	0.0

PROGR.						60.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	-168738.6	369.3	0.0	-18334.4	-0.6	-4916.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	17	Si	-756.8	0.0	0.0

PROGR.						120.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	-515993.6	405.6	0.0	-18334.4	-0.6	-6658.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	no	17	Si	-1716.7	0.0	0.0

tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.)						
tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)						

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo17 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y

Ncrz = 6459971.1 | Ncry = 924508.7 |
 Nmax = -18334.4 | Mzeq = -386995.2 | Myeq = 405.6 |
 Ss = -1398.8

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 231
 PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	-522043.4	406.2	0.0	-19117.5	12.0	6969.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	no	17	Si	-1745.7	0.0	0.0

tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.)						
tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)						

PROGR.						60.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	-156119.4	-314.6	0.0	-19117.5	12.0	5227.9
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	18	Si	-733.8	0.0	0.0

PROGR.						120.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	105302.3	-1035.3	0.0	-19117.5	12.0	3486.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	8	Si	-583.2	0.0	0.0

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 120.0 | Lc = 120.0 | Ro = 3.2 | Im = 37.8 |
 Nodo18 | om = 1.12 | csz = 1.00 | csy = 1.03 |
 Infless. Y

Ncrz = 6459971.1 | Ncry = 924508.7 |
 Nmax = -19117.5 | Mzeq = -391532.6 | Myeq = -776.5 |
 Ss = -1428.3

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 233
 PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	105302.3	-1035.3	0.0	-19164.6	-15.4	3486.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	8	Si	-584.0	0.0	0.0

PROGR.						60.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	262221.5	-111.8	0.0	-19164.6	-15.4	1744.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	8	Si	-979.4	0.0	0.0

PROGR.						120.00

Caso	MZ	MY	MT	N	TZ	TY
8-1	314638.3	811.6	0.0	-19164.6	-15.4	2.8
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	8	Si			

| 8- 1|si| 9|Sx Si| -1122.4| 0.0| 0.0| 1122.4|

VERIFICA STABILITA` :

Caso 8- 1 | L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 8 | om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y | Ncrz = 6459971.1|Ncry= 924508.7|
 | Nmax = -19164.6|Mzeq= 314638.3|Myeq= -776.5|
 Ss = -1161.4

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 235
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | 314638.3 | 811.6 | 0.0 | -19120.8 | 16.4 | 2.8
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|si| 9|Sx Si| -1121.7 | Tz 0.0 | Ty 0.0 | Si 1121.7

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | 262552.7 | -175.0 | 0.0 | -19120.8 | 16.4 | -1738.9
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|si| 8|Sx Si| -980.2 | Tz 0.0 | Ty 0.0 | Si 980.2

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | 105964.6 | -1161.7 | 0.0 | -19120.8 | 16.4 | -3480.7
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|si| 8|Sx Si| -586.4 | Tz 0.0 | Ty 0.0 | Si 586.4

VERIFICA STABILITA` :

Caso 8- 1 | L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 8 | om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y | Ncrz = 6459971.1|Ncry= 924508.7|
 | Nmax = -19120.8|Mzeq= 314638.3|Myeq= -871.3|
 Ss = -1161.7

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 236
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | 105964.6 | -1161.7 | 0.0 | -18771.0 | -15.7 | -3480.7
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|si| 8|Sx Si| -580.9 | Tz 0.0 | Ty 0.0 | Si 580.9

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | -155125.9 | -221.9 | 0.0 | -18771.0 | -15.7 | -5222.4
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|si| 18|Sx Si| -724.9 | Tz 0.0 | Ty 0.0 | Si 724.9

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | -520718.8 | 717.9 | 0.0 | -18771.0 | -15.7 | -6964.1
 TENSIONI :
 Caso|Ve|No|massimi :
 8- 1|no| 17|Sx Si| -1739.1 | Tz 0.0 | Ty 0.0 | Si 1739.1
 tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)

VERIFICA STABILITA` :

Caso 8- 1 | L0 = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo18 | om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y | Ncrz = 6459971.1|Ncry= 924508.7|
 | Nmax = -18771.0|Mzeq= -390539.1|Myeq= -871.3|
 Ss = -1420.2

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 237
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ : MY | MT | N | TZ | TY
 8- 1 | -514838.6 | 717.3 | 0.0 | -17938.7 | 15.7 | 6655.2
 TENSIONI :
 Caso|Ve|No|massimi :
 Sx | Tz | Ty | Si |

| 8- 1|no|17|Sx |Si| -1709.7| 0.0| 0.0| 1709.7|
 tensione normale "Sx" > Sigma ammissibile ("Sx" < Samm. magg.
 tensione ideale "Si" > Sigma ammissibile ("Si" < Samm. magg.)

PROGR. 60.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 -167776.1 -226.2 0.0 -17938.7 15.7 4913.5
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 1|si|18|Sx Si -746.8 0.0 0.0 746.8
 PROGR. 120.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 74784.0 -1169.7 0.0 -17938.7 15.7 3171.8
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 1|si| 8|Sx Si -487.4 0.0 0.0 487.4

VERIFICA STABILITA' :
 Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo18 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -17938.7|Mzeq= -386129.0|Myeq= -877.2|
 Ss = -1393.2

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 239
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 1 74784.0 -1169.7 0.0 -17011.5 -9.6 3171.8
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 1|si| 8|Sx Si -472.8 0.0 0.0 472.8
 PROGR. 60.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 212841.7 -625.4 0.0 16107.5 -10.8 1430.1
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 2|si|17|Sx Si 845.7 0.0 0.0 845.7
 PROGR. 120.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 246396.9 25.0 0.0 16107.5 -10.8 -311.6
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 2|si|18|Sx Si 933.8 0.0 0.0 933.8

VERIFICA STABILITA' :
 Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|
 Nodo 8 |om = 1.12|csz= 1.00|csy= 1.03|
 Infless. Y
 Ncrz = 6459971.1|Ncry= 924508.7|
 Nmax = -17011.5|Mzeq= 247805.1|Myeq= -877.2|
 Ss = -951.0

U_HEB140+T100 (10) - metodo: tensioni ammissibili - ASTA 240
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 246396.9 25.0 0.0 16621.1 0.2 -311.6
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 2|si|18|Sx Si 941.8 0.0 0.0 941.8
 PROGR. 60.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 175449.7 12.5 0.0 16621.1 0.2 -2053.3
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 2|si| 8|Sx Si 745.7 0.0 0.0 745.7
 PROGR. 120.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 8- 2 0.0 0.0 0.0 16621.1 0.2 -3795.0
 TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 8- 2|si| 8|Sx Si 260.7 0.0 0.0 260.7

VERIFICA STABILITA' :
 Caso 8- 1 |LO = 120.0|Lc = 120.0|Ro = 3.2 |Im= 37.8|

Nodo 8 |om = 1.12|csz= 1.00|csy= 1.03|
 Inflex. Y |Ncrz = 6459971.1|Ncry= 924508.7|
 |Nmax = -16330.9|Mzeq= 205442.3|Myeq= -15.3|
 |Ss = -819.4

VERIFICA ELEMENTI IN ACCIAIO
 lavoro : SCIPR3

Unita` di misura : Kgf ; cm ; Kgf/cmq ; Kgf*cm

MATERIALI
 Fe430: Mod.El.= 2100000.; Samm= 1900.(1700. per sp>40 mm)

CASI DI CARICO

N	Descrizione	Soll.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

CARATTERISTICHE GEOMETRICHE

CIRCOLARE_S007 (7) :
 A = 7.0596E+00 Jz= 3.9660E+00 Jy= 3.9660E+00 Jt= 7.9522E+00
 Diam= 3.0

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 160
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 7084.0 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1003.5 | 0.0 | 0.0 | 1003.5 |

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 7084.0 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1003.5 | 0.0 | 0.0 | 1003.5 |

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 7084.0 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1003.5 | 0.0 | 0.0 | 1003.5 |

VERIFICA STABILITA` :

Caso10- 2 |L0 = 398.4|Lc = 0.0|Ro = 0.7 |Im= 0.0|
 Nodo 1 |om = 1.00|csz= 1.00|csy= 1.00|
 Inflex. Y |Ncrz = Infinity|Ncry= Infinity|
 |Nmax = -6975.6|Mzeq= 0.0|Myeq= 0.0|
 |Ss = -988.1

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 161
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 13092.2 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1854.5 | 0.0 | 0.0 | 1854.5 |

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 13092.2 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1854.5 | 0.0 | 0.0 | 1854.5 |

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 0.0 | 0.0 | 0.0 | 13092.2 | 0.0 | 0.0 |

TENSIONI :
 Caso|Ve|No|massimi | Sx | Ty | Si |
 10- 1|si | 1|Sx | Si | 1854.5 | 0.0 | 0.0 | 1854.5 |

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	si	1854.5	0.0	0.0	1854.5

VERIFICA STABILITA` :

Caso 10- 2 | L0 = 380.3 | Lc = 0.0 | Ro = 0.7 | lm = 0.0
 Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00
 Infless. Y

| Ncrz = Infinity | Ncry = Infinity
 | Nmax = -13086.6 | Mzeq = 0.0 | Myeq = 0.0
 Ss = -1853.7

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 162
 PROGR. 0.00

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1996.8	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	282.9	0.0	0.0	282.9

PROGR. 190.15

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1996.8	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	282.9	0.0	0.0	282.9

PROGR. 380.30

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1996.8	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	282.9	0.0	0.0	282.9

VERIFICA STABILITA` :

Caso 8- 2 | L0 = 380.3 | Lc = 0.0 | Ro = 0.7 | lm = 0.0
 Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00
 Infless. Y

| Ncrz = Infinity | Ncry = Infinity
 | Nmax = -1991.8 | Mzeq = 0.0 | Myeq = 0.0
 Ss = -282.1

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 163
 PROGR. 0.00

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1908.6	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	270.4	0.0	0.0	270.4

PROGR. 199.20

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1908.6	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	270.4	0.0	0.0	270.4

PROGR. 398.40

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1908.6	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	si	270.4	0.0	0.0	270.4

VERIFICA STABILITA` :

Caso 8- 2 | L0 = 398.4 | Lc = 0.0 | Ro = 0.7 | lm = 0.0
 Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00
 Infless. Y

| Ncrz = Infinity | Ncry = Infinity
 | Nmax = -1801.1 | Mzeq = 0.0 | Myeq = 0.0
 Ss = -255.1

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 164
 PROGR. 0.00

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	7929.6	0.0	0.0	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	1	si	1123.2	0.0	0.0	1123.2

PROGR. 223.03

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	7929.6	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1123.2	0.0	0.0	1123.2
							PROGR. 446.07

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	7929.6	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1123.2	0.0	0.0	1123.2

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	13240.4	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1875.5	0.0	0.0	1875.5
							PROGR. 168.65

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	13240.4	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1875.5	0.0	0.0	1875.5
							PROGR. 337.30

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	13240.4	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1875.5	0.0	0.0	1875.5

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	13240.4	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	1875.5	0.0	0.0	1875.5

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2
							PROGR. 168.65

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2
							PROGR. 337.30

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2

SOLLECITAZIONI							:
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1992.2	0.0	0.0	
TENSIONI							:
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	282.2	0.0	0.0	282.2

Ss = -281.4

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 167
PROGR. 0.00

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2007.2 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 284.3 | Tz 0.0 | Ty 0.0 | Si 284.3 |
PROGR. 223.03

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2007.2 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 284.3 | Tz 0.0 | Ty 0.0 | Si 284.3 |
PROGR. 446.07

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2007.2 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 284.3 | Tz 0.0 | Ty 0.0 | Si 284.3 |

VERIFICA STABILITA' :

Caso 8-2 | L0 = 446.1 | Lc = 0.0 | Ro = 0.7 | Im = 0.0 |
Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
Inflless. Y | Ncrz = Infinity | Ncry = Infinity | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -1885.3 | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -267.1

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 168
PROGR. 0.00

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2338.7 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 331.3 | Tz 0.0 | Ty 0.0 | Si 331.3 |
PROGR. 223.03

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2338.7 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 331.3 | Tz 0.0 | Ty 0.0 | Si 331.3 |
PROGR. 446.07

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 2338.7 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 331.3 | Tz 0.0 | Ty 0.0 | Si 331.3 |

VERIFICA STABILITA' :

Caso 8-2 | L0 = 446.1 | Lc = 0.0 | Ro = 0.7 | Im = 0.0 |
Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
Inflless. Y | Ncrz = Infinity | Ncry = Infinity | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -2335.5 | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -330.8

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 169
PROGR. 0.00

SOLLECITAZIONI :
Caso 10-1 MZ 0.0 MY 0.0 MT 0.0 N 5954.3 TZ 0.0 TY 0.0
TENSIONI :
Caso 10-1 | Ve | No | massimi |
10-1 | si | 1 | Sx | Si | Sx 843.4 | Tz 0.0 | Ty 0.0 | Si 843.4 |
PROGR. 223.03

SOLLECITAZIONI :
Caso 10-1 MZ 0.0 MY 0.0 MT 0.0 N 5954.3 TZ 0.0 TY 0.0
TENSIONI :
Caso 10-1 | Ve | No | massimi |
10-1 | si | 1 | Sx | Si | Sx 843.4 | Tz 0.0 | Ty 0.0 | Si 843.4 |
PROGR. 446.07

SOLLECITAZIONI :
Caso 10-1 MZ 0.0 MY 0.0 MT 0.0 N 5954.3 TZ 0.0 TY 0.0
TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	843.4	0.0	0.0	843.4

VERIFICA STABILITA' :

Caso10-2	LO = 446.1	LC = 0.0	Ro = 0.7	lm = 0.0
Nodo 1	om = 1.00	csz = 1.00	csy = 1.00	
Influss. Y	Ncrz = Infinity	Ncry = Infinity	Mz = 0.0	Myeq = 0.0
	Nmax = -5950.9	Mz = 0.0		
	Ss = -843.0			

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 170
PROGR. 0.00

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	2299.8	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	325.8	0.0	0.0	325.8

PROGR. 199.20

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	2299.8	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	325.8	0.0	0.0	325.8

PROGR. 398.40

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	2299.8	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	325.8	0.0	0.0	325.8

VERIFICA STABILITA' :

Caso 8-2	LO = 398.4	LC = 0.0	Ro = 0.7	lm = 0.0
Nodo 1	om = 1.00	csz = 1.00	csy = 1.00	
Influss. Y	Ncrz = Infinity	Ncry = Infinity	Mz = 0.0	Myeq = 0.0
	Nmax = -2296.1	Mz = 0.0		
	Ss = -325.2			

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 171
PROGR. 0.00

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	4897.9	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	693.8	0.0	0.0	693.8

PROGR. 199.20

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	4897.9	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	693.8	0.0	0.0	693.8

PROGR. 398.40

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
10-1	0.0	0.0	0.0	4897.9	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	1	1	1	693.8	0.0	0.0	693.8

VERIFICA STABILITA' :

Caso10-2	LO = 398.4	LC = 0.0	Ro = 0.7	lm = 0.0
Nodo 1	om = 1.00	csz = 1.00	csy = 1.00	
Influss. Y	Ncrz = Infinity	Ncry = Infinity	Mz = 0.0	Myeq = 0.0
	Nmax = -4894.8	Mz = 0.0		
	Ss = -693.3			

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 172
PROGR. 0.00

SOLLECITAZIONI							
Caso	MZ	MY	MT	N	TZ	TY	
8-1	0.0	0.0	0.0	1619.0	0.0	0.0	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	1	1	1	229.3	0.0	0.0	229.3

PROGR. 304.87

SOLLECITAZIONI :
 Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1619.0 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 8-1 No massimi : SX 229.3 TZ 0.0 Ty 0.0 Si 229.3
 8-1 si 1 Sx Si

PROGR. 609.73

SOLLECITAZIONI :
 Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1619.0 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 8-1 No massimi : SX 229.3 TZ 0.0 Ty 0.0 Si 229.3
 8-1 si 1 Sx Si

VERIFICA STABILITA` :

Caso 8-2 |LO = 609.7|Lc = 0.0|Ro = 0.7|Im= 0.0|
 Nodo 1 |om = 1.00|csz= 1.00|csy= 1.00|
 Inflex. y
 |Ncrz = Infinity|Ncry= Infinity|
 |Nmax = -1619.0|Mzeq= 0.0|Myeq= 0.0|
 Ss = -229.3

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 173
 PROGR. 0.00

SOLLECITAZIONI :
 Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6933.0 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 9-1 No massimi : SX 982.1 TZ 0.0 Ty 0.0 Si 982.1
 9-1 si 1 Sx Si

PROGR. 304.87

SOLLECITAZIONI :
 Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6933.0 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 9-1 No massimi : SX 982.1 TZ 0.0 Ty 0.0 Si 982.1
 9-1 si 1 Sx Si

PROGR. 609.73

SOLLECITAZIONI :
 Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6933.0 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 9-1 No massimi : SX 982.1 TZ 0.0 Ty 0.0 Si 982.1
 9-1 si 1 Sx Si

VERIFICA STABILITA` :

Caso 9-2 |LO = 609.7|Lc = 0.0|Ro = 0.7|Im= 0.0|
 Nodo 1 |om = 1.00|csz= 1.00|csy= 1.00|
 Inflex. y
 |Ncrz = Infinity|Ncry= Infinity|
 |Nmax = -6933.5|Mzeq= 0.0|Myeq= 0.0|
 Ss = -981.8

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 174
 PROGR. 0.00

SOLLECITAZIONI :
 Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1748.6 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 8-1 No massimi : SX 247.7 TZ 0.0 Ty 0.0 Si 247.7
 8-1 si 1 Sx Si

PROGR. 280.92

SOLLECITAZIONI :
 Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1748.6 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 8-1 No massimi : SX 247.7 TZ 0.0 Ty 0.0 Si 247.7
 8-1 si 1 Sx Si

PROGR. 561.84

SOLLECITAZIONI :
 Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1748.6 TZ 0.0 TY 0.0
 TENSIONI :
 Caso 8-1 No massimi : SX 247.7 TZ 0.0 Ty 0.0 Si 247.7
 8-1 si 1 Sx Si

VERIFICA STABILITA` :

Caso 8-2 |LO = 561.8|Lc = 0.0|Ro = 0.7|Im= 0.0|
 Nodo 1 |om = 1.00|csz= 1.00|csy= 1.00|
 Inflex. y
 |Ncrz = Infinity|Ncry= Infinity|
 |Nmax = -1748.6|Mzeq= 0.0|Myeq= 0.0|

Ss = -247.7

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 175
PROGR. 0.00

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6299.1 TZ 0.0 TY 0.0
TENSIONI :
Caso 9-1 | Ve | No | massimi |
9-1 | si | 1 | Sx | Si | Sx 892.3 Ty 0.0 Si 892.3

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6299.1 TZ 0.0 TY 0.0
TENSIONI :
Caso 9-1 | Ve | No | massimi |
9-1 | si | 1 | Sx | Si | Sx 892.3 Ty 0.0 Si 892.3

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 6299.1 TZ 0.0 TY 0.0
TENSIONI :
Caso 9-1 | Ve | No | massimi |
9-1 | si | 1 | Sx | Si | Sx 892.3 Ty 0.0 Si 892.3

VERIFICA STABILITA` :

Caso 9- 2 | LO = 561.8 | Lc = 0.0 | Ro = 0.7 | lm= 0.0 |
Nodo 1 | om = 1.00 | csz= 1.00 | csy= 1.00 |
Influss. Y
NCRZ = Infinity | Ncry= Infinity |
Nmax = -6299.1 | Mzeq= 0.0 | Myeq= 0.0 |
Ss = -892.3

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 176
PROGR. 0.00

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1612.8 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 228.4 Ty 0.0 Si 228.4

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1612.8 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 228.4 Ty 0.0 Si 228.4

SOLLECITAZIONI :
Caso 8-1 MZ 0.0 MY 0.0 MT 0.0 N 1612.8 TZ 0.0 TY 0.0
TENSIONI :
Caso 8-1 | Ve | No | massimi |
8-1 | si | 1 | Sx | Si | Sx 228.4 Ty 0.0 Si 228.4

VERIFICA STABILITA` :

Caso 8- 2 | LO = 609.7 | Lc = 0.0 | Ro = 0.7 | lm= 0.0 |
Nodo 1 | om = 1.00 | csz= 1.00 | csy= 1.00 |
Influss. Y
NCRZ = Infinity | Ncry= Infinity |
Nmax = -1612.8 | Mzeq= 0.0 | Myeq= 0.0 |
Ss = -228.4

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 177
PROGR. 0.00

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 7683.2 TZ 0.0 TY 0.0
TENSIONI :
Caso 9-1 | Ve | No | massimi |
9-1 | si | 1 | Sx | Si | Sx 1088.3 Ty 0.0 Si 1088.3

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 7683.2 TZ 0.0 TY 0.0
TENSIONI :
Caso 9-1 | Ve | No | massimi |
9-1 | si | 1 | Sx | Si | Sx 1088.3 Ty 0.0 Si 1088.3

SOLLECITAZIONI :
Caso 9-1 MZ 0.0 MY 0.0 MT 0.0 N 7683.2 TZ 0.0 TY 0.0
TENSIONI :

Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
9- 1|si| 1|Sx | Si | 1088.3 | 0.0 | 0.0 | 1088.3 |

VERIFICA STABILITA` :

Caso 9- 2 | LO = 609.7 | LC = 0.0 | RO = 0.7 | lm = 0.0 |
Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
Influss. Y
Ncrz = Infinity | Ncry = Infinity |
Nmax = -7681.1 | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -1088.0

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 178
PROGR. 0.00

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
8- 1 0.0 0.0 0.0 1755.3 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
8- 1|si| 1|Sx | Si | 248.6 | 0.0 | 0.0 | 248.6 |

PROGR. 280.92

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
8- 1 0.0 0.0 0.0 1755.3 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
8- 1|si| 1|Sx | Si | 248.6 | 0.0 | 0.0 | 248.6 |

PROGR. 561.84

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
8- 1 0.0 0.0 0.0 1755.3 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
8- 1|si| 1|Sx | Si | 248.6 | 0.0 | 0.0 | 248.6 |

VERIFICA STABILITA` :

Caso 8- 2 | LO = 561.8 | LC = 0.0 | RO = 0.7 | lm = 0.0 |
Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
Influss. Y
Ncrz = Infinity | Ncry = Infinity |
Nmax = -1755.3 | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -248.6

CIRCOLARE_S007 (7) - metodo: tensioni ammissibili - ASTA 179
PROGR. 0.00

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
9- 1 0.0 0.0 0.0 6785.5 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
9- 1|si| 1|Sx | Si | 961.2 | 0.0 | 0.0 | 961.2 |

PROGR. 280.92

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
9- 1 0.0 0.0 0.0 6785.5 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
9- 1|si| 1|Sx | Si | 961.2 | 0.0 | 0.0 | 961.2 |

PROGR. 561.84

SOLLECITAZIONI :
Caso MZ : MY MT N TZ TY
9- 1 0.0 0.0 0.0 6785.5 0.0 0.0

TENSIONI :
Caso|Ve|No|massimi | Sx | Tz | Ty | Si |
9- 1|si| 1|Sx | Si | 961.2 | 0.0 | 0.0 | 961.2 |

VERIFICA STABILITA` :

Caso 9- 2 | LO = 561.8 | LC = 0.0 | RO = 0.7 | lm = 0.0 |
Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
Influss. Y
Ncrz = Infinity | Ncry = Infinity |
Nmax = -6785.5 | Mzeq = 0.0 | Myeq = 0.0 |
Ss = -961.2

VERIFICA ELEMENTI IN ACCIAIO
lavoro : SCIPR3

Unita` di misura : Kgf ; cm ; Kgf/cm² ; Kgf*cm

MATERIALI
Fe360: Mod.El.= 2100000.; Samm= 1600.(1400. per sp>40 mm)

CASI DI CARICO

N	Descrizione	Soil.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

CARATTERISTICHE GEOMETRICHE

P_HEB120_S003 (3) :
 A = 34.0119E+00 Jz=864.4877E+00 Jy=317.5257E+00 Jt= 10.9301E+00

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 10
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-124095.5	-139.9	0.0	-1345.8	-0.4	551.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-903.5	0.0	0.0	903.5
6- 1	si	6	Tz	822.4	-15.6	0.0	822.8
6- 1	si	9	Ty	-39.7	0.0	-81.1	145.9

PROGR. 159.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-48920.0	-70.0	0.0	-1303.4	-0.4	394.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-379.2	0.0	0.0	379.2
6- 1	si	6	Tz	301.5	-11.1	0.0	302.2
6- 1	si	9	Ty	-38.4	0.0	-58.0	107.5

PROGR. 318.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	1275.6	0.0	0.0	-1260.9	-0.4	237.1

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	2	Sx	-45.9	0.0	0.0	45.9
6- 1	si	6	Tz	-45.9	-6.7	0.0	47.4
6- 1	si	9	Ty	-37.1	0.0	-34.9	70.9
6- 1	si	11	Si	-42.5	0.0	-33.0	71.2

VERIFICA STABILITA` :

Caso 6- 1 | L0 = 318.0 | Lc = 222.6 | Ro = 3.1 | Im = 72.9 |
 Nodo 4 | om = 1.51 | csz = 1.01 | csy = 1.02 |
 Inflex. Y

Ncrz = 361599.3 | Ncry = 132815.1 |
 Nmax = -1345.8 | Mzeq = -93071.7 | Myeq = -104.9 |
 Ss = -711.2

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 11
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-124116.9	-148.3	0.0	-1345.8	-0.5	551.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-903.8	0.0	0.0	903.8
6- 1	si	6	Tz	822.6	-15.6	0.0	823.0
6- 1	si	9	Ty	-39.7	0.0	-81.1	145.9

PROGR. 159.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-48941.4	-74.1	0.0	-1303.4	-0.5	394.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-379.4	0.0	0.0	379.4
6- 1	si	6	Tz	301.7	-11.1	0.0	302.3
6- 1	si	9	Ty	-38.4	0.0	-58.0	107.5

PROGR. 318.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	1254.2	0.0	0.0	-1260.9	-0.5	237.1

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	1	Sx	-45.8	0.0	0.0	45.8
6- 1	si	6	Tz	-45.8	-6.7	0.0	47.2
6- 1	si	9	Ty	-37.1	0.0	-34.9	70.9
6- 1	si	11	Si	-42.4	0.0	-33.0	71.2

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 318.0 | Lc = 222.6 | Ro = 3.1 | Im = 72.9 |
 Nodo 4 | om = 1.51 | csz = 1.01 | csy = 1.02 |
 Influss. Y | Ncrz = 361599.3 | Ncry = 132815.1 |
 | Nmax = -1345.8 | Mzeq = -93087.7 | Myeq = -111.2 |
 | Ss = -711.5

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 12
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-124123.2	-41.1	0.0	-1385.2	-0.1	551.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-903.0	0.0	0.0	903.0
6- 1	si	6	Tz	821.0	-15.6	0.0	821.4
6- 1	si	9	Ty	-40.8	0.0	-81.1	146.2

PROGR. 159.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-48947.7	-20.6	0.0	-1342.7	-0.1	394.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-379.6	0.0	0.0	379.6
6- 1	si	6	Tz	300.3	-11.1	0.0	301.0
6- 1	si	9	Ty	-39.5	0.0	-58.0	107.9
6- 1	si	7	Si	-379.3	-11.1	0.0	379.8

PROGR. 318.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10- 2	9.0	0.0	0.0	-5885.5	-16.9	0.0
6- 1	1247.9	0.0	0.0	-1300.3	-0.1	237.1

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10- 2	si	2	Sx	-173.1	0.0	0.0	173.1
6- 1	si	6	Tz	-46.9	-6.7	0.0	48.3
6- 1	si	9	Ty	-38.2	0.0	-34.9	71.5
10- 2	si	6	Si	-173.1	-0.9	0.0	173.1

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 318.0 | Lc = 222.6 | Ro = 3.1 | Im = 72.9 |
 Nodo 4 | om = 1.51 | csz = 1.01 | csy = 1.02 |
 Influss. Y | Ncrz = 361599.3 | Ncry = 132815.1 |
 | Nmax = -1385.2 | Mzeq = -93092.4 | Myeq = -30.9 |
 | Ss = -711.8

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 13
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-124118.5	174.6	0.0	-1345.8	0.5	551.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	3	Sx	-904.3	0.0	0.0	904.3
6- 1	si	5	Tz	822.7	15.6	0.0	823.2
6- 1	si	9	Ty	-39.4	0.0	-81.1	145.8

PROGR. 159.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-48942.9	87.3	0.0	-1303.4	0.5	394.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	3	Sx	-379.7	0.0	0.0	379.7
6- 1	si	5	Tz	301.8	11.2	0.0	302.4
6- 1	si	9	Ty	-38.2	0.0	-58.0	107.4

PROGR. 318.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	1252.7	0.0	0.0	-1260.9	0.5	237.1

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	2	Sx	-45.8	0.0	0.0	45.8
6- 1	si	5	Tz	-45.8	6.7	0.0	47.2
6- 1	si	9	Ty	-37.1	0.0	-34.9	70.9
6- 1	si	11	Si	-42.4	0.0	-33.0	71.2

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 318.0 | Lc = 222.6 | Ro = 3.1 | Im = 72.9 |
 Nodo 3 | om = 1.51 | csz = 1.01 | csy = 1.02 |

Infless. Y

Ncrz = 361599.3 | Ncry = 132815.1 |
 Nmax = -1345.8 | Mzeq = -93088.9 | Myeq = 130.9 |
 Ss = -711.9

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 14
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	6-1	-156565.2	491.4	0.0	-1361.3	1.3	608.7
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
6-1	si	3	Sx	Si	-1136.0	0.0	1136.0
6-1	si	5	Tz		1049.0	17.2	1049.4
6-1	si	9	Ty		-39.5	0.0	-89.5
							160.0

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	6-1	-59597.7	245.7	0.0	-1311.1	1.3	422.9
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
6-1	si	3	Sx	Si	-456.8	0.0	456.8
6-1	si	5	Tz		376.3	12.0	376.8
6-1	si	9	Ty		-38.3	0.0	-62.2
							114.3

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	6-1	2446.6	0.0	0.0	-1260.9	1.3	237.1
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
6-1	si	2	Sx	Si	-54.1	0.0	54.1
6-1	si	5	Tz		-54.1	6.8	55.3
6-1	si	9	Ty		-37.1	0.0	70.9
6-1	si	11	Si		-47.5	0.0	-33.0
							74.3

VERIFICA STABILITA' :

Caso 6-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | lm = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.01 | csy = 1.02 |
 Infless. Y
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -1361.3 | Mzeq = -117423.9 | Myeq = 368.6 |
 Ss = -897.9

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 15
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	8-1	7762.7	6922.8	0.0	-6516.8	35.7	-37.5
6-1		-19548.0	300.8	0.0	-6496.3	1.1	204.2
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
8-1	si	2	Sx	Si	-376.3	0.0	376.3
6-1	si	5	Tz		-53.9	5.8	54.8
6-1	si	9	Ty		-190.7	0.0	-30.0
							197.7

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	10-2	413.9	-4030.0	0.0	-6467.0	2.4	-4.8
8-1		713.6	205.2	0.0	-6466.6	35.7	-37.5
9-2		7871.3	-50.5	0.0	-6516.1	-1.1	-75.0
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
10-2	si	1	Sx	Si	-269.2	0.0	269.2
8-1	si	6	Tz		-196.1	3.0	196.1
9-2	si	9	Ty		-191.6	0.0	11.0
							192.6

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso	8-1	-6335.4	-6512.4	0.0	-6416.4	35.7	-37.5
6-1		-12622.2	-109.2	0.0	-6395.9	1.1	-167.3
TENSIONI		Sx	Tz	Ty	Si		
Caso	Ve	No	massimi				
8-1	si	4	Sx	Si	-355.7	0.0	355.7
6-1	si	6	Tz		-99.9	4.8	100.3
6-1	si	9	Ty		-188.2	0.0	24.6
							192.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | lm = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.04 | csy = 1.11 |
 Infless. Y
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -6496.3 | Mzeq = -14661.0 | Myeq = 225.6 |
 Ss = -441.5

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 16
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	-6343.2	-6508.9	0.0	-5130.7	-22.6	21.5
6-1	-12028.3	-110.4	0.0	-5110.1	-0.4	329.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	4	Sx	-317.9	0.0	0.0	317.9
6-1	si	6	Tz	-66.2	-9.3	0.0	68.2
6-1	si	9	Ty	-150.4	0.0	-48.4	172.2

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
6-1	14995.0	-53.4	0.0	-5071.2	-0.4	40.8
8-1	-3209.3	-3215.9	0.0	-5091.7	-22.6	21.5

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	-254.2	0.0	0.0	254.2
8-1	si	6	Tz	-112.0	-1.8	0.0	112.0
6-1	si	9	Ty	-149.2	0.0	-6.0	149.5

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	-94.8	-92.6	0.0	-5052.5	-44.6	1.0
6-1	-106.0	3.5	0.0	-5032.2	-0.4	-247.7

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	4	Sx	-151.0	0.0	0.0	151.0
6-1	si	5	Tz	-147.2	-7.0	0.0	147.7
6-1	si	9	Ty	-148.0	0.0	36.4	160.8
6-1	si	10	Si	-148.0	0.0	36.4	160.8

VERIFICA STABILITA' :

Caso 8-1 | L0 = 292.0 | Lc = 204.4 | Ro = 3.1 | Im = 66.9 |
 Nodo 4 | om = 1.42 | csz = 1.02 | csy = 1.05 |
 Influss. Y
 Ncrz = 428860.5 | Ncry = 157520.2 |
 Nmax = -5130.7 | Mzeq = -3836.1 | Myeq = -3874.5 |
 Ss = -318.0

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 17
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	-6507.3	2685.6	0.0	-4910.3	-75.7	22.1
6-1	-13354.5	-16.6	0.0	-4891.6	-2.3	234.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	3	Sx	-240.3	0.0	0.0	240.3
6-1	si	6	Tz	-51.1	-6.7	0.0	52.4
6-1	si	9	Ty	-143.8	0.0	-34.5	155.7

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	-3887.1	11661.7	0.0	-4878.7	-75.7	22.1
6-1	7487.1	252.8	0.0	-4860.0	-2.3	117.3

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	3	Sx	-390.8	0.0	0.0	390.8
8-1	si	6	Tz	-172.5	-4.6	0.0	172.7
6-1	si	9	Ty	-142.6	0.0	-17.3	145.7

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	-1267.0	20637.7	0.0	-4847.1	-75.7	22.1
7-1	-185.4	10644.6	0.0	-4847.7	-185.6	2.1

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	3	Sx	-541.3	0.0	0.0	541.3
7-1	si	6	Tz	-192.4	-9.9	0.0	193.1
8-1	si	9	Ty	-121.4	0.0	-3.3	121.5

VERIFICA STABILITA' :

Caso 8-1 | L0 = 237.0 | Lc = 165.9 | Ro = 3.1 | Im = 54.3 |
 Nodo 3 | om = 1.26 | csz = 1.01 | csy = 1.03 |
 Influss. Y
 Ncrz = 651006.1 | Ncry = 239114.1 |
 Nmax = -4910.3 | Mzeq = -4411.1 | Myeq = 13456.9 |
 Ss = -475.7

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 18
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
9- 2	25254.4	935.7	0.0	-7230.5	3.7	-87.9
7- 1	1964.3	9334.6	0.0	-7177.5	157.1	-7.0
6- 1	-20594.1	250.5	0.0	-7158.1	1.3	221.6

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9- 2	si	2	Sx Si	-405.5	0.0	0.0	405.5
7- 1	si	6	Tz	-269.5	8.5	0.0	269.9
6- 1	si	9	Ty	-210.2	0.0	-32.6	217.6

SOLLECITAZIONI : PROGR. 159.00

Caso	MZ	MY	MT	N	TZ	TY
9- 2	11272.4	344.1	0.0	-7188.1	3.7	-87.9

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9- 2	si	2	Sx Si	-296.1	0.0	0.0	296.1
9- 2	si	6	Tz	-291.2	2.7	0.0	291.3
9- 2	si	9	Ty	-211.0	0.0	12.9	212.2

SOLLECITAZIONI : PROGR. 318.00

Caso	MZ	MY	MT	N	TZ	TY
7- 1	-274.7	11754.8	0.0	-7092.6	-172.3	-7.0
6- 1	-77.5	-149.3	0.0	-7073.2	1.3	-92.6

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	3	Sx Si	-432.6	0.0	0.0	432.6
7- 1	si	5	Tz	-150.2	-9.3	0.0	151.0
6- 1	si	9	Ty	-208.1	0.0	13.6	209.4

VERIFICA STABILITA' :

Caso 7- 1 | LO = 318.0 | LC = 222.6 | Ro = 3.1 | Im = 72.9 |
 Nodo 2 | om = 1.51 | csz = 1.03 | csy = 1.09 |
 Infless. Y | Ncrz = 361599.3 | Ncry = 132815.1 |
 | Nmax = -7177.5 | Mzeq = 1473.2 | Myeq = 8816.1 |
 | Ss = -509.9 |

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 19
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
7- 1	-280.9	11754.8	0.0	-6462.1	306.3	-7.0
6- 1	554.7	-149.3	0.0	-6442.7	-2.3	-211.2

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	3	Sx Si	-414.1	0.0	0.0	414.1
7- 1	si	6	Tz	-244.5	16.4	0.0	246.2
6- 1	si	9	Ty	-189.6	0.0	31.0	197.1

SOLLECITAZIONI : PROGR. 29.00

Caso	MZ	MY	MT	N	TZ	TY
7- 1	-485.1	3306.2	0.0	-6454.4	276.3	-7.0
6- 1	-5984.4	-83.4	0.0	-6435.0	-2.3	-239.8

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	3	Sx Si	-255.6	0.0	0.0	255.6
7- 1	si	6	Tz	-202.3	14.9	0.0	203.9
6- 1	si	9	Ty	-189.3	0.0	35.3	198.9

SOLLECITAZIONI : PROGR. 58.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	-6507.3	2738.4	0.0	-6446.0	-75.7	-39.8
7- 1	-689.3	-4271.4	0.0	-6446.6	246.3	-7.0
6- 1	-13354.5	-17.5	0.0	-6427.3	-2.3	-268.5

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	3	Sx Si	-286.4	0.0	0.0	286.4
7- 1	si	6	Tz	-164.2	13.3	0.0	165.8
6- 1	si	9	Ty	-189.0	0.0	39.5	201.0

VERIFICA STABILITA' :

Caso 7- 1 | LO = 58.0 | LC = 40.6 | Ro = 3.1 | Im = 13.3 |
 Nodo 3 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 10869905.8 | Ncry = 3992508.6 |
 | Nmax = -6462.1 | Mzeq = -630.6 | Myeq = 8816.1 |
 | Ss = -361.4 |

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 20
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	-1216.1	20637.7	0.0	-3586.1	379.3	22.1
6- 1	14523.8	522.2	0.0	-3567.4	9.6	-236.9

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	3	Sx Si	-503.9	0.0	0.0	503.9
8-1	si	5	Tz	2.1	20.7	0.0	36.0
6-1	si	9	Ty	-104.4	0.0	34.8	120.5

PROGR. 27.50

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	-608.1	10207.9	0.0	-3578.8	379.3	22.1
6-1	7635.5	257.5	0.0	-3560.0	9.6	-264.1

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	3	Sx Si	-302.3	0.0	0.0	302.3
8-1	si	5	Tz	-52.0	20.7	0.0	63.2
6-1	si	9	Ty	-104.4	0.0	38.8	124.2

PROGR. 55.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	-448.4	0.0	-3572.1	173.2	2.1
8-1	0.0	-221.8	0.0	-3571.4	379.3	22.1
6-1	0.0	-7.2	0.0	-3552.7	9.6	-291.2

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-113.5	0.0	0.0	113.5
8-1	si	5	Tz	-106.1	20.7	0.0	112.0
6-1	si	9	Ty	-104.5	0.0	42.8	128.1

VERIFICA STABILITA' :

Caso 8-1 | L0 = 55.0 | Lc = 38.5 | Ro = 3.1 | Im = 12.6 |
 Nodo 3 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Infless. Y |
 Ncrz = 12088053.9 | Ncry = 4439933.5 |
 Nmax = -3586.1 | Mzeq = -729.7 | Myeq = 12293.9 |
 Ss = -343.1

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 49
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	-109592.6	-343.7	0.0	-16601.3	-5.1	699.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	4	Sx Si	-1255.2	0.0	0.0	1255.2
7-1	si	6	Tz	274.2	-20.0	0.0	276.4
7-1	si	9	Ty	-488.5	0.0	-102.8	519.9

PROGR. 188.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9-2	-266.0	3905.7	0.0	-19937.1	15.3	0.5
7-1	3595.9	606.9	0.0	-16551.2	-5.1	504.7

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	3	Sx Si	-661.8	0.0	0.0	661.8
7-1	si	6	Tz	-514.5	-14.5	0.0	515.1
7-1	si	9	Ty	-486.0	0.0	-74.2	502.7

PROGR. 376.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	80179.6	1557.6	0.0	-16501.0	-5.1	310.0

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx Si	-1071.1	0.0	0.0	1071.1
7-1	si	6	Tz	-1049.1	-9.0	0.0	1049.2
7-1	si	9	Ty	-483.6	0.0	-45.6	490.0

VERIFICA STABILITA' :

Caso 7-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.11 | csy = 1.36 |
 Infless. Y |
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -16601.3 | Mzeq = -82194.5 | Myeq = 1168.2 |
 Ss = -1507.0

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 50
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	80196.0	1557.6	0.0	-12899.0	28.9	-125.0

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx Si	-965.3	0.0	0.0	965.3
7-1	si	6	Tz	-943.3	5.1	0.0	943.4
7-1	si	9	Ty	-377.7	0.0	18.4	379.0

PROGR. 146.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	50911.6	-2657.6	0.0	-12860.1	28.9	-276.2

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	1	Sx	-781.7	0.0	0.0
7-1	si	6	Tz	-718.7	9.3	0.0
7-1	si	9	Ty	-380.8	0.0	40.6

PROGR. 292.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9-2	-3.4	-14251.0	0.0	-12699.1	52.3	0.5
7-1	-449.0	-6872.7	0.0	-12821.1	28.9	-427.4

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
9-2	si	4	Sx	-642.7	0.0	0.0
7-1	si	6	Tz	-340.8	13.6	0.0
7-1	si	9	Ty	-384.0	0.0	62.8

VERIFICA STABILITA` :

Caso 7-1 | L0 = 292.0 | Lc = 204.4 | Ro = 3.1 | Im = 66.9 |
 Nodo 1 | om = 1.42 | csz = 1.05 | csy = 1.14 |
 Infless. Y | Ncrz = 428860.5 | Ncry = 157520.2 |
 | Nmax = -12899.0 | Mzeq = 61401.9 | Myeq = -5154.5 |
 | Ss = -1095.1

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 51
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	-109724.4	521.4	0.0	-16548.5	5.5	699.7

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	3	Sx	-1258.0	0.0	0.0
7-1	si	5	Tz	277.5	20.0	0.0
7-1	si	9	Ty	-486.0	0.0	-102.9

PROGR. 188.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9-1	-377.3	-3928.6	0.0	-24658.0	-9.0	0.8
7-1	3516.0	-521.0	0.0	-16498.4	5.5	505.0

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
9-1	si	4	Sx	-801.8	0.0	0.0
7-1	si	5	Tz	-512.0	14.5	0.0
7-1	si	9	Ty	-485.6	0.0	-74.2

PROGR. 376.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	80151.7	-1563.5	0.0	-16448.2	5.5	310.3

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	1	Sx	-1069.4	0.0	0.0
7-1	si	5	Tz	-1047.4	9.0	0.0
7-1	si	9	Ty	-485.2	0.0	-45.6

VERIFICA STABILITA` :

Caso 7-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 4 | om = 1.73 | csz = 1.11 | csy = 1.35 |
 Infless. Y | Ncrz = 258646.2 | Ncry = 95000.6 |
 | Nmax = -16548.5 | Mzeq = -82293.3 | Myeq = -1172.6 |
 | Ss = -1504.9

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 52
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	80115.2	-1563.5	0.0	-12879.1	-28.2	-124.7

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	1	Sx	-964.3	0.0	0.0
7-1	si	5	Tz	-942.2	-5.0	0.0
7-1	si	9	Ty	-380.3	0.0	18.3

PROGR. 146.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
7-1	50871.2	2557.2	0.0	-12840.2	-28.2	-275.9

TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
7-1	si	2	Sx	-778.9	0.0	0.0
7-1	si	5	Tz	-718.3	-9.3	0.0
7-1	si	9	Ty	-374.9	0.0	40.6

SOLLECITAZIONI : ----- PROGR. 292.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-7.3	15792.6	0.0	-16208.7	-61.7	0.8
7-1	-449.1	6677.8	0.0	-12801.2	-28.2	-427.1

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	3	Sx	-775.0	0.0	0.0	775.0
7-1	si	5	Tz	-341.2	-13.5	0.0	342.0
7-1	si	9	Ty	-369.5	0.0	62.8	385.2

VERIFICA STABILITA' :

Caso 7-1 | L0 = 292.0 | Lc = 204.4 | Ro = 3.1 | Im = 66.9 |
 Nodo 2 | om = 1.42 | csz = 1.05 | csy = 1.14 |
 Inflex. y |
 Ncrz = 428860.5 | Ncry = 157520.2 |
 Nmax = -12879.1 | Mzeq = 61349.4 | Myeq = 5008.3 |
 Ss = -1090.7

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 53
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	-1645.0	16266.4	0.0	-6755.8	215.4	5.9
9-1	-22044.4	1108.7	0.0	-6820.4	4.3	68.9

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	3	Sx	-517.4	0.0	0.0	517.4
7-1	si	5	Tz	-109.1	11.6	0.0	110.9
9-1	si	9	Ty	-199.4	0.0	-10.1	200.2

PROGR. 188.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	-533.6	-5934.2	0.0	-6705.6	20.7	5.9
9-1	-9082.2	301.9	0.0	-6770.2	4.3	68.9

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	4	Sx	-313.0	0.0	0.0	313.0
9-1	si	5	Tz	-134.6	2.2	0.0	134.6
9-1	si	9	Ty	-198.7	0.0	-10.1	199.5

PROGR. 376.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	577.7	8469.8	0.0	-6655.5	-174.0	5.9
9-1	3880.1	-505.0	0.0	-6720.0	4.3	68.9

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx	-359.7	0.0	0.0	359.7
7-1	si	6	Tz	-240.4	-9.4	0.0	240.9
9-1	si	9	Ty	-198.1	0.0	-10.1	198.9

VERIFICA STABILITA' :

Caso 7-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.04 | csy = 1.12 |
 Inflex. y |
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -6755.8 | Mzeq = -1233.7 | Myeq = 12199.8 |
 Ss = -611.2

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 54
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	585.6	8433.6	0.0	-4893.1	135.0	-1.8
6-1	700.2	-424.4	0.0	-4916.9	-5.4	60.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	2	Sx	-307.3	0.0	0.0	307.3
7-1	si	6	Tz	-188.4	7.2	0.0	188.8
6-1	si	9	Ty	-145.0	0.0	-8.8	145.8

PROGR. 118.50

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	3851.9	11500.9	0.0	-4861.4	-114.3	-21.9

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx	-387.0	0.0	0.0	387.0
8-1	si	5	Tz	-114.4	-6.7	0.0	115.0
8-1	si	9	Ty	-131.2	0.0	3.2	131.3

PROGR. 237.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	1255.9	25047.2	0.0	-4829.8	-114.3	-21.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx Si	-624.0	0.0	0.0	624.0
8-1	si	5	Tz	-30.4	-6.7	0.0	32.6
8-1	si	9	Ty	-116.4	0.0	3.2	116.5

VERIFICA STABILITA' :

Caso 8-1 | L0 = 237.0 | Lc = 165.9 | Ro = 3.1 | Im = 54.3 |
 Nodo 2 | om = 1.26 | csz = 1.01 | csy = 1.03 |
 Infless. Y | Ncrz = 651006.1 | Ncry = 239114.1 |
 | Nmax = -4893.1 | Mzeq = 4371.1 | Myeq = 14210.2 |
 Ss = -489.4

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 55
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	1204.9	25047.2	0.0	-3588.5	459.6	-21.9
9-1	5513.5	1153.2	0.0	-3653.0	21.2	-100.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx Si	-587.2	0.0	0.0	587.2
8-1	si	6	Tz	-234.2	25.0	0.0	238.1
9-1	si	9	Ty	-106.2	0.0	14.7	109.2

PROGR. 27.50

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8-1	602.4	12408.8	0.0	-3581.1	459.6	-21.9
6-1	2982.0	425.5	0.0	-3604.9	15.7	-104.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx Si	-343.9	0.0	0.0	343.9
8-1	si	6	Tz	-169.1	25.0	0.0	174.5
6-1	si	9	Ty	-105.6	0.0	15.3	108.8

PROGR. 55.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7-1	0.0	-449.8	0.0	-3573.8	80.1	-1.8
8-1	0.0	-229.7	0.0	-3573.8	459.6	-21.9
6-1	0.0	-6.6	0.0	-3597.6	15.7	-112.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	-113.6	0.0	0.0	113.6
8-1	si	6	Tz	-104.0	25.0	0.0	112.6
6-1	si	9	Ty	-105.8	0.0	16.6	109.6
8-1	si	7	Si	-106.2	25.0	0.0	114.7

VERIFICA STABILITA' :

Caso 8-1 | L0 = 55.0 | Lc = 38.5 | Ro = 3.1 | Im = 12.6 |
 Nodo 2 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Infless. Y | Ncrz = 12088053.9 | Ncry = 4439933.5 |
 | Nmax = -3588.5 | Mzeq = 722.9 | Myeq = 14936.5 |
 Ss = -393.1

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 81
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	-29000.7	134.8	0.0	-553.8	0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx Si	-220.1	0.0	0.0	220.1
6-1	si	5	Tz	185.6	2.2	0.0	185.7
6-1	si	9	Ty	-16.1	0.0	-11.5	25.6

PROGR. 188.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	-14339.3	67.4	0.0	-503.6	0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx Si	-115.6	0.0	0.0	115.6
6-1	si	5	Tz	85.0	2.2	0.0	85.1
6-1	si	9	Ty	-14.7	0.0	-11.5	24.7

PROGR. 376.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6-1	322.0	0.0	0.0	-453.4	0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	2	Sx	-15.6	0.0	0.0	15.6
6-1	si	5	Tz	-15.6	2.2	0.0	16.0
6-1	si	9	Ty	-13.3	0.0	-11.5	23.9

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.00 | csy = 1.01 |
 Infless. Y | Ncrz = 258646.2 | Ncry = 95000.6 |
 | Nmax = -553.8 | Mzeq = -17271.6 | Myeq = 80.9 |
 | Ss = -150.0 |

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 82
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-28971.1	-131.8	0.0	-553.8	-0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-219.8	0.0	0.0	219.8
6- 1	si	6	Tz	185.4	-2.2	0.0	185.5
6- 1	si	9	Ty	-16.4	0.0	-11.5	25.8

PROGR. 188.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-14309.7	-65.9	0.0	-503.6	-0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-115.4	0.0	0.0	115.4
6- 1	si	6	Tz	84.8	-2.2	0.0	84.9
6- 1	si	9	Ty	-14.9	0.0	-11.5	24.8

PROGR. 376.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	351.7	0.0	0.0	-453.4	-0.4	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	1	Sx	-15.8	0.0	0.0	15.8
6- 1	si	6	Tz	-15.8	-2.2	0.0	16.2
6- 1	si	9	Ty	-13.3	0.0	-11.5	23.9
6- 1	si	11	Si	-14.8	0.0	-10.8	23.9

VERIFICA STABILITA' :

Caso 6- 1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 4 | om = 1.73 | csz = 1.00 | csy = 1.01 |
 Infless. Y | Ncrz = 258646.2 | Ncry = 95000.6 |
 | Nmax = -553.8 | Mzeq = -17242.0 | Myeq = -79.1 |
 | Ss = -149.8 |

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 83
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
6- 1	-28968.2	-79.6	0.0	-624.4	-0.2	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6- 1	si	4	Sx	-220.9	0.0	0.0	220.9
6- 1	si	6	Tz	183.1	-2.2	0.0	183.1
6- 1	si	9	Ty	-18.4	0.0	-11.5	27.1

PROGR. 188.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10- 2	29.8	-2828.0	0.0	-3251.4	-15.0	0.0
6- 1	-14306.8	-39.8	0.0	-574.2	-0.2	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10- 2	si	1	Sx	-149.2	0.0	0.0	149.2
6- 1	si	6	Tz	82.6	-2.2	0.0	82.7
6- 1	si	9	Ty	-16.9	0.0	-11.5	26.1

PROGR. 376.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
10- 2	29.8	0.0	0.0	-3201.2	-15.0	0.0
6- 1	354.6	0.0	0.0	-524.1	-0.2	78.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10- 2	si	1	Sx	-94.3	0.0	0.0	94.3
6- 1	si	6	Tz	-17.9	-2.2	0.0	18.3
6- 1	si	9	Ty	-15.4	0.0	-11.5	25.1
10- 2	si	5	Si	-94.3	-0.8	0.0	94.3

VERIFICA STABILITA' :

Caso 10- 2 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 1 | om = 1.73 | csz = 1.02 | csy = 1.05 |
 Infless. Y |

Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -3301.6 | Mzeq = 29.8 | Myeq = -3393.6 |
 Ss = -236.1

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 84
 SOLLECITAZIONI :----- PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	-28974.8	30.9	0.0	-553.8	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx	-218.0	0.0	0.0	218.0
6-1	si	5	Tz	185.0	2.2	0.0	185.0
6-1	si	9	Ty	-16.2	0.0	-11.5	25.7

SOLLECITAZIONI :----- PROGR. 188.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	-14313.4	15.5	0.0	-503.6	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx	-114.4	0.0	0.0	114.4
6-1	si	5	Tz	84.6	2.2	0.0	84.7
6-1	si	9	Ty	-14.8	0.0	-11.5	24.8

SOLLECITAZIONI :----- PROGR. 376.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	347.9	0.0	0.0	-453.4	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	-15.7	0.0	0.0	15.7
6-1	si	5	Tz	-15.7	2.2	0.0	16.2
6-1	si	9	Ty	-13.3	0.0	-11.5	23.9
6-1	si	11	Si	-14.8	0.0	-10.8	23.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.00 | csy = 1.01 |
 Infless. Y

Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -553.8 | Mzeq = -17245.7 | Myeq = 18.6 |
 Ss = -148.6

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 85
 SOLLECITAZIONI :----- PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	-29004.0	40.5	0.0	-553.8	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx	-218.3	0.0	0.0	218.3
6-1	si	5	Tz	185.2	2.2	0.0	185.3
6-1	si	9	Ty	-16.2	0.0	-11.5	25.7

SOLLECITAZIONI :----- PROGR. 188.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	-14342.6	20.2	0.0	-503.6	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	3	Sx	-114.7	0.0	0.0	114.7
6-1	si	5	Tz	84.8	2.2	0.0	84.9
6-1	si	9	Ty	-14.8	0.0	-11.5	24.8

SOLLECITAZIONI :----- PROGR. 376.00

Caso	MZ	MY	MT	N	TZ	TY
6-1	318.8	0.0	0.0	-453.4	0.1	78.0

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
6-1	si	1	Sx	-15.5	0.0	0.0	15.5
6-1	si	5	Tz	-15.5	2.2	0.0	16.0
6-1	si	9	Ty	-13.3	0.0	-11.5	23.9

VERIFICA STABILITA' :

Caso 6-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.00 | csy = 1.01 |
 Infless. Y

Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -553.8 | Mzeq = -17274.9 | Myeq = 24.3 |
 Ss = -149.0

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 86
 SOLLECITAZIONI :----- PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-19062.0	-405.6	0.0	-5840.9	-1.9	58.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	4	Sx Si	-311.7	0.0	0.0	311.7
9-1	si	6	Tz	-37.5	-1.7	0.0	37.6
9-1	si	9	Ty	-172.1	0.0	-8.6	172.8

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
10-1	-387.7	3142.5	0.0	-5732.6	19.5	4.3
9-1	-8073.6	-47.7	0.0	-5790.7	-1.9	58.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
10-1	si	3	Sx Si	-230.6	0.0	0.0	230.6
9-1	si	6	Tz	-114.0	-1.7	0.0	114.0
9-1	si	9	Ty	-170.3	0.0	-8.6	171.0

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	6239.0	1842.9	0.0	-5681.1	0.8	36.6
9-1	2914.8	310.2	0.0	-5740.6	-1.9	58.4

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx Si	-245.2	0.0	0.0	245.2
9-1	si	6	Tz	-190.5	-1.7	0.0	190.5
9-1	si	9	Ty	-168.5	0.0	-8.6	169.1

VERIFICA STABILITA' :

Caso 10-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1
 Nodo 3 | om = 1.73 | csz = 1.03 | csy = 1.10
 Infless. Y | Ncrz = 258646.2 | Ncry = 95000.6
 | Nmax = -5782.8 | Mzeq = -548.9 | Myeq = 3877.4
 | Ss = -379.2

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 87
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	6243.7	1895.0	0.0	-5114.3	113.8	-21.2
6-1	957.0	251.8	0.0	-5140.2	4.8	59.1

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	2	Sx Si	-229.5	0.0	0.0	229.5
8-1	si	6	Tz	-202.8	6.6	0.0	203.1
6-1	si	9	Ty	-150.9	0.0	-8.7	151.6

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	3730.6	-11591.7	0.0	-5082.7	113.8	-21.2

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx Si	-394.4	0.0	0.0	394.4
8-1	si	6	Tz	-119.7	6.6	0.0	120.2
8-1	si	9	Ty	-161.3	0.0	3.1	161.4

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	1217.5	-25078.3	0.0	-5051.1	113.8	-21.2

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx Si	-630.8	0.0	0.0	630.8
8-1	si	6	Tz	-36.5	6.6	0.0	38.3
8-1	si	9	Ty	-174.2	0.0	3.1	174.3

VERIFICA STABILITA' :

Caso 8-1 | L0 = 237.0 | Lc = 165.9 | Ro = 3.1 | Im = 54.3
 Nodo 1 | om = 1.26 | csz = 1.01 | csy = 1.03
 Infless. Y | Ncrz = 651006.1 | Ncry = 239114.1
 | Nmax = -5114.3 | Mzeq = 4233.2 | Myeq = -14289.0
 | Ss = -498.6

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 88
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	1166.4	-25078.3	0.0	-3809.7	-460.2	-21.2
9-1	5334.3	-632.2	0.0	-3869.2	-11.6	-97.0

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx Si	-594.0	0.0	0.0	594.0
8-1	si	5	Tz	-240.6	-25.0	0.0	244.4
9-1	si	9	Ty	-114.4	0.0	14.3	117.0

PROGR. 27.50

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	583.2	-12422.9	0.0	-3802.4	-460.2	-21.2
6- 1	3006.1	-440.9	0.0	-3828.3	-16.4	-104.8

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-350.6	0.0	0.0	350.6
8- 1	si	5	Tz	-175.5	-25.0	0.0	180.8
6- 1	si	9	Ty	-113.0	0.0	15.4	116.1

PROGR. 55.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	0.0	232.4	0.0	-3795.0	-460.2	-21.2
6- 1	0.0	10.5	0.0	-3820.9	-16.4	-113.8

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	3	Sx	-116.0	0.0	0.0	116.0
8- 1	si	5	Tz	-110.5	-25.0	0.0	118.6
6- 1	si	9	Ty	-112.3	0.0	16.7	116.0
8- 1	si	8	Si	-112.7	-25.0	0.0	120.7

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 55.0 | Lc = 38.5 | Ro = 3.1 | Im = 12.6 |
 Nodo 1 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Infless. Y |
 Ncrz = 12088053.9 | Ncry = 4439933.5 |
 Nmax = -3809.7 | Mzeq = 699.9 | Myeq = -14954.0 |
 Ss = -399.8

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 114
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	-28493.2	-571.4	0.0	-14584.9	-5.9	133.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	4	Sx	-637.4	0.0	0.0	637.4
7- 1	si	6	Tz	-228.3	-4.1	0.0	228.4
7- 1	si	9	Ty	-429.4	0.0	-19.6	430.7

PROGR. 188.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
9- 2	-155.1	3591.7	0.0	-17724.4	12.0	0.3
7- 1	-3403.0	535.0	0.0	-14534.7	-5.9	133.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9- 2	si	3	Sx	-590.1	0.0	0.0	590.1
7- 1	si	6	Tz	-406.3	-4.1	0.0	406.4
7- 1	si	9	Ty	-426.8	0.0	-19.6	428.1

PROGR. 376.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	21687.2	1641.4	0.0	-14484.5	-5.9	133.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	2	Sx	-607.4	0.0	0.0	607.4
7- 1	si	6	Tz	-584.3	-4.1	0.0	584.3
7- 1	si	9	Ty	-424.2	0.0	-19.6	425.5

VERIFICA STABILITA' :

Caso 9- 2 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 3 | om = 1.73 | csz = 1.11 | csy = 1.39 |
 Infless. Y |
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -17774.6 | Mzeq = -167.6 | Myeq = 4043.9 |
 Ss = -1013.1

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 115
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	21689.3	1641.4	0.0	-13706.4	29.3	-20.9
9- 2	-95.3	1330.7	0.0	-13607.0	52.3	0.3

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7- 1	si	2	Sx	-584.5	0.0	0.0	584.5
9- 2	si	5	Tz	-393.0	2.8	0.0	393.0
7- 1	si	9	Ty	-401.3	0.0	3.1	401.3

PROGR. 146.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
7- 1	14716.2	-2638.4	0.0	-13667.5	29.3	-74.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
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7-1	si	1	Sx	Si	-553.8	0.0	0.0	553.8
7-1	si	6	Tz		-491.3	3.7	0.0	491.4
7-1	si	9	Ty		-404.5	0.0	11.0	405.0

SOLLECITAZIONI : PROGR. 292.00

Caso	MZ	MY	MT	N	TZ	TY
9-2	1.3	-13929.9	0.0	-13529.1	52.3	0.3
7-1	-92.5	-6918.3	0.0	-13628.5	29.3	-128.3

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-2	si	1	Sx	Si	0.0	0.0	661.0
7-1	si	6	Tz		5.2	0.0	366.9
7-1	si	9	Ty		0.0	18.9	409.1

VERIFICA STABILITA' :

Caso 7-1 | L0 = 292.0 | Lc = 204.4 | Ro = 3.1 | Im = 66.9 |
 Nodo 1 | om = 1.42 | csz = 1.05 | csy = 1.15 |
 Inflex. Y |
 Ncrz = 428860.5 | Ncry = 157520.2 |
 Nmax = -13706.4 | Mzeq = 17433.3 | Myeq = -5188.7 |
 Ss = -811.3

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 116
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-181.1	-4764.7	0.0	-22031.2	-6.3	0.3
7-1	-28412.1	668.8	0.0	-14625.6	6.1	133.3

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	4	Sx	Si	0.0	0.0	739.0
7-1	si	5	Tz		4.1	0.0	229.7
7-1	si	9	Ty		0.0	-19.6	430.7

SOLLECITAZIONI : PROGR. 188.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-127.9	-3587.8	0.0	-21981.0	-6.3	0.3
7-1	-3349.9	-485.9	0.0	-14575.4	6.1	133.3

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	4	Sx	Si	0.0	0.0	715.0
7-1	si	5	Tz		4.1	0.0	407.7
7-1	si	9	Ty		0.0	-19.6	430.4

SOLLECITAZIONI : PROGR. 376.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-74.6	-2410.8	0.0	-21930.8	-6.3	0.3
7-1	21712.3	-1640.5	0.0	-14525.3	6.1	133.3

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	4	Sx	Si	0.0	0.0	690.9
7-1	si	5	Tz		4.1	0.0	585.7
7-1	si	9	Ty		0.0	-19.6	430.1

VERIFICA STABILITA' :

Caso 9-1 | L0 = 376.0 | Lc = 263.2 | Ro = 3.1 | Im = 86.1 |
 Nodo 4 | om = 1.73 | csz = 1.15 | csy = 1.53 |
 Inflex. Y |
 Ncrz = 258646.2 | Ncry = 95000.6 |
 Nmax = -22031.2 | Mzeq = -138.5 | Myeq = -3823.2 |
 Ss = -1234.3

P_HEB120_S003 (3) - metodo: tensioni ammissibili - ASTA 117
PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
7-1	21702.9	-1640.5	0.0	-13712.1	-29.0	-21.1
9-1	-76.1	-2410.8	0.0	-16862.0	-60.6	0.3

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
7-1	si	1	Sx	Si	0.0	0.0	584.8
9-1	si	6	Tz		-3.2	0.0	483.7
7-1	si	9	Ty		0.0	3.1	404.9

SOLLECITAZIONI : PROGR. 146.00

Caso	MZ	MY	MT	N	TZ	TY
9-1	-34.7	6433.2	0.0	-16823.1	-60.6	0.3
7-1	14708.0	2590.0	0.0	-13673.1	-29.0	-74.7

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9-1	si	3	Sx	Si	0.0	0.0	616.4
7-1	si	5	Tz		-3.6	0.0	491.7
7-1	si	9	Ty		0.0	11.0	399.8

PROGR. 292.00

| 1- 1|si|17|Sx Si| -339.1| 0.0| 0.0| 339.1|

 SOLLECITAZIONI : PROGR. 147.50

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-269501.5	140.4	0.0	-12897.0	1.6	-1034.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	17	Sx Si	-588.0	0.0	0.0	588.0

SOLLECITAZIONI : PROGR. 295.00

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-422102.7	-93.6	0.0	-12793.6	1.6	-1034.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	18	Sx Si	-837.6	0.0	0.0	837.6

VERIFICA STABILITA` :

Caso 1- 1 |L0 = 295.0|Lc = 206.5|Ro = 5.1 |Im= 40.8|
 Nodo17 |om = 1.14|csz= 1.01|csy= 1.02|
 Infless. Y

|Ncrz = 3495963.4|Ncry= 1111908.1|
 |Nmax = -13000.4|Mzeq= -300021.7|Myeq= 187.2|
 Ss = -662.4

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 3

 SOLLECITAZIONI : PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
9- 2	236760.1	-727.3	0.0	-16043.7	-4.7	-934.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9- 2	si	8	Sx Si	-599.8	0.0	0.0	599.8

SOLLECITAZIONI : PROGR. 159.00

Caso	MZ	MY	MT	N	TZ	TY
9- 2	88257.5	14.8	0.0	-15932.3	-4.7	-934.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
9- 2	si	9	Sx Si	-334.0	0.0	0.0	334.0

SOLLECITAZIONI : PROGR. 318.00

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-118438.5	370.4	0.0	-14261.1	-4.6	-1026.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	17	Sx Si	-355.8	0.0	0.0	355.8

VERIFICA STABILITA` :

Caso 9- 2 |L0 = 318.0|Lc = 222.6|Ro = 5.1 |Im= 44.0|
 Nodo 9 |om = 1.16|csz= 1.01|csy= 1.03|
 Infless. Y

|Ncrz = 3008546.1|Ncry= 956882.6|
 |Nmax = -16043.7|Mzeq= 117958.0|Myeq= 302.8|
 Ss = -419.2

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 4

 SOLLECITAZIONI : PROGR. 0.00

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-118304.8	370.4	0.0	-13000.1	2.1	-1026.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	17	Sx Si	-341.4	0.0	0.0	341.4

SOLLECITAZIONI : PROGR. 147.50

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-269695.9	55.0	0.0	-12896.7	2.1	-1026.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	17	Sx Si	-588.1	0.0	0.0	588.1

SOLLECITAZIONI : PROGR. 295.00

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-421086.9	-260.3	0.0	-12793.4	2.1	-1026.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	18	Sx Si	-836.5	0.0	0.0	836.5

VERIFICA STABILITA` :

Caso 1- 1 |L0 = 295.0|Lc = 206.5|Ro = 5.1 |Im= 40.8|
 Nodo17 |om = 1.14|csz= 1.01|csy= 1.02|
 Infless. Y

Ncrz = 3495963.4 | Ncry = 1111908.1 |
 Nmax = -13000.1 | Mzeq = -299974.1 | Myeq = 148.2 |
 Ss = -662.2

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 5
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 63282.2 40886.7 0.0 -30109.1 141.9 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si| 9|Sx Si -609.6 Tz 0.0 Ty 0.0 Si 609.6

PROGR. 159.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 -1790.5 18322.6 0.0 -29997.7 141.9 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si|16|Sx Si -409.4 Tz 0.0 Ty 0.0 Si 409.4

PROGR. 318.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 -66863.2 -4241.5 0.0 -29886.3 141.9 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si|18|Sx Si -459.5 Tz 0.0 Ty 0.0 Si 459.5

VERIFICA STABILITA' :

Caso10- 1 | L0 = 318.0 | Lc = 222.6 | Ro = 5.1 | Im = 44.0 |
 Nodo17 | om = 1.16 | csz = 1.02 | csy = 1.05 |
 Influss. Y
 Ncrz = 3008546.1 | Ncry = 956882.6 |
 Nmax = -30109.1 | Mzeq = -26745.3 | Myeq = 22835.5 |
 Ss = -519.7

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 6
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 -66858.3 -4241.5 0.0 -24715.9 -357.0 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si|18|Sx Si -401.6 Tz 0.0 Ty 0.0 Si 401.6

PROGR. 147.50
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 -127224.5 48413.8 0.0 -24612.5 -357.0 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si|17|Sx Si -654.2 Tz 0.0 Ty 0.0 Si 654.2

PROGR. 295.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 -187590.7 101069.0 0.0 -24509.2 -357.0 -409.3
 TENSIONI :
 Caso|Ve|No|massimi
 10- 1|si|17|Sx Si -936.4 Tz 0.0 Ty 0.0 Si 936.4

VERIFICA STABILITA' :

Caso10- 1 | L0 = 295.0 | Lc = 206.5 | Ro = 5.1 | Im = 40.8 |
 Nodo17 | om = 1.14 | csz = 1.01 | csy = 1.03 |
 Influss. Y
 Ncrz = 3495963.4 | Ncry = 1111908.1 |
 Nmax = -24715.9 | Mzeq = -139297.8 | Myeq = 58944.8 |
 Ss = -759.7

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 7
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 9- 2 234392.8 1718.7 0.0 -15953.5 6.4 -918.5
 TENSIONI :
 Caso|Ve|No|massimi
 9- 2|si| 9|Sx Si -598.5 Tz 0.0 Ty 0.0 Si 598.5

PROGR. 159.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 9- 2 88356.3 699.9 0.0 -15842.1 6.4 -918.5
 TENSIONI :
 Caso|Ve|No|massimi
 9- 2|si| 9|Sx Si -335.9 Tz 0.0 Ty 0.0 Si 335.9

PROGR. 318.00
 SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY

1- 1	-116890.0	-523.3	0.0	-13946.5	8.0	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						350.2

VERIFICA STABILITA' :

Caso 9- 2	LO = 318.0	Lc = 222.6	Ro = 5.1	lm = 44.0
Nodo 9	om = 1.16	csz = 1.01	csy = 1.03	
Inflless. y	Ncrz = 3008546.1	Ncry = 956882.6		
	Nmax = -15953.5	Mzeq = 117563.6	Myeq = 903.7	
	Ss = -419.8			

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 8
PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-176842.0	-339.5	0.0	-12960.1	-1.9	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						437.1

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-299627.7	-112.7	0.0	-12877.1	-1.9	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						637.2

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-422413.3	114.2	0.0	-12794.0	-1.9	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	17	Sx	Si	Sx	Tz
						Ty
						Si
						838.2

VERIFICA STABILITA' :

Caso 1- 1	LO = 237.0	Lc = 165.9	Ro = 5.1	lm = 32.8
Nodo 18	om = 1.08	csz = 1.00	csy = 1.01	
Inflless. y	Ncrz = 5416443.5	Ncry = 1722726.1		
	Nmax = -12960.1	Mzeq = -324184.8	Myeq = -158.0	
	Ss = -692.2			

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 9
PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-116821.3	-523.3	0.0	-13316.0	-3.2	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						343.0

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-146870.1	-431.4	0.0	-13295.7	-3.2	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						391.9

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	-176918.9	-339.5	0.0	-13275.4	-3.2	-1036.2
TENSIONI						
Caso	Ve	No	massimi			
1- 1	si	18	Sx	Si	Sx	Tz
						Ty
						Si
						440.8

VERIFICA STABILITA' :

Caso 1- 1	LO = 58.0	Lc = 40.6	Ro = 5.1	lm = 8.0
Nodo 18	om = 1.00	csz = 1.00	csy = 1.00	
Inflless. y	Ncrz = 90438826.6	Ncry = 28764506.8		
	Nmax = -13316.0	Mzeq = -152879.9	Myeq = -449.8	
	Ss = -402.1			

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 73
PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9- 1	-240373.1	1039.4	0.0	-15433.5	2.1	924.2
TENSIONI						
Caso	Ve	No	massimi			

| 9- 1|si|17|Sx Si | -571.7| 0.0| 0.0| 571.7|
 ----- PROGR. 188.00

SOLLECITAZIONI :
 Caso 9- 2 MZ 78558.6 MY -1089.8 MT 0.0 N -14828.8 TZ -6.9 TY -60.8
 TENSIONI :
 Caso|Ve|No|massimi
 9- 2|si| 8|Sx Si | Sx -308.8 Tz 0.0 Ty 0.0 Si 308.8

SOLLECITAZIONI :
 Caso 1- 1 MZ 176705.7 MY 105.8 MT 0.0 N -13373.6 TZ -1.6 TY 1034.8
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si| 9|Sx Si | Sx -461.6 Tz 0.0 Ty 0.0 Si 461.6

VERIFICA STABILITA' :

Caso10- 2 |LO = 376.0|Lc = 263.2|Ro = 5.1|Im= 52.0|
 Nodo 8 |om = 1.24|csz= 1.01|csy= 1.03|
 Infless. Y
 Ncrz = 2151965.1|Ncry= 684442.9|
 Nmax = -15199.1|Mzeq= 35257.0|Myeq= -29331.8|
 Ss = -393.3

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 74
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 1- 1 MZ 176628.6 MY 105.8 MT 0.0 N -12920.2 TZ 1.0 TY 1034.8
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si| 9|Sx Si | Sx -456.4 Tz 0.0 Ty 0.0 Si 456.4

SOLLECITAZIONI :
 Caso 1- 1 MZ 299253.1 MY -9.6 MT 0.0 N -12837.2 TZ 1.0 TY 1034.8
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si| 8|Sx Si | Sx -671.2 Tz 0.0 Ty 0.0 Si 671.2

SOLLECITAZIONI :
 Caso 1- 1 MZ 421877.5 MY -124.9 MT 0.0 N -12754.1 TZ 1.0 TY 1034.8
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si| 8|Sx Si | Sx -886.8 Tz 0.0 Ty 0.0 Si 886.8

VERIFICA STABILITA' :

Caso 1- 1 |LO = 237.0|Lc = 165.9|Ro = 5.1|Im= 32.8|
 Nodo 8 |om = 1.08|csz= 1.00|csy= 1.01|
 Infless. Y
 Ncrz = 5416443.5|Ncry= 1722726.1|
 Nmax = -12920.2|Mzeq= 323778.0|Myeq= -50.0|
 Ss = -729.1

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 75
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso 9- 1 MZ -234379.1 MY -233.1 MT 0.0 N -15433.9 TZ -2.5 TY 912.1
 TENSIONI :
 Caso|Ve|No|massimi
 9- 1|si|18|Sx Si | Sx -559.0 Tz 0.0 Ty 0.0 Si 559.0

SOLLECITAZIONI :
 Caso 9- 2 MZ 80220.0 MY -549.5 MT 0.0 N -14835.7 TZ -5.8 TY -60.5
 TENSIONI :
 Caso|Ve|No|massimi
 9- 2|si| 8|Sx Si | Sx -309.7 Tz 0.0 Ty 0.0 Si 309.7

SOLLECITAZIONI :
 Caso 1- 1 MZ 177607.7 MY 214.3 MT 0.0 N -13373.9 TZ -2.5 TY 1027.7
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si| 9|Sx Si | Sx -463.6 Tz 0.0 Ty 0.0 Si 463.6

VERIFICA STABILITA' :

Caso10- 2 |LO = 376.0|Lc = 263.2|Ro = 5.1|Im= 52.0|
 Nodo 8 |om = 1.24|csz= 1.01|csy= 1.03|
 Infless. Y

Ncrz = 2151965.1 | Ncry = 684442.9 |
 Nmax = -15201.2 | Mzeq = 36177.6 | Myeq = -26827.5 |
 Ss = -384.7

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 76
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 1- 1 | 177551.5 | 214.3 | 0.0 | -12920.5 | 2.3 | 1027.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 1- 1 | si | 9 | Sx | Si | -458.4 | 0.0 | 0.0 | 458.4 |
 PROGR. 118.50

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 1- 1 | 299334.3 | -63.6 | 0.0 | -12837.4 | 2.3 | 1027.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 1- 1 | si | 8 | Sx | Si | -671.5 | 0.0 | 0.0 | 671.5 |
 PROGR. 237.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 1- 1 | 421117.1 | -341.4 | 0.0 | -12754.4 | 2.3 | 1027.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 1- 1 | si | 8 | Sx | Si | -886.3 | 0.0 | 0.0 | 886.3 |

VERIFICA STABILITA' :

Caso 1- 1 | L0 = 237.0 | Lc = 165.9 | Ro = 5.1 | Im = 32.8 |
 Nodo 8 | om = 1.08 | csz = 1.00 | csy = 1.01 |
 Infless. Y
 Ncrz = 5416443.5 | Ncry = 1722726.1 |
 Nmax = -12920.5 | Mzeq = 323690.9 | Myeq = -136.6 |
 Ss = -729.3

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 77
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | -64168.8 | 46470.9 | 0.0 | -29519.7 | 150.4 | 410.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 10- 1 | si | 17 | Sx | Si | -598.7 | 0.0 | 0.0 | 598.7 |
 PROGR. 188.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 13048.6 | 18188.2 | 0.0 | -29387.9 | 150.4 | 410.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 10- 1 | si | 9 | Sx | Si | -423.7 | 0.0 | 0.0 | 423.7 |
 PROGR. 376.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 90266.0 | -10094.4 | 0.0 | -29256.2 | 150.4 | 410.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 10- 1 | si | 8 | Sx | Si | -526.5 | 0.0 | 0.0 | 526.5 |

VERIFICA STABILITA' :

Caso 10- 1 | L0 = 376.0 | Lc = 263.2 | Ro = 5.1 | Im = 52.0 |
 Nodo 9 | om = 1.24 | csz = 1.02 | csy = 1.07 |
 Infless. Y
 Ncrz = 2151965.1 | Ncry = 684442.9 |
 Nmax = -29519.7 | Mzeq = 36106.4 | Myeq = 23844.8 |
 Ss = -575.3

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 78
 PROGR. 0.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 90300.9 | -10094.4 | 0.0 | -23783.8 | -495.9 | 410.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 10- 1 | si | 8 | Sx | Si | -465.2 | 0.0 | 0.0 | 465.2 |
 PROGR. 118.50

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |
 10- 1 | 138972.6 | 48670.2 | 0.0 | -23700.8 | -495.9 | 410.7 |
 TENSIONI :
 Caso | Ve | No | massimi | Sx | Tz | Ty | Si |
 10- 1 | si | 9 | Sx | Si | -701.8 | 0.0 | 0.0 | 701.8 |
 PROGR. 237.00

SOLLECITAZIONI :
 Caso | MZ | MY | MT | N | TZ | TY |

10- 1	187644.2	107434.9	0.0	-23617.7	-495.9	410.7
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
10- 1 si 9 Sx Si		-1017.9	0.0	0.0	1017.9	

VERIFICA STABILITA` :

Caso10- 1 | LO = 237.0 | Lc = 165.9 | Ro = 5.1 | Im = 32.8 |
 Nodo 9 | om = 1.08 | csz = 1.01 | csy = 1.02 |
 Infless. y

| Ncrz = 5416443.5 | Ncry = 1722726.1 |
 | Nmax = -23783.8 | Mzeq = 148706.9 | Myeq = 60423.2 |
 Ss = -794.2

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 79
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9- 1	-231979.7	1544.7	0.0	-15420.8	6.0	899.5
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
9- 1 si 17 Sx Si		-559.5	0.0	0.0	559.5	

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
9- 2	74495.9	603.4	0.0	-14840.8	6.4	-35.4
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
9- 2 si 9 Sx Si		-299.9	0.0	0.0	299.9	

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	176590.8	-530.4	0.0	-13373.2	5.4	1035.1
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
1- 1 si 8 Sx Si		-463.1	0.0	0.0	463.1	

VERIFICA STABILITA` :

Caso10- 1 | LO = 376.0 | Lc = 263.2 | Ro = 5.1 | Im = 52.0 |
 Nodo 9 | om = 1.24 | csz = 1.01 | csy = 1.03 |
 Infless. y

| Ncrz = 2151965.1 | Ncry = 684442.9 |
 | Nmax = -15198.6 | Mzeq = 35325.7 | Myeq = 28835.6 |
 Ss = -391.4

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 80
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	176515.1	-530.4	0.0	-12919.8	-2.8	1035.1
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
1- 1 si 8 Sx Si		-457.9	0.0	0.0	457.9	

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	299175.6	-196.5	0.0	-12836.8	-2.8	1035.1
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
1- 1 si 8 Sx Si		-671.8	0.0	0.0	671.8	

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	421836.1	137.4	0.0	-12753.7	-2.8	1035.1
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
1- 1 si 9 Sx Si		-886.8	0.0	0.0	886.8	

VERIFICA STABILITA` :

Caso 1- 1 | LO = 237.0 | Lc = 165.9 | Ro = 5.1 | Im = 32.8 |
 Nodo 8 | om = 1.08 | csz = 1.00 | csy = 1.01 |
 Infless. y

| Ncrz = 5416443.5 | Ncry = 1722726.1 |
 | Nmax = -12919.8 | Mzeq = 323707.7 | Myeq = -263.3 |
 Ss = -729.8

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 128
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
1- 1	422014.5	-124.9	0.0	-10271.4	-2.3	1034.8
TENSIONI						
Caso Ve No massimi		Sx	Tz	Ty	Si	
1- 1 si 9 Sx Si						

| 1- 1|si| 8|Sx Si| -859.2| 0.0| 0.0| 859.2|
 ----- PROGR. 27.50

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 450471.7 -62.2 0.0 -10252.1 -2.3 1034.8

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 8|Sx Si| -908.9 0.0 0.0 908.9
 ----- PROGR. 55.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 478928.8 0.4 0.0 -10232.8 -2.3 1034.8

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 9|Sx Si| -958.6 0.0 0.0 958.6

VERIFICA STABILITA' :

Caso 1- 1 |LO = 55.0|LC = 38.5|Ro = 5.1|Im= 7.6|
 Nodo 8 |om = 1.00|csz= 1.00|csy= 1.00|
 Infless. Y
 |Ncrz =100573954.6|Ncry= 31988033.3|
 |Nmax = -10271.4|Mzeq= 456163.1|Myeq= -74.8|
 Ss = -919.3

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 129
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 421117.6 -341.4 0.0 -10271.7 -6.2 1027.7

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 8|Sx Si| -858.5 0.0 0.0 858.5
 ----- PROGR. 27.50

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 449379.4 -170.5 0.0 -10252.4 -6.2 1027.7

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 8|Sx Si| -907.4 0.0 0.0 907.4
 ----- PROGR. 55.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 477641.3 0.4 0.0 -10233.1 -6.2 1027.7

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 9|Sx Si| -956.3 0.0 0.0 956.3

VERIFICA STABILITA' :

Caso 1- 1 |LO = 55.0|LC = 38.5|Ro = 5.1|Im= 7.6|
 Nodo 8 |om = 1.00|csz= 1.00|csy= 1.00|
 Infless. Y
 |Ncrz =100573954.6|Ncry= 31988033.3|
 |Nmax = -10271.7|Mzeq= 455031.8|Myeq= -204.7|
 Ss = -917.8

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 130
 ----- PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 10- 1 187647.0 107434.9 0.0 -11831.7 1952.7 410.7

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 10- 1|si| 9|Sx Si| -885.9 0.0 0.0 885.9
 ----- PROGR. 27.50

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 449243.3 90.7 0.0 -10252.3 3.3 1027.0

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 9|Sx Si| -906.8 0.0 0.0 906.8
 ----- PROGR. 55.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 477485.3 0.3 0.0 -10233.0 3.3 1027.0

TENSIONI :
 Caso|Ve|No|massimi| Sx Tz Ty Si
 1- 1|si| 9|Sx Si| -956.0 0.0 0.0 956.0

VERIFICA STABILITA' :

Caso 1- 1 |LO = 55.0|LC = 38.5|Ro = 5.1|Im= 7.6|
 Nodo 9 |om = 1.00|csz= 1.00|csy= 1.00|
 Infless. Y

|Ncrz =100573954.6|Ncry= 31988033.3|
 |Nmax = -10271.6|Mzeq= 454891.7|Myeq= 108.7|
 Ss = -917.2

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 131
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 421973.1 137.4 0.0 -10271.0 2.5 1035.1
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|9|Sx Si Sx Ty Si
 -859.2 0.0 0.0 859.2

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 450438.6 68.6 0.0 -10251.7 2.5 1035.1
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|9|Sx Si Sx Ty Si
 -908.9 0.0 0.0 908.9

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 478904.1 -0.3 0.0 -10232.4 2.5 1035.1
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|8|Sx Si Sx Ty Si
 -958.5 0.0 0.0 958.5

VERIFICA STABILITA' :

Caso 1- 1 |L0 = 55.0|Lc = 38.5|Ro = 5.1|Im= 7.6|
 Nodo 9 |om = 1.00|csz= 1.00|csy= 1.00|
 Infless. Y
 |Ncrz =100573954.6|Ncry= 31988033.3|
 |Nmax = -10271.0|Mzeq= 456131.7|Myeq= 82.3|
 Ss = -919.3

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 132
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 -422239.9 -93.6 0.0 -10271.7 -1.7 -1034.6
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|18|Sx Si Sx Ty Si
 -809.6 0.0 0.0 809.6

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 -450691.0 -47.0 0.0 -10252.5 -1.7 -1034.6
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|18|Sx Si Sx Ty Si
 -856.0 0.0 0.0 856.0

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 -479142.0 -0.4 0.0 -10233.2 -1.7 -1034.6
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|18|Sx Si Sx Ty Si
 -902.4 0.0 0.0 902.4

VERIFICA STABILITA' :

Caso 1- 1 |L0 = 55.0|Lc = 38.5|Ro = 5.1|Im= 7.6|
 Nodo18 |om = 1.00|csz= 1.00|csy= 1.00|
 Infless. Y
 |Ncrz =100573954.6|Ncry= 31988033.3|
 |Nmax = -10271.7|Mzeq= -456381.2|Myeq= -56.4|
 Ss = -865.7

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 133
 PROGR. 0.00

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 -421087.3 -260.3 0.0 -10271.5 -4.7 -1026.4
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|18|Sx Si Sx Ty Si
 -808.3 0.0 0.0 808.3

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY
 1- 1 -449312.7 -130.4 0.0 -10252.2 -4.7 -1026.4
 TENSIONI :
 Caso|Ve|No|massimi
 1- 1|si|18|Sx Si Sx Ty Si
 -854.0 0.0 0.0 854.0

SOLLECITAZIONI :
 Caso MZ MY MT N TZ TY

1- 1	-477538.2	-0.4	0.0	-10232.9	-4.7	-1026.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	18	Sx	Si	0.0	0.0
				-899.7		899.7

VERIFICA STABILITA' :

Caso 1- 1 | LO = 55.0 | LC = 38.5 | Ro = 5.1 | Im = 7.6 |
 Nodo18 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Influss. Y

| Ncrz = 100573954.6 | Ncry = 31988033.3 |
 | Nmax = -10271.5 | Mzeq = -454957.8 | Myeq = -156.4 |
 Ss = -863.7

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 134
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-421053.8	199.4	0.0	-10271.6	3.6	-1026.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	17	Sx	Si	0.0	0.0
				-808.0		808.0

 PROGR. 27.50

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-449267.8	99.5	0.0	-10252.3	3.6	-1026.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	17	Sx	Si	0.0	0.0
				-853.8		853.8

 PROGR. 55.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-477481.9	-0.3	0.0	-10233.0	3.6	-1026.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	18	Sx	Si	0.0	0.0
				-899.6		899.6

VERIFICA STABILITA' :

Caso 1- 1 | LO = 55.0 | LC = 38.5 | Ro = 5.1 | Im = 7.6 |
 Nodo17 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Influss. Y

| Ncrz = 100573954.6 | Ncry = 31988033.3 |
 | Nmax = -10271.6 | Mzeq = -454910.6 | Myeq = 119.5 |
 Ss = -863.5

U_HEB180+UPN160 (2) - metodo: tensioni ammissibili - ASTA 135
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-422412.8	114.2	0.0	-11533.1	2.1	-1036.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	17	Sx	Si	0.0	0.0
				-824.1		824.1

 PROGR. 27.50

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-450907.4	57.2	0.0	-11513.8	2.1	-1036.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	17	Sx	Si	0.0	0.0
				-870.5		870.5

 PROGR. 55.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	-479401.9	0.3	0.0	-11494.6	2.1	-1036.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty
1- 1	si	17	Sx	Si	0.0	0.0
				-916.9		916.9

VERIFICA STABILITA' :

Caso 1- 1 | LO = 55.0 | LC = 38.5 | Ro = 5.1 | Im = 7.6 |
 Nodo17 | om = 1.00 | csz = 1.00 | csy = 1.00 |
 Influss. Y

| Ncrz = 100573954.6 | Ncry = 31988033.3 |
 | Nmax = -11533.1 | Mzeq = -456606.3 | Myeq = 68.6 |
 Ss = -880.3

VERIFICA ELEMENTI IN ACCIAIO
 lavoro : SCIPR3

Unita' di misura : Kgf ; cm ; Kgf/cmq ; Kgf*cm

MATERIALI

Fe360: Mod.El.= 2100000.; Samm= 1600.(1400. per sp>40 mm)

CASI DI CARICO

N	Descrizione	Soil.
1	P.P.+ Perm.	1
2	P.P.+Perm.(no masset	1
3	C.2 +Pretens.	1
4	C.3+Nuovo Massetto	1
5	C.4 + Accid.	1
6	C.5 + Vx	1
7	C.5 + Vy	1
8	C.5 + Dt	2
9	C.5 + Sx	2
10	C.5 + Sy	2

CARATTERISTICHE GEOMETRICHE

P_IPE550_S001 (1) :

A =134.4390E+00 Jz= 67.1308E+03 Jy= 2.6676E+03 Jt= 91.0612E+00

P_IPE550_S001 (1)

- metodo: tensioni ammissibili - ASTA 136
PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 2	-220435.7	4.2	0.0	43980.9	2.4	6198.1
1- 1	-479598.1	0.6	0.0	-3531.7	0.4	9208.9

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 2	si	1	Sx	417.5	0.0	0.0	417.5
1- 1	si	5	Tz	170.2	27.6	0.0	176.8
1- 1	si	9	Ty	-26.3	0.0	-172.2	299.5
8- 2	si	11	Si	403.9	0.0	-90.7	433.4

PROGR. 150.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	452227.8	-782.9	0.0	-65381.3	5.3	2925.2
1- 1	709860.8	-66.1	0.0	-3531.7	0.4	6650.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-674.7	0.0	0.0	674.7
1- 1	si	5	Tz	-317.1	19.9	0.0	319.0
1- 1	si	9	Ty	-26.3	0.0	-124.4	217.1

PROGR. 300.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	669881.4	-1571.8	0.0	-65381.3	5.3	-23.1
1- 1	1515581.2	-132.8	0.0	-3531.7	0.4	4092.3

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-766.9	0.0	0.0	766.9
1- 1	si	5	Tz	-647.3	12.3	0.0	647.6
1- 1	si	9	Ty	-26.3	0.0	-76.5	135.2

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.19 |
 Infless. Y
 | Ncrz = 15459597.3 | Ncry = 614333.6 |
 | Nmax = -65381.3 | Mzeq = 502411.0 | Myeq = -1178.9 |
 Ss = -841.7

P_IPE550_S001 (1)

- metodo: tensioni ammissibili - ASTA 139
PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	670808.8	-765.9	0.0	-65571.9	-2.6	26.1
1- 1	1515928.9	-96.0	0.0	-3562.4	-0.3	-4091.2

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-765.6	0.0	0.0	765.6
1- 1	si	5	Tz	-647.6	-12.3	0.0	647.9
1- 1	si	9	Ty	-26.5	0.0	76.5	135.2

PROGR. 150.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	453610.6	-380.9	0.0	-65571.9	-2.6	-2922.1
1- 1	710381.6	-47.8	0.0	-3562.4	-0.3	-6649.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-675.1	0.0	0.0	675.1
1- 1	si	5	Tz	-317.6	-19.9	0.0	319.4
1- 1	si	9	Ty	-26.5	0.0	124.4	217.1

PROGR. 300.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
------	----	----	----	---	----	----

8-1	-205826.0	4.2	0.0	-65571.9	-2.6	-5870.4
1-1	-478904.1	0.5	0.0	-3562.4	-0.3	-9207.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	3	Sx	-572.1	0.0	0.0
1-1	si	5	Tz	169.7	-27.6	0.0
1-1	si	9	Ty	-26.5	0.0	172.2
8-1	si	14	Si	-559.4	0.0	85.9
						572.1
						176.3
						299.5
						578.9

VERIFICA STABILITA' :

Caso 8-1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.19 |
 Infless. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -65571.9 | Mzeq = 503106.6 | Myeq = -574.4 |
 Ss = -841.0

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 140
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-2	-219264.5	0.7	0.0	42126.8	0.1	6223.9
1-1	-477481.9	0.1	0.0	-3752.4	0.0	9210.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-2	si	1	Sx	403.2	0.0	0.0
1-1	si	6	Tz	167.7	-27.6	0.0
1-1	si	9	Ty	-27.9	0.0	-172.3
8-2	si	11	Si	389.7	0.0	-91.1
						403.2
						174.4
						299.7
						420.4

PROGR. 150.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	457736.4	26.5	0.0	-67356.2	-0.2	2955.4
1-1	712255.6	1.0	0.0	-3752.4	0.0	6652.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	2	Sx	-688.6	0.0	0.0
1-1	si	6	Tz	-319.7	-19.9	0.0
1-1	si	9	Ty	-27.9	0.0	-124.4
8-1	si	6	Si	-688.6	-8.9	0.0
						688.6
						321.5
						217.3
						688.7

PROGR. 300.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	679920.8	52.4	0.0	-67356.2	-0.2	7.1
1-1	1518254.7	2.0	0.0	-3752.4	0.0	4094.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	2	Sx	-779.8	0.0	0.0
1-1	si	6	Tz	-649.9	-12.3	0.0
1-1	si	9	Ty	-27.9	0.0	-76.6
						779.8
						650.2
						135.5

VERIFICA STABILITA' :

Caso 8-1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Infless. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -67356.2 | Mzeq = 509940.6 | Myeq = 39.3 |
 Ss = -858.5

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 143
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	680208.7	82.0	0.0	-67178.6	0.3	-6.1
1-1	1518252.4	3.7	0.0	-3741.4	0.0	-4094.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	2	Sx	-778.7	0.0	0.0
1-1	si	6	Tz	-649.8	12.3	0.0
1-1	si	9	Ty	-27.8	0.0	76.6
						778.7
						650.1
						135.5

PROGR. 150.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8-1	458177.9	41.2	0.0	-67178.6	0.3	-2954.3
1-1	712252.7	1.9	0.0	-3741.4	0.0	-6652.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8-1	si	2	Sx	-687.5	0.0	0.0
1-1	si	6	Tz	-319.6	19.9	0.0
1-1	si	9	Ty	-27.8	0.0	124.4
8-1	si	6	Si	-687.4	8.9	0.0
						687.5
						321.5
						217.3
						687.6

PROGR. 300.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY

8- 1	-206091.2	0.4	0.0	-67178.6	0.3	-5902.6
1- 1	-477485.3	0.0	0.0	-3741.4	0.0	-9210.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	3	Sx	-584.1	0.0	0.0
1- 1	si	6	Tz	167.8	27.6	0.0
1- 1	si	9	Ty	-27.8	0.0	172.3
8- 1	si	14	Si	-571.5	0.0	86.4
						584.1
						174.4
						299.7
						590.7

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Influss. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -67178.6 | Mzeq = 510156.5 | Myeq = 61.5 |
 Ss = -857.0

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 144
 PROGR. 0.00

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
8- 2	-219495.7	-0.8	0.0	42107.1	0.0	6224.7
1- 1	-477538.2	0.0	0.0	-3743.9	0.0	9210.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 2	si	2	Sx	403.1	0.0	0.0
1- 1	si	5	Tz	167.8	27.6	0.0
1- 1	si	9	Ty	-27.8	0.0	-172.3
8- 2	si	12	Si	389.7	0.0	-91.1
						403.1
						174.4
						299.7
						420.4

SOLLECITAZIONI PROGR. 150.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	457593.7	-13.3	0.0	-67190.5	0.1	2953.7
1- 1	712187.5	-1.0	0.0	-3743.9	0.0	6652.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	1	Sx	-687.3	0.0	0.0
1- 1	si	5	Tz	-319.6	19.9	0.0
1- 1	si	9	Ty	-27.8	0.0	-124.4
8- 1	si	5	Si	-687.3	8.8	0.0
						687.3
						321.5
						217.3
						687.4

SOLLECITAZIONI PROGR. 300.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	679533.8	-26.2	0.0	-67190.5	0.1	5.5
1- 1	1518174.9	-1.9	0.0	-3743.9	0.0	4094.1
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	1	Sx	-778.3	0.0	0.0
1- 1	si	5	Tz	-649.8	12.3	0.0
1- 1	si	9	Ty	-27.8	0.0	-76.6
						778.3
						650.1
						135.5

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Influss. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -67190.5 | Mzeq = 509650.4 | Myeq = -19.6 |
 Ss = -856.7

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 147
 PROGR. 0.00

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
8- 1	679682.4	-37.9	0.0	-67205.9	-0.1	-5.0
1- 1	1518123.4	-1.8	0.0	-3743.6	0.0	-4094.3
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	1	Sx	-778.5	0.0	0.0
1- 1	si	5	Tz	-649.7	-12.3	0.0
1- 1	si	9	Ty	-27.8	0.0	76.6
						778.5
						650.1
						135.5

SOLLECITAZIONI PROGR. 150.00

Caso	MZ	MY	MT	N	TZ	TY
8- 1	457816.0	-19.2	0.0	-67205.9	-0.1	-2953.2
1- 1	712110.3	-1.0	0.0	-3743.6	0.0	-6652.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	1	Sx	-687.5	0.0	0.0
1- 1	si	5	Tz	-319.6	-19.9	0.0
1- 1	si	9	Ty	-27.8	0.0	124.4
8- 1	si	5	Si	-687.5	-8.8	0.0
						687.5
						321.4
						217.3
						687.6

SOLLECITAZIONI PROGR. 300.00

Caso	MZ	MY	MT	N	TZ	TY
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8- 1	-206288.7	-0.6	0.0	-67205.9	-0.1	-5901.5
1- 1	-477641.3	-0.1	0.0	-3743.6	0.0	-9210.8
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	4	Sx	-584.4	0.0	0.0
1- 1	si	5	Tz	167.8	-27.6	0.0
1- 1	si	9	Ty	-27.8	0.0	172.3
8- 1	si	13	Si	-571.7	0.0	86.4
						591.0

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Infless. y | Ncrz = 15459597.3 | Ncry = 614333.6 |
 | Nmax = -67205.9 | Mzeq = 509761.8 | Myeq = -28.4 |
 | Ss = -856.9

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 148
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 2	-220411.6	-5.1	0.0	43825.8	-3.6	6195.0
1- 1	-479142.0	-0.5	0.0	-3548.7	-0.4	9208.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 2	si	2	Sx	416.3	0.0	0.0
1- 1	si	6	Tz	169.9	-27.6	0.0
1- 1	si	9	Ty	-26.4	0.0	-172.2
8- 2	si	12	Si	402.8	0.0	-90.7
						432.3

PROGR. 150.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	453146.7	447.7	0.0	-65523.6	-3.0	2925.3
1- 1	710222.5	56.3	0.0	-3548.7	-0.4	6650.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	2	Sx	-674.8	0.0	0.0
1- 1	si	6	Tz	-317.4	-19.9	0.0
1- 1	si	9	Ty	-26.4	0.0	-124.4
						217.1

PROGR. 300.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	670819.3	899.4	0.0	-65523.6	-3.0	-23.0
1- 1	1515848.7	113.1	0.0	-3548.7	-0.4	4091.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	2	Sx	-765.7	0.0	0.0
1- 1	si	6	Tz	-647.5	-12.3	0.0
1- 1	si	9	Ty	-26.4	0.0	-76.5
						135.2

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.19 |
 Infless. y | Ncrz = 15459597.3 | Ncry = 614333.6 |
 | Nmax = -65523.6 | Mzeq = 503114.4 | Myeq = 674.6 |
 | Ss = -841.0

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 151
 PROGR. 0.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	670968.7	868.3	0.0	-65600.0	2.9	23.5
1- 1	1515955.2	113.0	0.0	-3553.6	0.4	-4091.4
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	2	Sx	-766.2	0.0	0.0
1- 1	si	6	Tz	-647.6	12.3	0.0
1- 1	si	9	Ty	-26.4	0.0	76.5
						135.2

PROGR. 150.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	453368.9	432.1	0.0	-65600.0	2.9	-2924.8
1- 1	710382.4	56.2	0.0	-3553.6	0.4	-6649.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
8- 1	si	2	Sx	-675.4	0.0	0.0
1- 1	si	6	Tz	-317.5	19.9	0.0
1- 1	si	9	Ty	-26.4	0.0	124.4
						217.0

PROGR. 300.00

SOLLECITAZIONI						
Caso	MZ	MY	MT	N	TZ	TY
8- 1	-206469.4	-4.1	0.0	-65600.0	2.9	-5873.0
1- 1	-478928.8	-0.6	0.0	-3553.6	0.4	-9207.9

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	4	Sx	-572.5	0.0	0.0	572.5
1-1	si	6	Tz	169.8	27.6	0.0	176.4
1-1	si	9	Ty	-26.4	0.0	172.2	299.5
8-1	si	13	Si	-559.9	0.0	85.9	579.3

VERIFICA STABILITA' :

Caso 8-1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.19 |
 Infless. Y | Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -65600.0 | Mzeq = 503226.6 | Myeq = 651.2 |
 Ss = -841.7

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 152
 PROGR. 0.00

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
8-1	668993.2	-1563.7	0.0	-63549.9	-4.9	2936.5
1-1	1513400.9	-132.1	0.0	-3406.9	-0.3	4601.2

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-752.9	0.0	0.0	752.9
1-1	si	6	Tz	-645.2	-13.8	0.0	645.6
1-1	si	9	Ty	-25.4	0.0	-86.1	151.2

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
1-1	2011706.4	-81.0	0.0	-3406.9	-0.3	2042.9

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1-1	si	1	Sx	-849.8	0.0	0.0	849.8
1-1	si	6	Tz	-849.3	-6.1	0.0	849.4
1-1	si	9	Ty	-25.4	0.0	-38.2	70.9

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
1-1	2126273.5	-30.0	0.0	-3406.9	-0.3	-515.3
9-1	732837.5	-215.5	0.0	-29502.8	-3.1	-3103.4

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1-1	si	1	Sx	-896.5	0.0	0.0	896.5
9-1	si	5	Tz	-519.9	-9.4	0.0	520.1
9-1	si	9	Ty	-219.5	0.0	58.0	241.4

VERIFICA STABILITA' :

Caso 8-1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.18 |
 Infless. Y | Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -63549.9 | Mzeq = 888348.8 | Myeq = -1172.7 |
 Ss = -983.1

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 153
 PROGR. 0.00

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
1-1	2126273.7	-30.1	0.0	-3422.2	0.2	516.5
9-2	730933.6	-304.3	0.0	-29443.3	1.8	3104.9

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1-1	si	1	Sx	-896.6	0.0	0.0	896.6
9-2	si	5	Tz	-518.8	9.3	0.0	519.0
9-2	si	9	Ty	-219.1	0.0	-58.1	241.1

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
1-1	2011880.0	-62.8	0.0	-3422.2	0.2	-2041.8

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1-1	si	1	Sx	-849.9	0.0	0.0	849.9
1-1	si	6	Tz	-849.5	6.1	0.0	849.6
1-1	si	9	Ty	-25.5	0.0	38.2	70.9

SOLLECITAZIONI

Caso	MZ	MY	MT	N	TZ	TY
8-1	669914.9	-763.1	0.0	-63927.9	2.2	-2933.4
1-1	1513748.0	-95.4	0.0	-3422.2	0.2	-4600.0

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8-1	si	1	Sx	-752.9	0.0	0.0	752.9
1-1	si	6	Tz	-645.5	13.8	0.0	645.9
1-1	si	9	Ty	-25.5	0.0	86.0	151.2

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.18 |
 Infless. Y |
 Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -63927.9 | Mzeq = 888811.7 | Myeq = -572.3 |
 Ss = -984.1

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 154
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	679067.3	54.9	0.0	-68536.9	1.4	2951.1
1- 1	1516076.8	2.1	0.0	-3907.5	0.1	4601.8

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	2	Sx	-788.2	0.0	0.0	788.2
1- 1	si	5	Tz	-650.1	13.8	0.0	650.6
1- 1	si	9	Ty	-29.1	0.0	-86.1	151.9

PROGR. 150.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	900619.1	-155.7	0.0	-68536.9	1.4	2.9
1- 1	2014478.7	-17.6	0.0	-3907.5	0.1	2043.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-879.3	0.0	0.0	879.3
1- 1	si	5	Tz	-854.3	6.1	0.0	854.4
1- 1	si	9	Ty	-29.1	0.0	-38.2	72.3

PROGR. 300.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2129142.3	-37.4	0.0	-3907.5	0.1	-514.7
9- 1	745452.7	-313.2	0.0	-33664.2	1.1	-3094.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	1	Sx	-901.4	0.0	0.0	901.4
9- 1	si	6	Tz	-555.4	9.3	0.0	555.7
9- 1	si	9	Ty	-250.5	0.0	57.9	269.8

VERIFICA STABILITA' :

Caso 8- 1 | L0 = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Infless. Y |
 Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -68536.9 | Mzeq = 900619.1 | Myeq = -274.7 |
 Ss = -1032.1

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 155
 PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2129142.1	-37.4	0.0	-3895.1	-0.1	514.7
9- 2	745571.2	-336.5	0.0	-33690.6	-1.2	3093.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	1	Sx	-901.3	0.0	0.0	901.3
9- 2	si	6	Tz	-555.7	-9.3	0.0	555.9
9- 2	si	9	Ty	-250.7	0.0	-57.9	270.0

PROGR. 150.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	900764.5	-141.6	0.0	-68260.8	-1.5	-1.9
1- 1	2014477.7	-16.8	0.0	-3895.1	-0.1	-2043.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	1	Sx	-877.3	0.0	0.0	877.3
1- 1	si	5	Tz	-854.2	-6.1	0.0	854.3
1- 1	si	9	Ty	-29.0	0.0	38.2	72.3

PROGR. 300.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	679362.2	82.7	0.0	-68260.8	-1.5	-2950.1
1- 1	1516074.9	3.9	0.0	-3895.1	-0.1	-4601.8

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	2	Sx	-786.4	0.0	0.0	786.4
1- 1	si	5	Tz	-650.0	-13.8	0.0	650.5
1- 1	si	9	Ty	-29.0	0.0	86.1	151.9

VERIFICA STABILITA' :

Caso 8- 1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 1 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Influss. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -68260.8 | Mzeq = 900764.5 | Myeq = -274.4 |
 Ss = -1029.5

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 156
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
8- 1		678681.8	-27.3	0.0	-68170.5	-1.0	2950.2
1- 1		1515997.2	-2.1	0.0	-3893.2	-0.1	4601.7

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
8- 1	si	1	Sx	-785.2	0.0	0.0	785.2
1- 1	si	6	Tz	-650.0	-13.8	0.0	650.4
1- 1	si	9	Ty	-29.0	0.0	-86.1	151.9
8- 1	si	5	Si	-785.1	8.8	0.0	785.3

SOLLECITAZIONI : PROGR. 150.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
8- 1		900093.2	129.0	0.0	-68170.5	-1.0	1.9
1- 1		2014387.1	17.3	0.0	-3893.2	-0.1	2043.5

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
8- 1	si	2	Sx	-876.3	0.0	0.0	876.3
1- 1	si	6	Tz	-854.2	-6.1	0.0	854.2
1- 1	si	9	Ty	-29.0	0.0	-38.2	72.3

SOLLECITAZIONI : PROGR. 300.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
1- 1		2129038.6	36.6	0.0	-3893.2	-0.1	-514.8
9- 1		745195.9	304.5	0.0	-33543.8	-1.0	-3099.3

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
1- 1	si	2	Sx	-901.3	0.0	0.0	901.3
9- 1	si	5	Tz	-554.4	-9.3	0.0	554.7
9- 1	si	9	Ty	-249.4	0.0	58.0	268.9

VERIFICA STABILITA' :

Caso 8- 1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.20 |
 Influss. Y

Ncrz = 15459597.3 | Ncry = 614333.6 |
 Nmax = -68170.5 | Mzeq = 900093.2 | Myeq = 214.0 |
 Ss = -1028.1

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 157
 PROGR. 0.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
1- 1		2129038.7	36.6	0.0	-3895.5	0.1	514.6
9- 2		745312.1	329.3	0.0	-33697.5	1.1	3098.8

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
1- 1	si	2	Sx	-901.3	0.0	0.0	901.3
9- 2	si	5	Tz	-555.6	9.3	0.0	555.8
9- 2	si	9	Ty	-250.6	0.0	-58.0	269.9

SOLLECITAZIONI : PROGR. 150.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
8- 1		900167.4	122.9	0.0	-68195.4	1.1	-1.5
1- 1		2014361.4	17.3	0.0	-3895.5	0.1	-2043.6

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
8- 1	si	2	Sx	-876.5	0.0	0.0	876.5
1- 1	si	6	Tz	-854.2	6.1	0.0	854.2
1- 1	si	9	Ty	-29.0	0.0	38.2	72.3

SOLLECITAZIONI : PROGR. 300.00

SOLLECITAZIONI		MZ	MY	MT	N	TZ	TY
Caso							
8- 1		678830.0	-39.5	0.0	-68195.4	1.1	-2949.7
1- 1		1515945.7	-1.9	0.0	-3895.5	0.1	-4601.9

TENSIONI		No	massimi	Sx	Tz	Ty	Si
Caso	Ve						
8- 1	si	1	Sx	-785.5	0.0	0.0	785.5
1- 1	si	6	Tz	-650.0	13.8	0.0	650.4
1- 1	si	9	Ty	-29.0	0.0	86.1	151.9
8- 1	si	5	Si	-785.4	-8.8	0.0	785.5

VERIFICA STABILITA' :

Caso 8- 1 | LO = 300.0 | Lc = 300.0 | Ro = 4.5 | Im = 67.3 |
 Nodo 2 | om = 1.29 | csz = 1.01 | csy = 1.20 |

Infless. Y

|Ncrz = 15459597.3|Ncry= 614333.6|
|Nmax = -68195.4|Mzeq= 900167.4|Myeq= 214.0|
Ss = -1028.3

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 158
PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	669931.4	894.7	0.0	-64040.1	2.4	2935.9
1- 1	1513667.4	112.5	0.0	-3397.1	0.3	4600.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	2	Sx Si	-754.3	0.0	0.0	754.3
1- 1	si	5	Tz	-645.2	13.8	0.0	645.7
1- 1	si	9	Ty	-25.2	0.0	-86.1	151.2

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2011895.5	68.8	0.0	-3397.1	0.3	2042.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	2	Sx Si	-849.7	0.0	0.0	849.7
1- 1	si	5	Tz	-849.4	6.1	0.0	849.4
1- 1	si	9	Ty	-25.3	0.0	-38.2	70.8

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2126385.1	25.0	0.0	-3397.1	0.3	-515.9
9- 1	732023.7	180.1	0.0	-29415.0	2.7	-3116.4

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	2	Sx Si	-896.4	0.0	0.0	896.4
9- 1	si	6	Tz	-518.9	9.4	0.0	519.1
9- 1	si	9	Ty	-218.8	0.0	58.3	240.9

VERIFICA STABILITA :

Caso 8- 1 |L0 = 300.0|Lc = 300.0|Ro = 4.5 |Im= 67.3|
Nodo 2 |om = 1.29|csz= 1.01|csy= 1.19|
Infless. Y |Ncrz = 15459597.3|Ncry= 614333.6|
|Nmax = -64040.1|Mzeq= 889200.1|Myeq= 689.0|
Ss = -985.9

P_IPE550_S001 (1) - metodo: tensioni ammissibili - ASTA 159
PROGR. 0.00

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2126384.9	25.0	0.0	-3374.5	-0.3	516.2
9- 2	731170.3	251.8	0.0	-29002.1	-2.6	3117.6

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	2	Sx Si	-896.3	0.0	0.0	896.3
9- 2	si	6	Tz	-515.5	-9.4	0.0	515.8
9- 2	si	9	Ty	-215.7	0.0	-58.3	238.2

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
1- 1	2011948.6	68.7	0.0	-3374.5	-0.3	-2042.0

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
1- 1	si	2	Sx Si	-849.6	0.0	0.0	849.6
1- 1	si	5	Tz	-849.2	-6.1	0.0	849.3
1- 1	si	9	Ty	-25.1	0.0	38.2	70.8

SOLLECITAZIONI :

Caso	MZ	MY	MT	N	TZ	TY
8- 1	670078.2	863.7	0.0	-63870.5	-2.3	-2935.4
1- 1	1513773.8	112.4	0.0	-3374.5	-0.3	-4600.3

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
8- 1	si	2	Sx Si	-753.0	0.0	0.0	753.0
1- 1	si	5	Tz	-645.1	-13.8	0.0	645.5
1- 1	si	9	Ty	-25.1	0.0	86.0	151.1

VERIFICA STABILITA :

Caso 8- 1 |L0 = 300.0|Lc = 300.0|Ro = 4.5 |Im= 67.3|
Nodo 2 |om = 1.29|csz= 1.01|csy= 1.18|
Infless. Y |Ncrz = 15459597.3|Ncry= 614333.6|
|Nmax = -63870.5|Mzeq= 889273.1|Myeq= 668.9|
Ss = -984.2